Nuclear Criticality Safety Evaluation for Contact-Handled Transuranic Waste Containers at the Waste Isolation Pilot Plant

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Revision 1, July 2009, Clarified limits in response to comments received during implementation. Revised shielded container calculations based on final drawing.	S.L. Larson	S.M. Painter
Revision 2, October 2010, Revised SLB2 calculations based on TRUPACT-III TRAMPAC.	D.L. Newell	S.L. Larson
Revision 3, August 2011, Included overpack considerations for damaged containers.	D.L. Newell	S.L. Larson
Revision 4, January 2014, Included CCO calculations based on TRUPACT-II TRAMPAC	B.A. Larsen	S.L. Larson
Revision 5, June 2015, Revised overbatch description and included radiological release event. Added assumption section to Section 9.0 and changed assume to evaluate throughout document where applicable.	B.A. Larsen	S.L. Larson
Revision 6, November 2021, Revised Appendix D and Appendix G to evaluate compacted waste in pipe overpacks and Criticality Control Overpacks, respectively. Incorporated changes to appendices into the main body and limit tables. Removed evaluation of the ARROW-PAK™ container, which was proposed but never used at WIPP. Made typographical corrections throughout the entire document.	N. Dickes S.L. Larson	E.P. Elliott W.D. Newmyer
Revision 7, September 2022, Added Appendix H to consolidate the Shielded Container analyses and evaluate four new designs. Removed Shielded Container analysis from Appendices A, B, and C and incorporated changes to appendices into the main body and limit tables.	N. Dickes S.L. Larson	W.D. Newmyer
Revision 8, July 2026, Revised Appendix C to increase the direct loaded SWB limit to 200 FGE and remove the 250 FGE limit for a 100-gal drum overpacked in an SWB. Reperformed all calculations in Appendix C in MCNP6.2 and incorporated changes to appendices into the main body and limit tables.	H.J. Zhu N. Dickes	S.L. Larson

EXECUTIVE SUMMARY

This nuclear criticality safety evaluation (NCSE) of the Waste Isolation Pilot Plant (WIPP) facility contact-handled (CH) transuranic (TRU) waste handling, storage, and disposal process provides a comprehensive analysis of waste forms, container types, and container stacking configurations at the WIPP. This NCSE addresses the disposal configuration during active waste emplacement up to when the filled panel is removed from active ventilation with a panel closure or substantial and isolation barrier.

Transuranic waste is currently shipped to the WIPP from the U.S. Department of Energy generator sites in the Transuranic Package Transporter Model II (TRUPACT-II) or Half-package Transporter (HalfPACT) shipping containers. The CH waste containers currently approved for disposal at WIPP include seven packs of 55-gallon drums, four packs of 85-gallon drums, or three packs of 100-gallon drums or shielded containers, standard waste boxes, ten drum overpacks, criticality control overpacks, and pipe configurations overpacked in 55-gallon drums. Waste may also be shipped in the Transuranic Package Transporter Model III (TRUPACT-III), which contains a standard large box 2 (SLB2).

This NCSE considers the normal WIPP waste handling, storage, and disposal configurations of these waste containers and evaluates interactions between the different waste forms in the various waste container types. The primary criticality control for WIPP is the fissile mass and special moderator/ reflector mass limits established by this NCSE for each container type and presented in Section 9.0. The fissile and special moderator/reflector mass limits for each waste container type are verified at generator sites through a waste certification process. While the transportation packages have specified fissile limits based on the associated analyses required to transport transuranic waste, the fissile limits modeled in this NCSE meet or exceed the transportation limit for each waste assembly. This was done to establish the maximum fissile and special moderator/reflector loading for each waste container type to be disposed of in the underground at WIPP while still remaining safety subcritical. This is conservative with respect to the fissile limits authorized for shipment.

The NCSE includes an evaluation of credible upset scenarios during waste handling, disposal, and storage at WIPP. The evaluation concludes that no credible criticality accident scenarios exist for CH waste container storage, handling, and disposal processes at the WIPP. Because the evaluation also demonstrates that a criticality accident at the WIPP is not credible, criticality alarm and detection systems are not required.

Section 9.0 also identifies the acceptable configurations for waste storage and disposal at WIPP.

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LIST OF ACRONYMS

AEOF	average energy of fission
ASTM	American Society for Testing and Materials
Be/Pu	beryllium-to-plutonium (ratio)
CBFO	Carlsbad Field Office
CCC	criticality control container
CCO	criticality control overpack
$C_6H_{10}O_5$	cellulose
CH	contact-handled
DOE	U.S. Department of Energy
DOT	U.S. Department of Transportation
DSA	Documented Safety Analysis
FGE	fissile gram equivalent
H/D	height-to-diameter (ratio)
H/Pu	hydrogen-to-plutonium (ratio)
HalfPACT	half-package transporter
HWFP	Hazardous Waste Facility Permit
MCNP	Monte Carlo N-Particle transport code
MgO	magnesium oxide
NCSE	nuclear criticality safety evaluation
NaCl	sodium chloride
NDA	non-destructive analysis
NWP	Nuclear Waste Partnership LLC
PDP	Performance Demonstration Program
RH	remote-handled
SAR	Safety Analysis Report
SLB2	standard large box 2
SWB	standard waste box
TD	theoretical density
TDOP	ten-drum overpack
TRAMPAC	TRUPACT-II Authorized Methods for Payload Control
TRU	transuranic
TRUPACT-II	TRU Package Transporter Model II
TRUPACT-III	TRU Package Transporter Model III
USL	upper subcritical limit
WHB	Waste Handling Building
WIPP	Waste Isolation Pilot Plant
WIPP WAC	Transuranic Waste Acceptance Criteria for the Waste Isolation Pilot Plant

wt%	weight percent
WTS	Washington TRU Solutions LLC

1.0 Introduction

This nuclear criticality safety evaluation (NCSE) of the Waste Isolation Pilot Plant (WIPP) facility contact-handled (CH) transuranic (TRU) waste handling, storage, and disposal process provides a comprehensive analysis of waste forms at the WIPP. This NCSE addresses the disposal configuration during active waste emplacement up to when the filled panel is removed from active ventilation with a panel closure or substantial and isolation barrier.

Transuranic waste is currently shipped to the WIPP from the U.S. Department of Energy (DOE) generator sites in either the TRU Package Transporter Model II (TRUPACT-II) or Half-package Transporter (HalfPACT) shipping containers. The waste containers currently approved for disposal at WIPP include seven packs of 55-gallon drums, four packs of 85-gallon drums, or three packs of 100-gallon drums, one to three packs of shielded containers, standard waste boxes, ten drum overpacks, criticality control overpacks (CCOs), and pipe configurations overpacked in 55-gallon drums. Waste may also be shipped in the TRU Package Transporter Model III (TRUPACT-III), which contains a standard large box 2 (SLB2).

The NCSE includes an evaluation of credible upset scenarios and identifies the appropriate controls. The evaluation concludes that no credible criticality accident scenarios exist for the CH TRU waste storage, handling, and disposal process at the WIPP. Because the evaluation demonstrates that a criticality accident at the WIPP is not credible, criticality alarm and detection systems are not required. The controls that ensure a criticality accident remain not credible are presented in Section 9.0.

An extent of condition (WIPP-099, *Extent of Condition Review for WIPP-016, Rev. 7* [42]) was performed to Revision 7 of this NCSE to confirm all established limits, assumptions, and judgements were adequately analyzed. Notes added to the applicable appendices discuss the additional supportive analyses that were performed, all of which affirmed the NCSE conclusions.

2.0 Descriptions

2.1 Facility and Process Description

The WIPP is located in southeastern New Mexico, 26 miles east of Carlsbad. This site is owned by the DOE and operated by a Management and Operating (M&O) Contractor. The purpose of the WIPP facility is to serve as a final repository for defense generated TRU waste and to demonstrate the feasibility of safe disposal of radioactive wastes in deep underground salt formations. The majority of waste to be disposed of at the WIPP is TRU waste with plutonium as the primary TRU isotope.

Two categories of waste, CH and remote-handled (RH), are approved for disposal at the WIPP. CH waste containers have surface radiation levels not exceeding 200 mrem/hr and are handled directly by human operators. Remote-handled waste containers have surface radiation levels up to 1,000 rem/hr. This NCSE evaluates CH waste containers only. The CH waste containers approved for disposal at the WIPP must meet the requirements of the *Waste Isolation Pilot Plant Hazardous Waste Facility Permit* (HWFP) [1] and this NCSE.

Contact-handled TRU waste is currently received at the WIPP in various types of waste containers: 55-gallon drums, 85-gallon drums, 100-gallon drums, standard waste boxes (SWBs), ten-drum overpacks (TDOPs), shielded containers, CCOs, and SLB2s. Waste may fill a drum or be contained in a pipe for which the drum is an overpack (i.e., a pipe overpack). The TDOP is currently used to isolate containers that have surface contamination in excess of permissible limits or degraded physical integrity and can contain up to ten 55-gallon drums or one SWB. The waste containers are configured as assemblies of

seven-packs of 55-gallon drums, four-packs of 85-gallon drums, or three-packs of 100-gallon drums when transported in the TRUPACT-II. The shorter HalfPACT is used for one drum or shielded container assembly or SWB. The fissile isotope loading is restricted by the *TRUPACT-II Safety Analysis Report* (SAR) [2] and the *HalfPACT Safety Analysis Report* [3]. The SLB2 is designed for shipment in the TRUPACT-III and its loading is restricted by the *TRUPACT-III Safety Analysis Report* [4].

Transporters carrying TRU waste arrive at the WIPP and are parked on the south side of the Waste Handling Building (WHB). After the CH TRU shipping container is inspected for contamination, the loaded shipping container is moved into the WHB. The WHB has two TRUDOCKs and four overhead cranes for opening and unloading the TRUPACT-II and HalfPACT shipping containers. Each TRUDOCK is designed to handle up to two TRUPACT-IIs. The CH Bay provides space for transferring loaded facility pallets to the waste hoist via forklifts, a shielded holding area, a waste handling equipment battery recharge area, and temporary storage areas for waste containers.

Once at the TRUDOCKs, the shipping containers are opened, surveyed for radiation and contamination levels, and the waste containers removed and placed on a facility pallet. Figure 2-1 shows how seven-packs are loaded onto a facility pallet for transport in the underground. This figure also illustrates the use of slipsheets between layers of seven packs. In the event a damaged container is identified during or after receipt, the container may be "overpacked" into a larger container as discussed in further sections of this NCSE. (Note: this type of on-site overpacking process does not pertain to containers that may be received from the generator site(s) in an already overpacked condition and are disposed of in the as-received overpack).

The same concept is used for the other waste containers. The 0.15-inch-thick polyethylene slipsheet is used to provide a mechanism for sliding the waste container(s) off the pallet and into a disposal location. Alternatives (cardboard) to the polyethylene slipsheets are utilized with SWBs. The reinforcement plate shown in Figure 2-1 is a second polyethylene sheet. A pallet can hold up to four drum assemblies, two shielded container assemblies, four SWBs, two TDOPs, or one SLB2, or combinations where the waste is stacked no more than two drum assemblies or SWBs high on the pallet. The TDOP occupies the footprint of a seven-pack, but is as tall as two seven-pack assemblies. The pallet is either transferred to the conveyance loading car, which is moved into the hoist cage for transfer to the underground repository for permanent disposal, or is temporarily stored in the WHB in a designated area for future transfer to the repository.

The WIPP underground disposal repository consists of eight panels and two panel equivalents mined from the Salado formation, a 2,000-foot-thick series of salt beds (approximately 95% sodium chloride [NaCl]). Figure 2-2 shows a plan view of the WIPP underground disposal repository. The disposal level lies 2,150 feet below the surface, a little below the middle of the Salado formation. A typical underground panel contains seven rooms, each of which is 300-feet long, 33-feet wide, and 13-feet high. The access drifts connect the rooms in a panel and provide an additional length of 33 feet on each side of the room for drum storage. The emplacement of seven-packs is illustrated in Figure 2-3. A magnesium oxide (MgO) backfill is used in the WIPP to reduce actinide solubility in the unlikely event the facility is flooded. A "supersack" of MgO is placed on top of the waste container stack. Figure 2-4 shows a typical waste emplacement pattern with different waste containers. This pattern is designed so that seven-packs of 55-gallon drums, four-packs of 85-gallon drums, three-packs of 100-gallon drums, a TDOP, and an SWB all occupy the same "footprint." A closely-packed hexagonal lattice is achieved for containers occupying the footprint in the storage array as shown in Figure 2-4. There can be spacing between these units, but it is typically less than 2 inches and is currently not controlled. Figure 2-5 shows the proposed emplacement of SLB2s. Because the SLB2 is rectangular, additional void space exists between it and other assemblies in the disposal array.

The shielded container is an alternative to disposal of RH waste in canisters in the walls of the disposal rooms. The shielded container is shipped in a HalfPACT and transported to the underground on a facility pallet. Shielded containers are currently only stacked on the floor against the wall or on each other, for a maximum of two high as shown in Figure 2-6. However, this NCSE does not restrict shielded container placement as it evaluates them in the same storage configuration as 55-gallon drums.

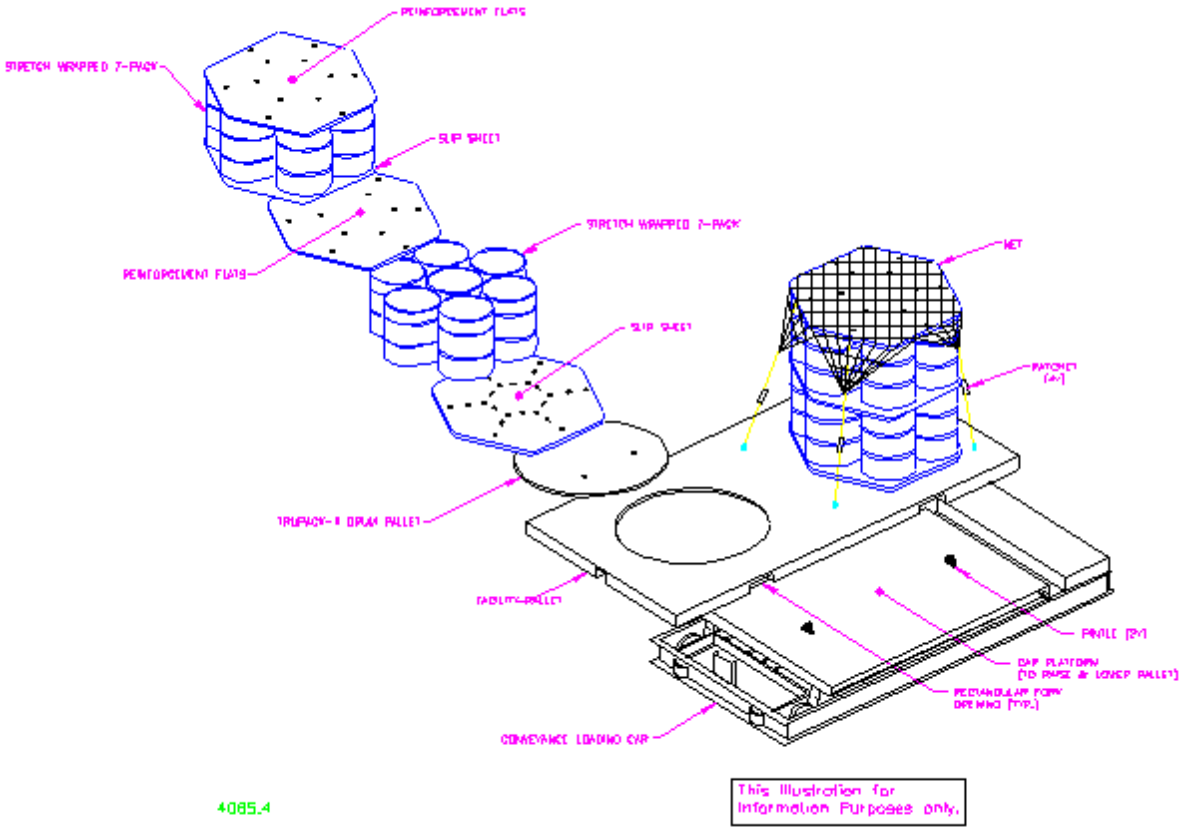


Figure 2-1. Seven Packs on a Facility Pallet

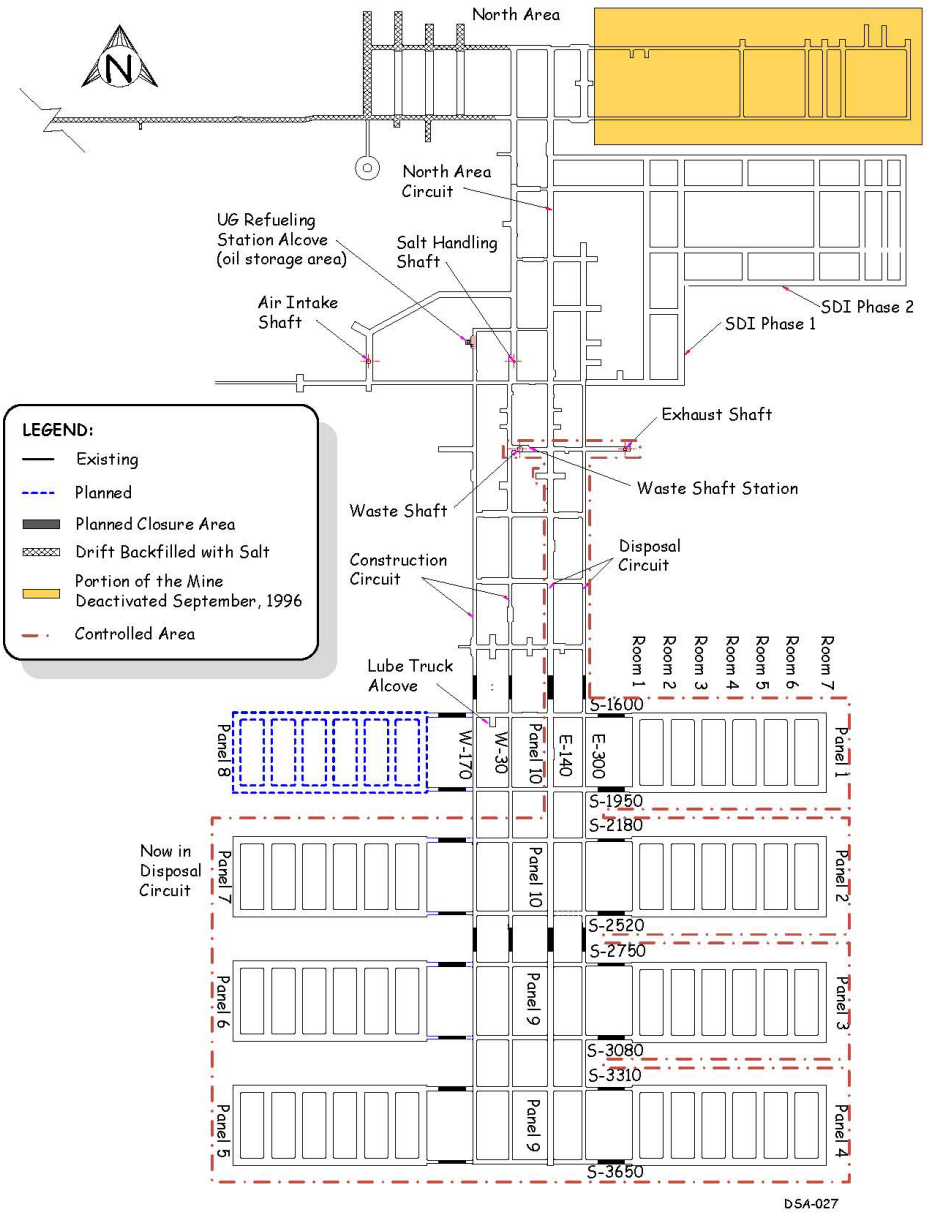


Figure 2-2. Layout of the WIPP Underground

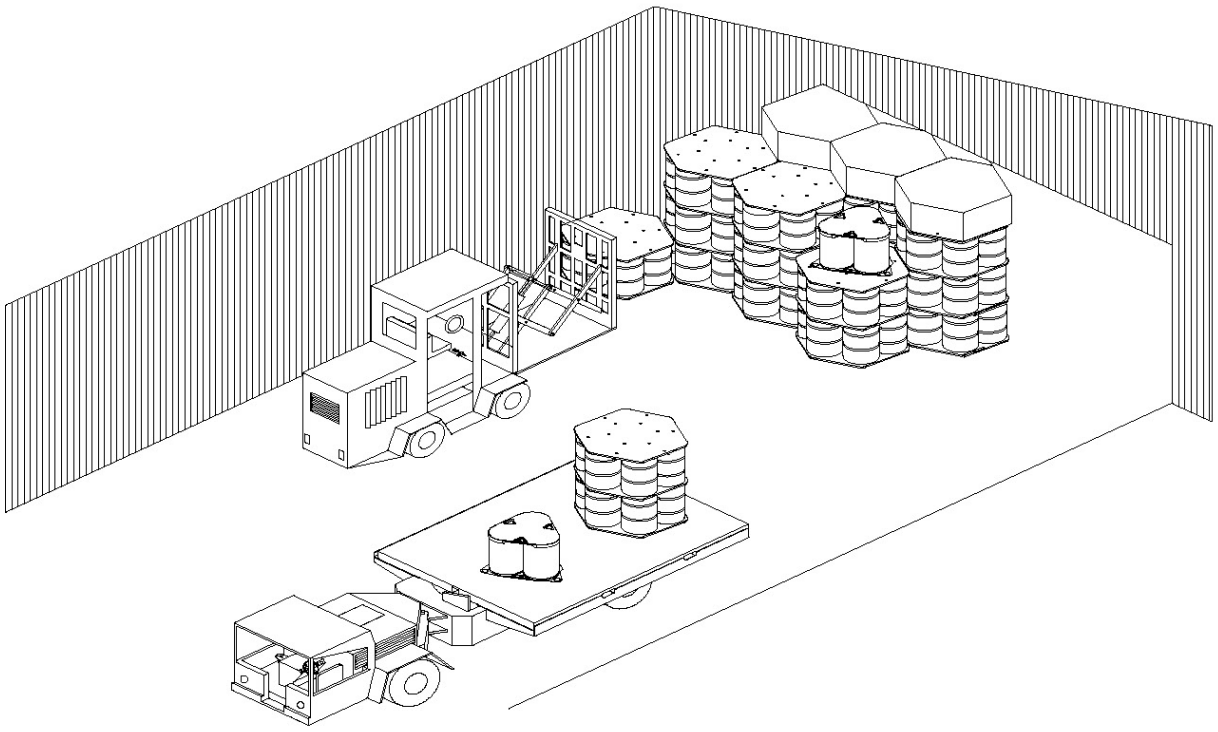


Figure 2-3. Drum Assemblies on the Transporter and Emplaced in the Disposal Array

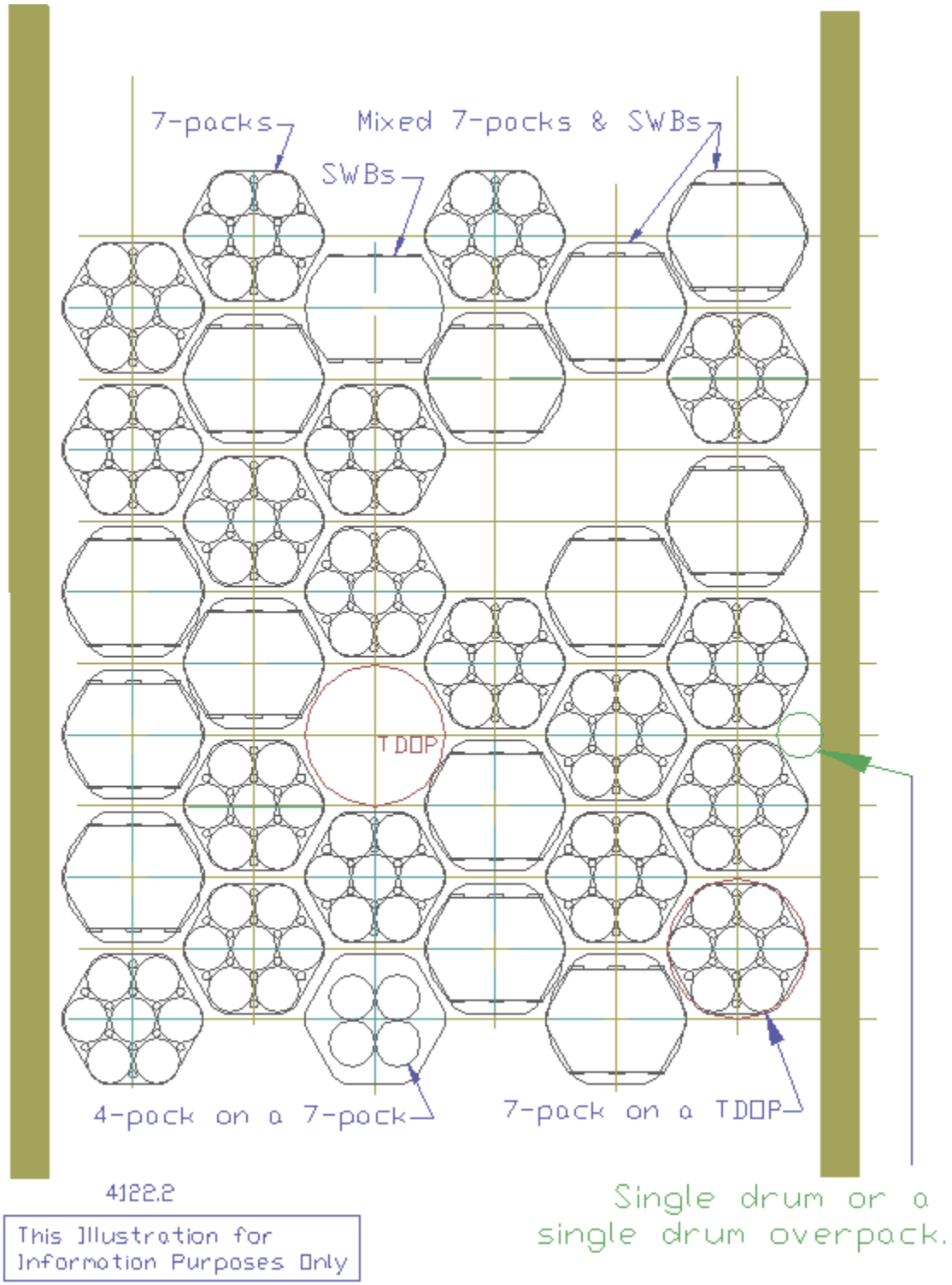


Figure 2-4. Typical Emplacement Pattern in the Underground Repository

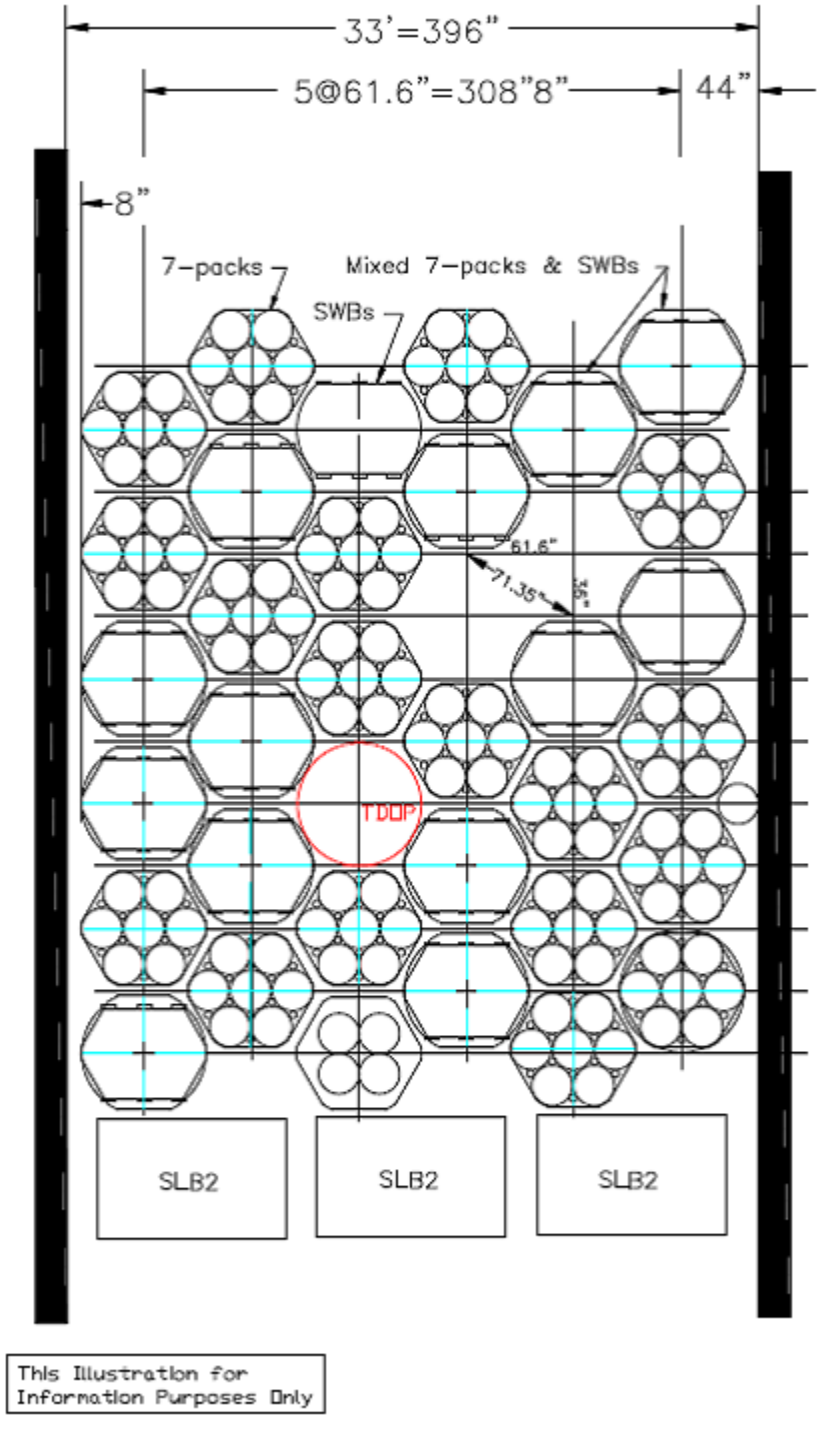


Figure 2-5. Typical Standard Large Box 2 Emplacement in the Underground Repository

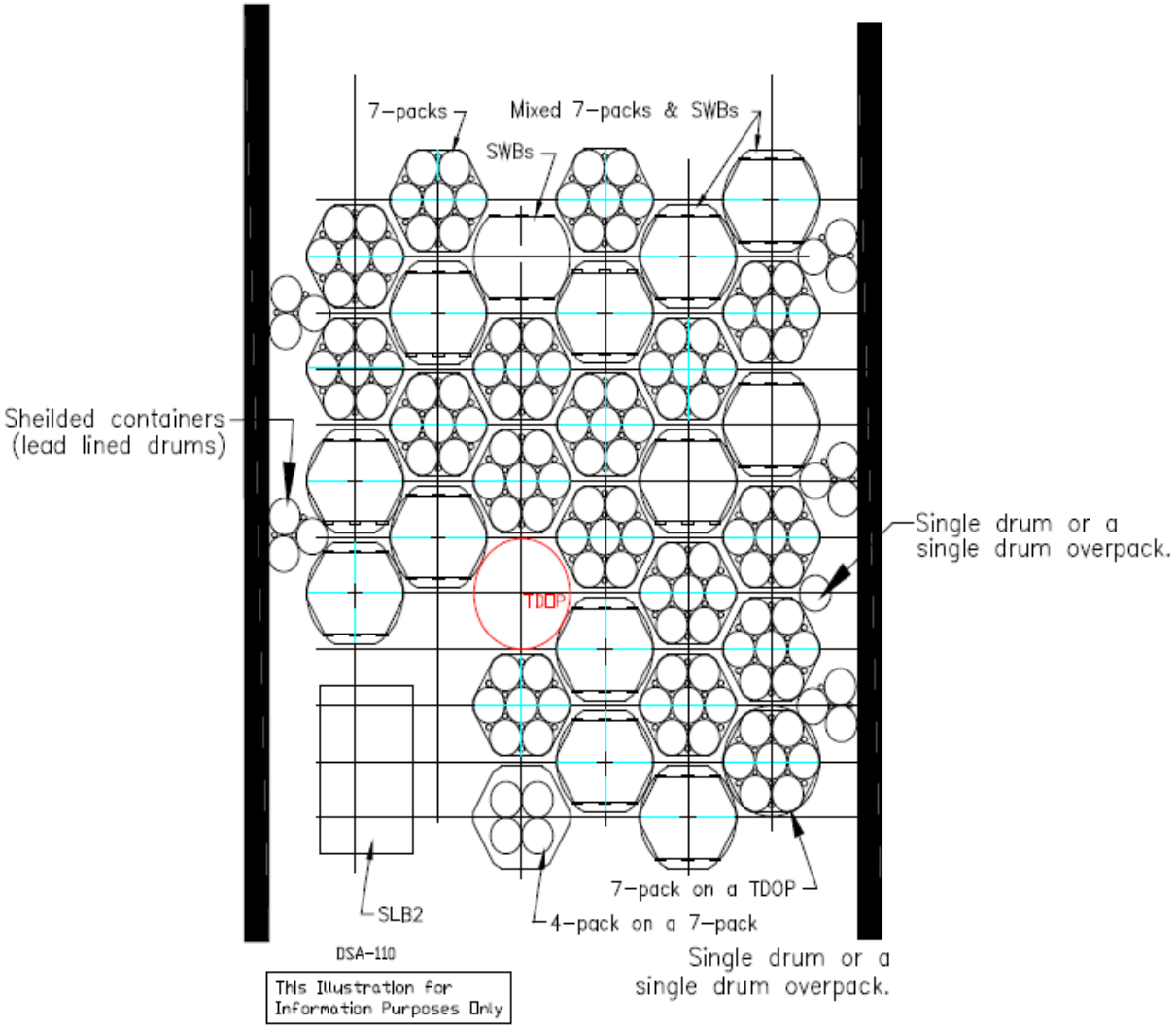


Figure 2-6. Shielded Container Emplacement in Underground Repository

2.2 Description of Waste Containers

Nine different container types are currently approved for disposal of CH waste at the WIPP and include 55-gallon drums, 85-gallon drums, 100-gallon drums, SWBs, SLB2s, pipe-overpacks, CCOs, shielded containers, and TDOPs. The five shielded container designs, described in Appendix H, are an alternative to RH canisters. These containers are considered in this analysis since the shielding will reduce the dose rate to levels appropriate for contact-handling and the disposal configuration will include these containers in the CH array. Thus, the shielded container is considered a CH container for the purposes of this analysis. Waste containers disposed of at the WIPP must meet the requirements of U.S. Department of Transportation (DOT) Type 7A.

The 55-gallon drum models in this NCSE are based on the dimensions given in Section 2.9.1 of the *Contact-Handled Transuranic Waste Authorized Methods for Payload Control (CH-TRAMPAC)* [5], which is based on the DOT 17H drum. The drum is constructed with an 18-gauge (0.0478-inch nominal) wall, and does not require a liner or plastic bagging. The drum has an inner diameter of 22.5 inches, an

interior height of 33.25 inches, a diameter across the rolling hoops of 24 inches, and an exterior height of 35 inches. The drum is authorized for a total gross weight of 900 or 1,000 pounds per Section 2.9.1 of the CH-TRAMPAC [5]. Table 2-1 summarizes the geometric characteristics of the DOT 17-H drum and Figure 2-7 depicts a generic illustration of the drum.

Table 2-1. Modeled 55-gallon Drum Dimensions

Dimension	Modeled Value (in.)	Modeled Value (cm)
Inner Radius	11.25	28.575
Outer Radius*	11.2978	28.69641
Inner Height	33.25	84.455
Outer Height*	33.3456	84.69782
Wall Thickness	0.0478	0.12141

* The Monte Carlo N-Particle (MCNP) transport code drum model uses inner dimensions plus the wall thickness.

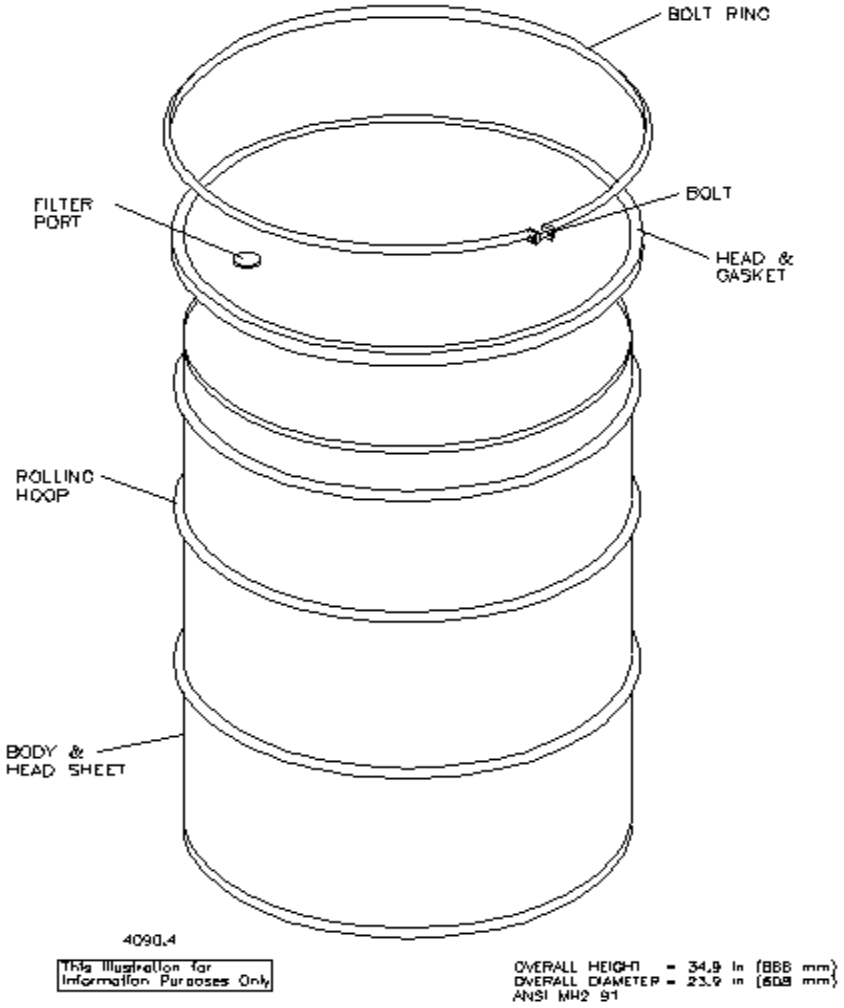


Figure 2-7. Typical 55-gallon Drum

In order to allow for increased fissile content in a single shipment and to allow for certain wastes to be contact handled, pipe overpack configurations for the 55-gallon drum have been approved. These configurations consist of an inner cylindrical container either approximately 6 or 12 inches in diameter surrounded by shock-absorbing dunnage. The waste is contained within the cylindrical containers, and additional shielding can be provided with inserts either in the containers or as part of the surrounding dunnage. The dunnage around the pipe consists of cane fiberboard packing in accordance with *Standard Specification for Cellulosic Fiber Insulating Board* (ASTM C208-95 [6]) and 1/2- or 1/4-inch plywood. In the case of the shielded 6-inch pipe component, a large portion of the dunnage is replaced by water extended polyester/ polyethylene composite or equivalent neutron shielding material. Sections 2.9.2 through 2.9.5 of the CH-TRAMPAC [5] describe the various configurations. The pipe components are constructed of 304 stainless steel. Further details of the pipe overpack actual and modeled dimensions are given in Appendix D of this NCSE.

In addition to the pipe overpack configurations, a CCO was also developed to allow for increased fissile content. The waste is contained within a criticality control container (CCC), an approximately 6-inch diameter cylindrical container constructed of 304 stainless steel. The CCC is placed inside of a 55-gallon drum and held in place by five plywood dunnage plates of 3/4-inch thickness at the top and bottom of the 55-gallon drum to provide stability. This configuration constitutes the CCO waste container as shown in Figure 2-8. Further details of the CCO and model dimensions are given in Appendix G of this NCSE.

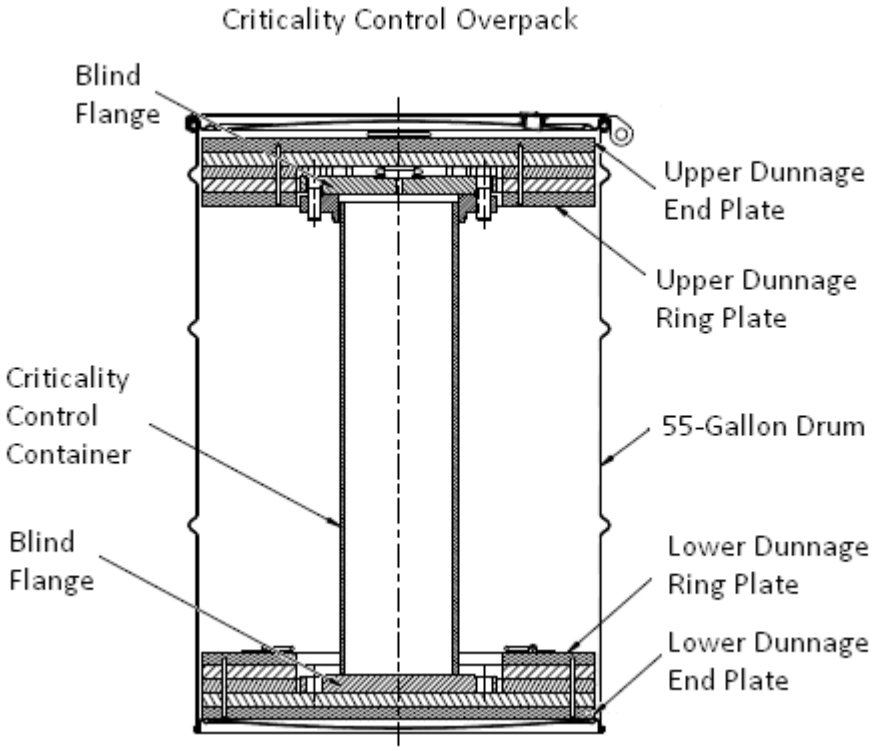


Figure 2-8. CCO Assembly

In addition to the 55-gallon drums, 85- and 100-gallon drums are also authorized for disposal at the WIPP. These drums may be direct loaded but are typically used as an overpack. The 85-gallon drums are bounded by the analysis of arrays of smaller 55-gallon drums and larger 100-gallon drums. The 85-gallon drums will be emplaced into the repository in four-packs versus the seven-pack emplacement pattern for

55-gallon drums and three-pack pattern for 100-gallon drum arrays. The two-container configurations for 85-gallon drums are bounded by the two-container model with 100-gallon drums presented in Section 5.4 as both drum types have 16-gauge walls per DOE/RL-96-57 (*DOE UN Container Packaging Specifications DOT 7A, Type A Cross Reference* [7]) and Drawing 53-9840 (*General Arrangement & Details 100-Gallon Puck Drum* [8]).

Figure 2-9 and Figure 2-10 illustrate a typical 100-gallon drum. This drum is constructed with a 16-gauge (0.0598 inch nominal) wall and is an authorized container for machine-compacted waste. The compacted wastes typically placed in the 100-gallon drum include 55-gallon drums that have been mechanically compressed into a puck, with up to 5 pucks placed in the 100-gallon drum. These drums are received at the WIPP facility and placed into the disposal array as a three-pack that occupies the area defined by a seven-pack of 55-gallon drums. The drum has an inner diameter of 30 inches, an interior height of 33.875 inches, a diameter across the rolling hoops of 31 inches, and an exterior height of 35 inches as shown in Drawing 53-9840 [8]. Table 2-2 shows the modeled dimensions for the 100-gallon drum. The drum is authorized for a total gross weight of 1,000 pounds per Section 2.9.7 of the CH-TRAMPAC [5].

Table 2-2. Modeled 100-gallon Drum Dimensions

Dimension	Modeled Value (in.)	Modeled Value (cm)
Inner Radius	15	38.1
Outer Radius*	15.0598	38.25189
Inner Height	33.875	86.0425
Outer Height*	33.9946	86.34628
Wall Thickness	0.0598	0.15189

* The MCNP transport code drum model uses inner dimensions plus the wall thickness.

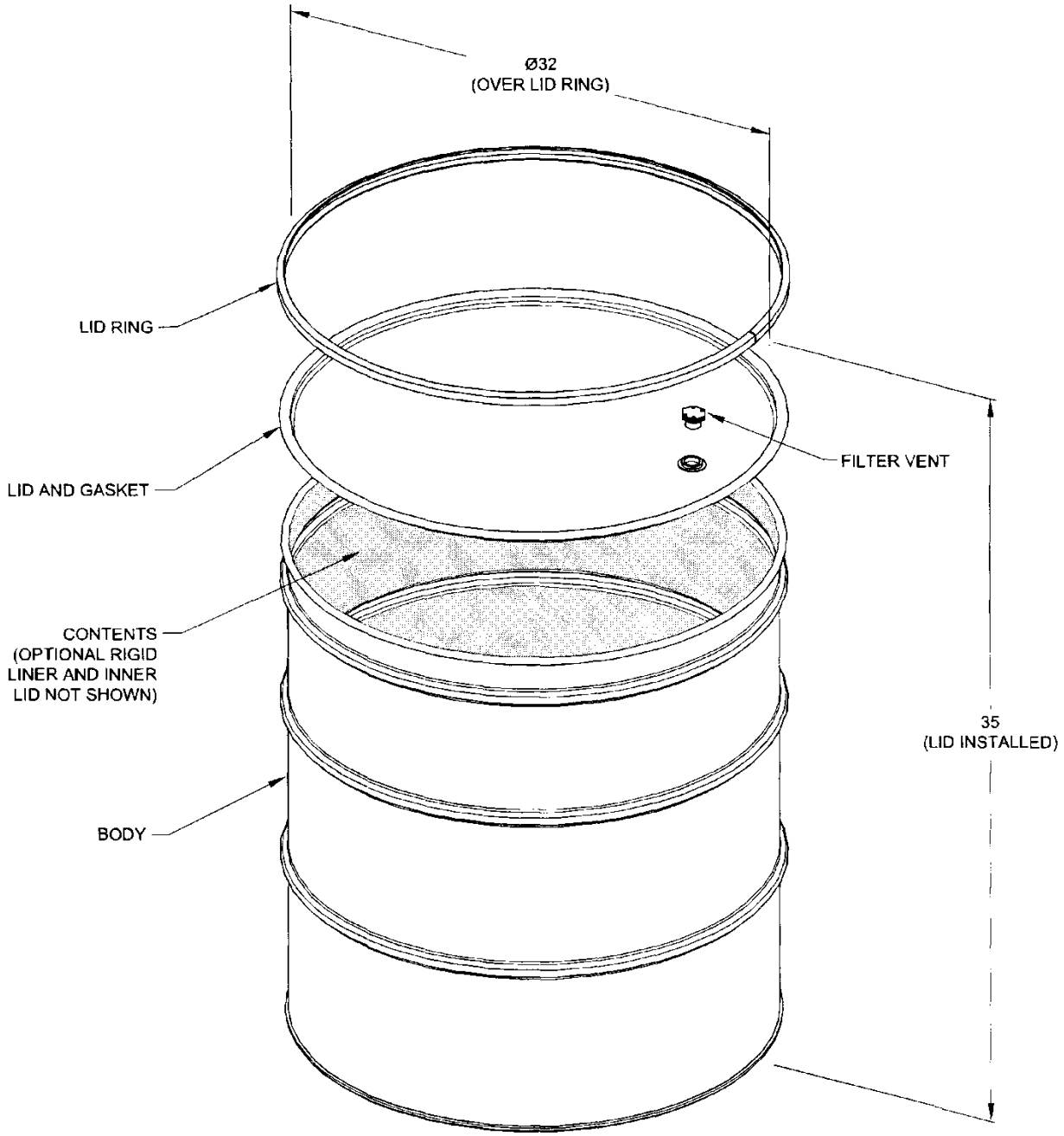


Figure 2-9. Typical 100-gallon Drum

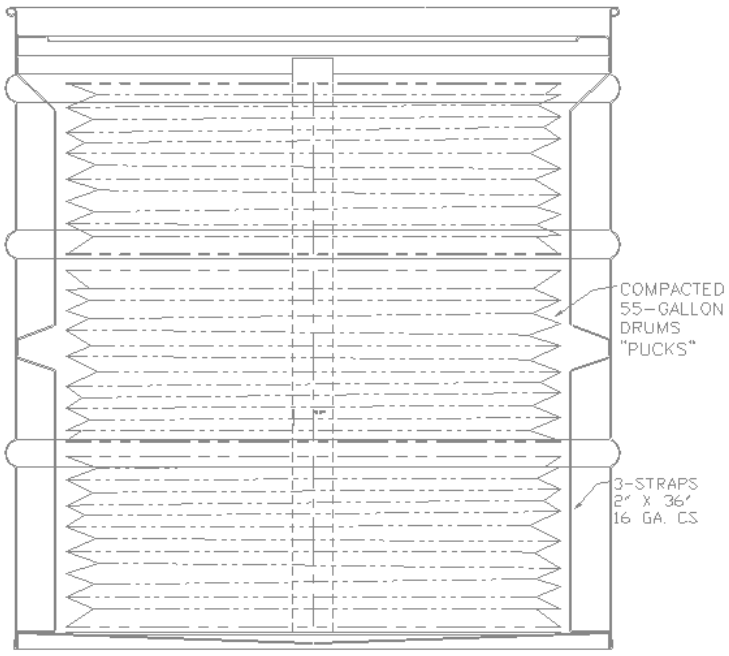


Figure 2-10. 100-gallon Drum Showing Machine-compacted Waste

The SWB is illustrated in Figure 2-11. Sides, walls, and bottom are constructed of 10-gauge carbon steel (ASTM A 569, *Standard Specification for Steel, Carbon (0.15 Maximum, Percent), Hot-Rolled Sheet and Strip Commercial* [9]). The ends of the box are rounded and the 1/8-inch-thick top lip is attached to the body for positive closure by screws located along the periphery of the box. The SWB dimensions modeled in MCNP transport code are given in Table 2-3, which result in an active volume of 1.92×10^6 cm^3. In addition to solids payloads, the SWB is authorized for transportation and disposal of four 55-gallon drums in an overpack arrangement. The SWB has a maximum gross weight of 4,000 pounds per Section 2.9.8 of the CH-TRAMPAC [5].

Table 2-3. Modeled SWB Dimensions

Dimension	Modeled Value (in.)	Modeled Value (cm)
Radius	34.375	87.3125
Inner Length	68.75	174.625
Inner Width	51.875	131.7625
Inner Height	36.75	93.345
Wall Thickness	0.125	0.3175

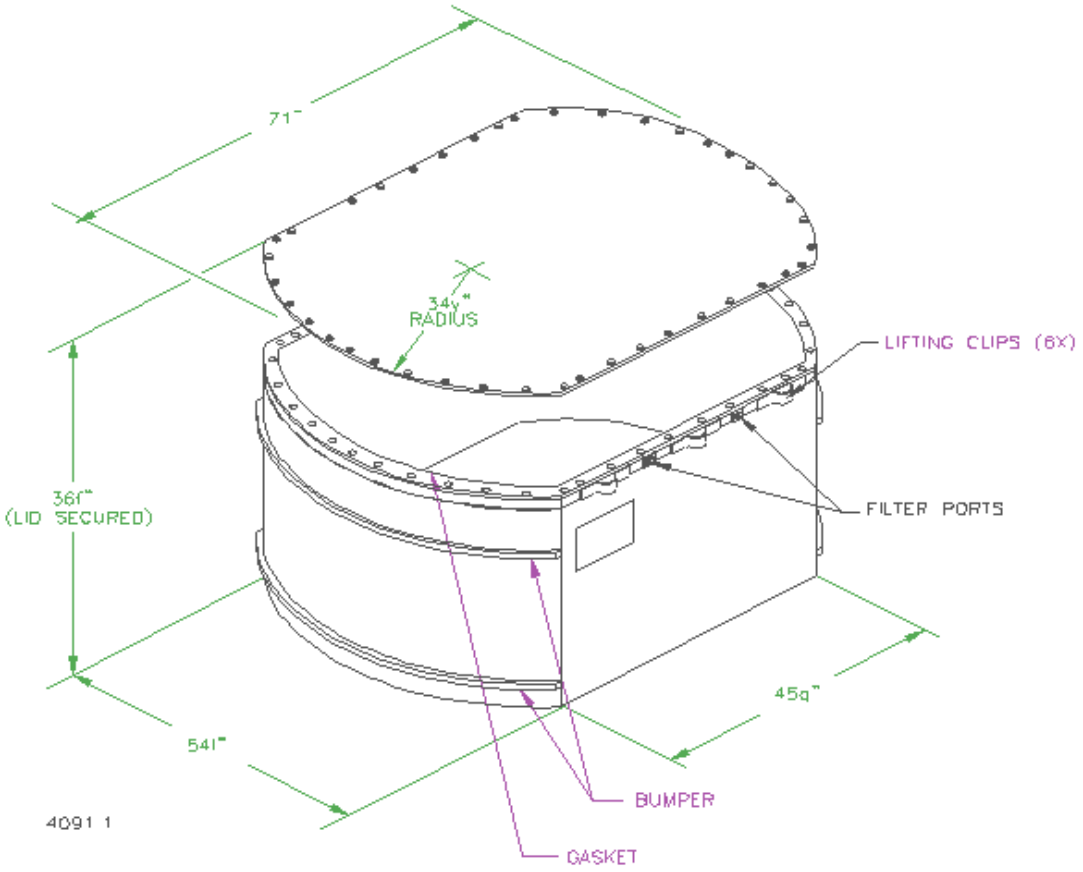


Figure 2-11. Standard Waste Box

The TDOP container is used to overpack up to ten containers that have some form of physical deterioration (e.g., rust or damage) or surface contamination and may contain up to ten 55-gallon drums or one SWB. The TDOP occupies the same footprint as a seven-pack of 55-gallon drums or an SWB, but is two tiers high. These containers are also not specifically assessed in this NCSE, since TDOPs are bounded by the SWB analysis. For direct-loaded waste, the TDOP total fissile mass is restricted to the same as that of a SWB and the maximum reflector packing fraction of 25% in both cases is the same. This results in a smaller areal density of fissile material than what may be contained within two SWBs, thus, the TDOPs are less reactive in the arrays than the SWB. In the two-container models of machine-compacted waste, the SWB also bounds TDOP because the fissile material in the SWB is fully reflected by the high-density polyethylene. Consequently, the additional non-fissile material in the TDOP will have little effect. The TDOP has a maximum gross weight of 6,700 pounds per Section 2.9.9 of the CH-TRAMPAC [5].

The SLB2 is a large box designed for transport in the TRUPACT-III shipping container. The SLB2 is only evaluated/approved for non-compacted waste with ≤ 1 wt% (where wt% is weight percent) special reflectors as that is the only waste form allowed to be shipped in the TRUPACT-III. An SLB2 may be either top loaded or bottom loaded but both have the same overall dimensions. The minimum inner dimensions of either SLB2 are 102 inches by 63 inches by 66 inches tall and the maximum outer dimensions are 108 inches by 69 inches by 73 inches tall as given in Drawing 165-F-016-W1 (*Standard*

Large Box 2 Assembly (SLB2) Top Loading [10]) and Drawing 165-F-017-W1 (*Standard Large Box 2 Assembly (SLB2) Bottom Loading* [11]). The dimensions modeled are shown in Table 2-4. The nominal inner dimensions plus applicable tolerances are such that the outer dimensions are less than the maximum values. The model consists of the inner payload volume, maximized based on tolerances, the minimum wall thickness around the payload volume, and a nominal 1.5-inch void area around the sides of the SLB2. The void represents the spacing created by protrusions around the actual payload volume while the protrusions themselves are modeled as void. The protrusions on top of the SLB2 are conservatively ignored to increase interaction with containers stacked on top of it. The bottom of the SLB2 is modeled with 4-inch square hollow steel skids with 1/8-inch-thick walls.

Table 2-4. Modeled Standard Large Box 2 Dimensions

Dimension	Modeled Value (in.)	Modeled Value (cm)
Inner Length	104.5	265.43
Inner Width	65.31	165.89
Inner Height	66.31	168.43
Wall Thickness	0.1875	0.48

There are five different types of shielded containers, as described in detail in Appendix H, designed to hold either a 30 gallon or 55-gallon drum with different amounts of shielding. The bounding shielded container from an NCS perspective, the SC-30G1, has the least amount of shielding and thus allows for the most interaction between the fissile material in adjacent containers. The SC-30G1 has approximately the same exterior dimensions as a standard 55-gallon drum and is designed to hold a 30-gallon drum. The cylindrical sidewall of the shielded container has nominal 1-inch-thick lead shielding sandwiched between steel shells as shown in Figure 2-12. The external wall is 11-gauge steel and the internal wall is 7-gauge steel. The lid and bottom of the container are carbon steel approximately 3 inches thick. The shielded container and the inner 30-gallon drum will be vented. The container has been tested to DOT Type 7A specifications, which will ensure that the container is safe for transport and handling and will contain the waste under the most severe accident conditions. The SC-30G1 is modeled with both the nominal dimensions and with the tolerance applied in a manner that maximizes the lead shielding thickness, because lead is an excellent neutron reflector. These dimensions, as summarized in Table 2-5, are taken from Drawing 163-008 Rev. 4 (*SC-30G1 Shielded Container SAR Drawing* [12]).

Table 2-5. Modeled Shielded Container SC-30G1 Dimensions

Dimension	Nominal Value (in.)[a]	Tolerance (in.)	Modeled Value (in.)	Modeled Value (cm)	Treatment of Tolerance
Inner Height	29.750	N/A	29.750	75.5650	N/A, tolerance not specified
Inner Diameter	20.375	-0.125	20.250	51.435	Minimum inner diameter to maximize Pb thickness
Inner Steel Wall Thickness	0.179 (7 gauge)	N/A	0.179	0.4547	Tolerance not specified
Lead Wall Thickness	1.00	N/A	1.166	2.9616	N/A, calculated value based on treatment of other tolerances
Outer Steel Wall Thickness	0.12 (11 gauge)	N/A	0.120	0.3048	Tolerance not specified
Outer Diameter	23.0	+0.180	23.180	58.8772	Maximum outside diameter to maximize Pb thickness
Lid/Bottom Thickness	3.0	N/A	3.0	7.62	Tolerance not specified

[a] Values used in "Nominal" Model

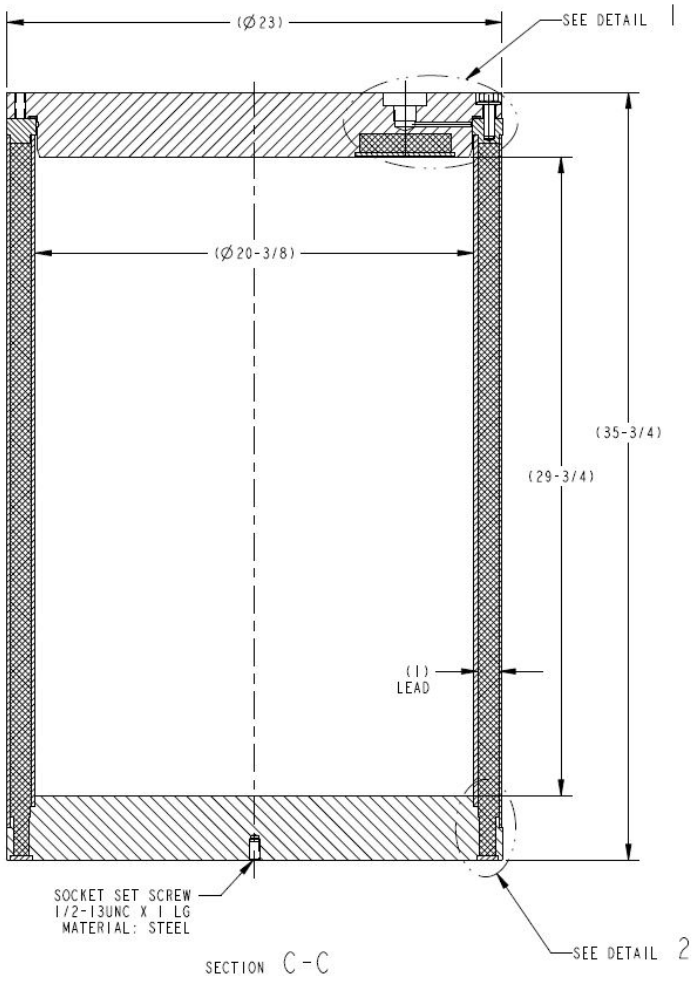


Figure 2-12. Shielded Container Model SC-30G1

3.0 Requirements Documentation

The WIPP facility is subject to the requirements of DOE O 420.1C Chg. 3, *Facility Safety*, Attachment 2, Chapter III, "Nuclear Criticality Safety" [13]. Compliance with the double contingency requirements of DOE Order 420.1C Chg. 3 is demonstrated for CH waste containers in this analysis. This NCSE is written to meet the content requirements of DOE-STD-3007-2007, *Guidelines for Preparing Criticality Safety Evaluations at Department of Energy Nonreactor Nuclear Facilities* [14].

4.0 Methodology

4.1 Evaluation Method

The methodology used in this NCSE evaluates control of both ^{239}Pu and special reflector materials, modeled as beryllium, in each waste container. Mass limits for plutonium and beryllium are the primary criticality safety control for storage, handling, and disposal of waste at the WIPP facility. After defining and evaluating the different container geometries, loading configurations and payloads in Sections 5.1 and 5.2, the overall bounding configurations for handling, storage and disposal are identified and narrowed to two bounding configurations. The two bounding configurations were evaluated using MCNP5 (LA-UR-03-1987, *MCNP — A General Monte Carlo N-Particle Transport Code, Version 5* [15]) or MCNP6.2 (LA-UR-17-29981, *MCNP User's Manual, Code Version 6.2* [16]) to determine the appropriate fissile mass limits.

The first configuration modeled is an infinite array of waste containers in the underground repository. The containers are stacked three tiers high and a hexagon placed close around the stacks as shown in Figure 2-4; however, the hexagon is infinitely reflected to model a tight-packed, infinite array. The MgO supersack is modeled on top of the stack and salt reflection modeled above the MgO and below the containers. The array results are summarized in Section 5.3.

The second configuration, termed the two-container model, evaluates two containers stacked on top of one another with the fissile masses closely located. The fissile mass in the lower container is positioned up against the container lid and the fissile mass in the upper container is concentrated on the bottom of the container directly above the mass in the lower container. The two containers are then infinitely reflected on all sides with concrete, MgO, or salt to represent the various reflector materials available above ground and in the underground repository. This configuration represents the worst-case fissile material interaction and reflection. The two-container results are summarized in Section 5.4.

Section 6.0 contains the parameter evaluation. In this section, the controlled parameters are identified as well as the contingent conditions to be evaluated in the event control of the parameter is lost. The hazard evaluation documented in Appendix F also provides a basis for the contingencies. Section 7.0 evaluates various contingent conditions related to waste operations at WIPP. The array model is used as the basis for these upset conditions.

The above configurations are evaluated for each waste type in detail in the appendices. Non-compacted, direct loaded waste is evaluated in Appendix A with less than or equal to 1 wt% special reflector materials and in Appendix B with higher special reflector material contents. Machine-compacted waste is evaluated in Appendix C. Pipe overpack drum assemblies containing non-compacted and compacted waste are evaluated separately in Appendix D and two-container configurations pairing up two different container types or loadings are evaluated in Appendix E. CCO assemblies containing non-compacted waste are evaluated separately in Appendix G. Shielded containers containing non-compacted waste and compacted waste are evaluated in Appendix H.

4.1.1 Evaluation Special Reflectors

Special reflectors are materials that provide greater than 25% polyethylene/75% water equivalent reflection. Special reflector analysis report SAIC-1322-001, *Reactivity Effects of Moderator and Reflector Materials on a Finite Plutonium System* [17] analyzed elements and select compounds resulting in the identification of six special reflectors. This analysis showed that, in known TRU waste configurations, only Beryllium (Be) and Beryllium Oxide (BeO) in quantities greater than 1% by weight could credibly increase the system reactivity more than 25% polyethylene/75% water. Process knowledge identified the other special reflectors as being chemically/mechanically bound to the fissile material or in forms/quantities that could not credibly reconfigure as a reflector. Therefore, in WIPP TRU waste, this analysis concluded the other evaluated elements and compounds could not credibly act as special reflectors.

GEN-REP-0002, *Analysis of Reflector Materials* [18] is an expanded analysis of the SAIC-1322-001 analysis that includes all solid elements and compounds identified to date in the TRU waste inventory. From this list, special reflectors are identified that could potentially provide reflection equivalent to a 2 ft thickness of 25% polyethylene and 75% water mixture (baseline for manually compacted waste) or 100% polyethylene (baseline for machine compacted waste) under either of the following originally implemented screening criteria:

- Less than 11/16 inch thick at 70% of theoretical density in the form of tightly-packed particulate solids.
- Less than 20% packing fraction at 24 inches thick in the form of randomly dispersed particulate solids.

Processes have been developed to assess if these special reflectors are present in a form, quantity, and concentration that would meet criteria defined in GEN-REP-0002. If a reflector material does not meet the GEN-REP-002 criteria for being a special reflector, FGE limits do not need to be lowered to accommodate the material. As an example, if the special reflector material, other than Be and some Be compounds, is chemically or mechanically bound to the fissile material, it acts as a moderator and not a reflector and a lower FGE limit is not needed. For the purposes of this NCSE, Be is modeled to bound all other special reflector materials and establish lower FGE limits where applicable.

4.2 Monte Carlo Computational Method

Monte Carlo calculations were performed to evaluate the reactivity state of various container type/package contents combinations and configurations.

4.2.1 MCNP5

Calculations supporting Revisions 0 to 5 of this NCSE were performed using MCNP5 [15] on a personal computer. The MCNP5 computer code was run under the allowed Microsoft® platforms and validated in accordance to established guidelines (*Verification of MCNP5 on SAIC Computers* [19]). Only the precompiled version of MCNP5 supplied by the vendor (Los Alamos National Laboratory) was used and the Evaluated Neutron Data File VI library was used for all cases.

Per CS-2004-002, *MCNP5 Bias Validation for the WIPP* [20] and CS-2002-002, *Determination of Calculational Bias for Criticality Calculations at the WIPP using MCNP* [21], the upper subcritical limit (USL) for MCNP at the WIPP for non-graphite bearing waste is 0.97. This USL includes an

administrative margin associated with using salt or MgO as a reflector. The USL was found to initially be 0.975 although the large presence of salt (NaCl) as a reflector was not considered to be adequately addressed in the benchmarks resulting in the addition of an administrative margin of 0.005. The basis for this offset value was that a USL of 0.975 gave a 5% probability that 1 in 10,000 critical systems would be modeled as having a reactivity of ≤0.975. Therefore, to account for salt or MgO reflection, a 1 in 100,000 USL was chosen that equated to 0.97. CS-2004-002 also considered steel containers in the development of the bias. The USL is also applicable to beryllium-bearing waste as justified in CS-2003-001, *Waste Isolation Plant Nuclear Criticality Safety Evaluation for Contact Handled Transuranic Waste Storage* [22]. The USL determination does include a number of benchmarks with beryllium. However, these were systems with average energy fission group well above the thermal range. The Falstaff experiments detailed in U233-SOL-INTER-001 of the *International Handbook of Evaluated Criticality Safety Benchmark Experiments* [23] were used in the reference to help further validate the use of MCNP for problems that involve beryllium at other than fast energies. These experiments consist of a steel spherical shell that contains a solution of uranium fluoride and water. The steel shell is reflected by different combinations of beryllium metal and polyethylene.

A supplemental validation document, SAIC-WIPP-VAL-001, *MCNP5 Bias Validation For Lead And Low Enriched Uranium At The Waste Isolation Pilot Plant* [24], was written to evaluate lead reflection and is applicable to the lead-lined drum calculations. The document evaluated 82 low enriched uranium benchmarks, 8 of which contained significant quantities of lead. The supplemental validation concluded that the lead benchmarks result in a higher USL when included in the evaluated benchmark set, as compared to when the benchmarks are removed. Thus, the USL determined in CS-2004-002 for plutonium systems is applicable for lead as modeled in the lead-lined drums.

In addition, the bias analysis states that if the average energy of fission (AEOF) is greater than 2.5 eV, then an additional 0.005 bias in k_{eff} should be utilized, which would further reduce the USL. Note that the AEOF values used were calculated based on the average neutron lethargy causing fission due to its basis from the KENO V.a runs taken from the benchmarks in CS-2002-002. This value was verified to be met based on the value of the "energy corresponding to the average neutron lethargy causing fission" in the MCNP output files, thus the USL was set at 0.97.

The 0.97 USL value was initially used in the development in NCSEs for CH waste containers. An additional 0.01 administrative margin has been applied in this NCSE to address concerns regarding administrative margin resulting in a final USL of 0.96. Some calculations originally done in earlier WIPP NCSEs have been revised to meet the final USL. Calculations performed under both USL values are referred to in this document and the modeling assumptions required to meet the final USL are discussed as applicable. The resulting modeled scenarios are shown to be compliant with the final USL of 0.96.

4.2.2 MCNP6.2

Calculations supporting Revision 6 and later revisions of this NCSE were performed using MCNP6.2 [16] on a personal computer. The MCNP6.2 computer code was run under the allowed Microsoft® platforms as described in WIPP-073, *MCNP 6.2 Software Quality Assurance Plan (SQAP)* [25] using the precompiled version of MCNP6.2 supplied by the vendor (Los Alamos National Laboratory). The Evaluated Neutron Data File VIII.0 cross-section library (LA-UR-20-30460, *Guide for Using ENDF/B-VIII.0 Nuclear Data with MCNP* [26]) was used for all cases performed with MCNP6.2.

MCNP6.2 was validated for use at WIPP in WIPP-078, *MCNP 6.2 Validation Report for Criticality Calculations at the Waste Isolation Pilot Plant* [27] in accordance with ANSI/ANS-8.24-2017, *Validation of Neutron Transport Methods for Nuclear Criticality Safety Calculations* [28]. The USL for thermal

^{239}Pu systems at the WIPP is 0.9659. This USL includes an administrative margin of 0.02. The area of applicability established in WIPP-078 includes polyethylene and water moderation and reflection by salt, MgO, concrete, beryllium, lead, steel, and water such that the systems modeled in this NCSE are within the area of applicability of the MCNP6.2 validation. Thus, the USL of 0.9659 can be used with no additional reductions or penalties.

5.0 Process Analysis

Because of the different container types, package contents, and disposal configurations at the WIPP facility, waste storage, handling, and disposal involve numerous criticality computations to evaluate the many combinations of container configurations that are possible. In this section, bounding configurations for the receipt, temporary storage in the WHB (above ground), transfer to the underground in the conveyance, and permanent disposal of CH waste containers in the underground repository are evaluated. To simplify the analyses and to ensure a conservative bound is placed on the multitude of waste container storage, handling, and disposal configurations, this NCSE considers two bounding geometric configurations: an infinite array configuration with reflection conditions representative of the salt repository and a two-container model where the fissile masses are close to one another and the containers are surrounded by an infinitely thick reflector. These configurations were modeled in MCNP5. The geometry of the waste payloads, underground array and two-container models are described in Section 5.1, the material compositions used in the models are given in Section 5.2 and the container array and two-container model results are summarized in Sections 5.3 and 5.4, respectively.

5.1 Geometry

The contents of the various allowed loadings, as modeled in MCNP5, are summarized below with respect to the container type. Further details are given in the appendices for the specific waste type being analyzed.

5.1.1 Direct-loaded 55-gallon Drums Containing Less Than or Equal to 1 Weight Percent Special Reflectors

The direct loaded 55-gallon drums are modeled with up to 200 fissile gram equivalents (FGE), modeled as 200 grams of ^{239}Pu mixed with a polyethylene-water moderator, which is 25% by volume polyethylene and 75% by volume water. The seven-pack of drums contains three 200 FGE drums and one 50 FGE drum, as shown in Figure A-1 in Appendix A, for a total of 650 FGE in the pack. This mass exceeds the 325 FGE limit for payload in the HalfPACT [3] and TRUPACT-II [2] shipping containers by a factor of two and thus is very conservative. A mixture of polyethylene and special reflector material fills the remainder of the drum reflecting the fissile mass. The special reflector material is modeled as beryllium based on the evaluation in SAIC-1322-001, *Reactivity Effects of Moderator and Reflector Materials on a Finite Plutonium System* [17], which found beryllium to be the most reactive reflector material at infinite thickness for a polyethylene-water moderated ^{239}Pu system. Polyethylene is modeled up to a maximum packing fraction of 25% as determined by physical testing to bound the packing fraction of direct loaded (non-machine compacted) waste per Section 6.2.1 of the TRUPACT-II SAR [2]. The amount of beryllium is based on 1 wt% of the maximum gross container loading limit of 1,000 pounds [5] or 4.54 kilograms, which is rounded up to 5 kilograms of beryllium per 55-gallon drum. The beryllium is modeled as homogeneously mixed throughout the polyethylene reflector. The beryllium density varies slightly with the hydrogen-to-plutonium (H/Pu) ratio as the fuel volume changes but is approximately 0.024 g/cm^3 in the 55-gallon drum. Note that beryllium is slightly more reactive modeled in the reflector than in the moderator as discussed in Section 6.4.3.2.2 of the TRUPACT-II SAR [2].

The 55-gallon drum dimensions given in Table 2-1 are used in the MCNP5 models. The drum walls are carbon steel (ASTM A 569), which is modeled with the composition from ASTM A 569 [9] as given in Table 5-5. The theoretical density of carbon steel is 7.86 g/cm^3, but is modeled at 50% of this value, or 3.93 g/cm^3, to allow for fabrication tolerances, localized wall thinning or other degradation. Thin layers of steel act as a neutron poison due to the high neutron absorption cross-sections of the material so modeling less steel than is present is conservative and increases reactivity. Section 2.1.2 of the CH-TRAMPAC [5] requires that the integrity of the container be visually inspected prior to transport to ensure there is no significant rusting such that the 50% value is conservative.

The 55-gallon drum is the only drum size modeled because it bounds the 85-gallon and 100-gallon drums from a criticality safety perspective. The 85- and 100-gallon drums have a larger diameter and thus the fissile material in these drums is spaced further apart than in the 55-gallon drums, which reduces reactivity. Thus, the fissile mass limits for 55-gallon drums are applicable to 85-gallon and 100-gallon drums containing the same waste type.

5.1.2 Direct-loaded Shielded Containers with Less Than or Equal to 1 Weight Percent Special Reflectors

The shielded containers are modeled with the same waste loading as discussed above for the 55-gallon drums, namely 200 fissile gram equivalents (FGE) in the 25% polyethylene and 75% water moderator with 3 kilograms of beryllium (1 wt% of net payload) in the remainder of the container. The shielded container dimensions are given in Table 2-5 for the most reactive shielded container design and the dimensions for the other designs are given in Section H.1 of Appendix H. The shielded container walls are carbon steel lining a lead wall, modeled per Table 5-6. The shielded containers have a thick steel lid and bottom, with some designs also incorporating lead in the lid or bottom for added shielding. In the shielded container, the steel wall sandwiching the lead and the thick steel lid and bottom are modeled at the theoretical density of 7.86 g/cm^3, which was shown in scoping studies to maximize reactivity due to its thickness (i.e., thick steel acts as a neutron reflector instead of a neutron absorber).

5.1.3 Direct-loaded SWB Containing Less Than or Equal to 1 Weight Percent Special Reflectors

The direct-loaded SWB FGE is modeled with a mixed polyethylene-water moderator, which is 25% by volume polyethylene and 75% by volume water. The TRUPACT-II SAR [2] allows 325 grams ^{239}Pu with no ^{240}Pu credited, 340 grams ^{239}Pu with 5 grams ^{240}Pu, 360 grams ^{239}Pu with 15 grams ^{240}Pu, and 380 grams ^{239}Pu with 25 grams ^{240}Pu. The ^{239}Pu mass is a maximum value whereas the ^{240}Pu mass is a minimum value in each case. A mixture of beryllium and polyethylene fills the remainder of the SWB reflecting the fissile mass. Polyethylene is modeled up to a maximum packing fraction of 25% as determined to bound the packing fraction of direct-loaded (non-machine compacted) waste in the TRUPACT-II SAR [2]. The amount of beryllium is based on 1 wt% of the maximum container gross weight of 4,000 pounds [5], which equates to 18.14 kilograms of beryllium per SWB. The beryllium is modeled as homogeneously mixed throughout the polyethylene reflector. The beryllium density varies slightly with the H/Pu ratio as the fuel volume changes but is approximately 0.0095 g/cm^3. Note that beryllium is slightly more reactive modeled in the reflector than in the moderator as discussed in Section 6.4.3.2.2 of the TRUPACT-II SAR [2].

The SWB dimensions given in Table 2-3 are used in the MCNP5 model. The carbon steel container wall is modeled at full thickness, but the carbon steel is only modeled at 50% of the theoretical density, or 3.93 g/cm^3, to allow for fabrication tolerances, localized wall thinning or other degradation, etc. The composition of carbon steel from ASTM A 569 [9] used in the models is given later in Table 5-5.

5.1.4 Direct-loaded SLB2 Containing Less Than or Equal to 1 Weight Percent Special Reflectors

The SLB2 is a large box designed for transport in the TRUPACT-III shipping container. The SLB2 dimensions given in Table 2-4 are used in the MCNP model. The maximum gross weight of an SLB2 is 10,500 pounds per the TRUPACT-III SAR [4]) where the beryllium mass at the 1 wt% limit is 47.7 kilograms. The beryllium is modeled as homogeneously mixed throughout the polyethylene reflector. The beryllium density varies slightly with the H/Pu ratio as the fuel volume changes but is approximately 0.0064 g/cm^3.

The FGE limits from the TRUPACT-III SAR [4], namely 325 grams ^{239}Pu with no ^{240}Pu credited, 340 grams ^{239}Pu with 5 grams ^{240}Pu, 360 grams ^{239}Pu with 15 grams ^{240}Pu, and 380 grams ^{239}Pu with 25 grams ^{240}Pu, were used to evaluate the effect of the SLB2 on waste handling, storage, and disposal configurations at WIPP. The ^{239}Pu mass is a maximum value whereas the ^{240}Pu mass is a minimum value in each case. These FGE limits are the same as the FGE limits for the SWB and the density of the 1 wt% beryllium is higher in the SWB so the SWB is often used to bound the SLB2. Also, the SWB is smaller in size and this yields a more conservative array.

5.1.5 Direct-loaded 55-gallon Drums Containing Greater Than 1 Weight Percent Special Reflectors

Special reflector materials are those materials that provide better reflection than the 25% polyethylene, 75% water mixture evaluated as the worst case reflector for direct-loaded waste with ≤ 1 wt% special reflectors. Drums with large quantities of these materials may not be subcritical unless a smaller FGE limit is imposed. Special reflector materials and the minimum quantity of concern are defined in Section 6.2.1 of the TRUPACT-II [2] and HalfPACT [3] SARs and Section 6.2.2 of the TRUPACT-II SAR [4], and payloads shipped to WIPP that are considered to contain > 1 wt% special reflector materials, must meet the limits in Table 9-1 for waste with > 1 wt% special reflector materials for disposal. (Because the containers evaluated herein are shipped to WIPP in these transportation packages, the SAR information is not repeated in this NCSE.) In this NCSE, the special reflector material is modeled as beryllium, which has been shown to result in the highest reactivity when reflecting a plutonium system in unlimited quantity in SAIC-1322-001 [17]. For these drums, the beryllium may be in large metal pieces or may be present in particulate form, thus the beryllium is modeled as either a moderator or a reflector. When beryllium is modeled as a reflector, the plutonium is moderated by 25% by volume polyethylene and 75% by volume water surrounded by beryllium conservatively modeled at 70% of its theoretical density. Reflection by 100% dense beryllium, although bounding, is not possible in these waste drums per LA-UR-04-0857, *Review of Special Reflectors in the TRU Waste Inventory* [29]. Because the beryllium consists of molds, shapes, chunks, coarse particles, and fines randomly filling the waste container instead of being specifically constructed to surround the fissile material and fill the container with no void, beryllium at 70% of theoretical density or 1.295 g/cm^3 is used given that the maximum theoretical density for randomly packed uniform spheres is 70% (“Recursive packing of dense particle mixtures” [30]; “Is random packing of spheres well defined?” [31]). When modeled as a moderator, the plutonium is homogeneously mixed with the beryllium and the beryllium-to-plutonium (Be/Pu) ratio in the mixture is varied to find the maximum reactivity.

The high beryllium content is only modeled explicitly in 55-gallon drums. As discussed in Section 5.1.1, the 55-gallon drum bounds the 85-gallon and 100-gallon drums from a criticality safety perspective. The 85- and 100-gallon drums have a larger diameter and thus the fissile material in these drums is spaced further apart than in the 55-gallon drums, which reduces reactivity. Thus, the limits for 55-gallon drums are applicable to 85-gallon and 100-gallon drums containing the same waste type.

5.1.6 Fully Compacted Waste in 100-gallon Drums

This configuration evaluates the contents as fully compacted and the non-fissile material in the drum, modeled as polyethylene, reaches theoretical density. Thus, the fissile mass is moderated with 100% dense polyethylene. The drums are modeled with two fissile limits. The first limit of 170 grams of ^{239}Pu does not credit any difference in the internal and external dimension when the drums are stacked. The second higher fissile mass is 200 grams of ^{239}Pu and only applies when the design of the container lid and bottom that provides inherent spacing between the internal contents of two stacked drums is credited. With both limits, the fissile mass is reflected by a 100% dense mixture of beryllium and polyethylene. The beryllium content in the reflector mixture is 5 kilograms, which slightly exceeds 1 percent by weight of the rated 1,000 pounds weight capacity of the drum [5]. The beryllium is modeled as homogeneously mixed throughout the polyethylene reflector. The 100-gallon drum is modeled with the dimensions given in Table 2-2 and the steel drum wall is modeled with the composition given in Table 5-5 at 50% density to allow for degradation.

5.1.7 Partially Compacted Waste in 100-gallon Drums

Because 100% compaction may be overly conservative with regard to the compaction that can physically be achieved, limits are also determined based on 70% compaction. This scenario is also evaluated in the TRUPACT-II SAR [2] and will require the waste generator to control the compaction process. The fissile mass in this model consists of 200 grams of ^{239}Pu moderated with a polyethylene-water mixture, which is 70% by volume polyethylene and 30% by volume water. This fissile mixture is consistent with the approved TRUPACT-II contents model used in the criticality safety analysis for partially compacted waste. Reflection of the fissile mass with a 70% dense mixture of 5 kilograms of beryllium and polyethylene is modeled. This reflector composition bounds controlled machine compaction operations. As with the fully compacted case, the beryllium is modeled as homogeneously mixed throughout the polyethylene reflector. The 100-gallon drum is modeled with the dimensions given in Table 2-1 and the steel drum wall is modeled with the composition given in Table 5-5 at 50% density to allow for degradation.

5.1.8 Fully Compacted Waste Direct Loaded in a Standard Waste Box

In an SWB, only full compaction is considered. Thus, moderation of the fissile mass is modeled with 100% dense polyethylene and the fissile mass is reflected with a 100% dense mixture of beryllium and polyethylene. The fissile mass consists of 200 grams of ^{239}Pu. The beryllium content in the reflector mixture is 18.14 kilograms, which represents 1% by weight of the rated weight capacity of the SWB, and is consistent with the TRUPACT-II SAR contents model for fully compacted waste [2]. The 18.14 kilograms of beryllium is homogeneously distributed throughout the polyethylene filling the container. The SWB is modeled with the dimensions given in Table 2-3 and the SWB wall is modeled at 60% density to allow for degradation with the composition given in Table 5-5.

5.1.9 Fully Compacted Waste in Shielded Containers

The shielded containers of compacted waste are modeled with 200 FGE moderated by 100% dense polyethylene with 3 kilograms of beryllium in 100% dense polyethylene filling the remainder of the container. The container geometry and materials are modeled as discussed in Section 5.1.2.

5.1.10 Pipe Overpacks in 55-gallon Drums containing Less Than or Equal to 1 Weight Percent Special Reflectors

The unshielded 12-inch pipe overpack assembly is modeled to bound all pipe overpack configurations. Because the unshielded 12-inch pipe overpack assembly design allows for less dunnage and, therefore, greater interaction between drums, this is considered conservative. Furthermore, the larger pipe diameter allows for a more favorable fissile material geometry over that of the smaller 6-inch pipe overpack. The cane fiberboard used in the pipe overpack assemblies as shock absorbing dunnage is represented by cellulose ($C_6H_{10}O_5$) at a density of 0.2248 g/cm^3.

5.1.11 Pipe Overpacks in 55-gallon Drums Containing Greater Than 1 Weight Percent Special Reflectors

The 12-inch pipe overpack model described in Section 5.1.10 is also used for the pipe overpacks containing high quantities of special reflectors. The special reflector material is again modeled as beryllium. The beryllium mass is unlimited and it fills the pipe volume around the fissile material.

5.1.12 CCOs containing Less Than or Equal to 1 Weight Percent Special Reflectors

The CCO is modeled as waste directly loaded into a CCC, constructed of a 6-inch pipe, and placed inside of a 55-gallon drum. The fissile mass consists of 380 grams of ^{239}Pu homogenously mixed with a mixture of 75% water and 25% polyethylene. A 1.6 kilogram solid mass of beryllium is also modeled inside the CCC and represents 1 wt% of the gross weight limit of the CCO [5]. The plywood dunnage plates are represented by cellulose ($C_6H_{10}O_5$) at a density of 0.387 g/cm^3.

A CCO may also contain machine compacted waste provided the plastic content is limited to 2,000 grams. As shown in Section G.4, this mass is less than the polyethylene modeled in non-compacted waste and thus such waste is bounded by the analysis of non-compacted waste evaluated with a moderating mixture of 25% by volume polyethylene and 75% by volume water.

5.1.13 Infinite Array Model Details

The underground repository array is modeled as a stack of containers in a hexagonal arrangement that is infinitely reflected on the six vertical faces to simulate a tight-packed, infinite array in x and y. The bottom of the stack is reflected with nominally 10 feet of salt modeled at 300 centimeters and the top of the stack is reflected by nominally 2 feet modeled at 62.23 centimeters of MgO backed by 300 centimeters of salt. The MgO represents the supersack placed on top of each stack and the salt thickness provides infinite reflection. (MgO between the containers would reduce the interaction between containers and thus reduce the reactivity of the array; reflection by MgO is considered in the two-container model as discussed in Section 5.1.14 to bound supersacks placed amongst the containers or a spill of MgO from a supersack.) The stack represents three tiers of drum assemblies or SWBs. The SLB2 and TDOP heights only allow one tier to be stacked on top but these arrays are not explicitly modeled because they are bounded by the SWB array. Waste container configurations are emplaced on a hexagonal lattice unit with pitch characteristics typical of a seven-pack of 55-gallon drums. The disposal configuration is based on typical disposal area dimensions that accommodate the stacked waste and required airflow within an active waste emplacement room.

Fissile masses are located in the center of the container in the infinite array model. In this centralized configuration, the fissile units are equal distance to all other fissile units in the array. With random

placement of the fissile unit in each container, the average center-to-center separation in either the horizontal or vertical direction will be statistically the same as that of the array with all fissile masses centered in the containers, because as two fissile masses are brought closer together, those masses become further separated from the fissile material in other containers. The two-container model discussed in the next section evaluates the credible extent of localized areas of high fissile concentration.

5.1.14 Two-Container Model Details

The two-container models used in this evaluation consider the different container types and approved loadings that could be stacked on top of one another in a bounding configuration. Whereas the fissile material is centered in each container in the array model, the two-container model considers worst-case fissile placement for maximum interaction between the two containers. The fissile mass in the lower container is located at the top of the container, while the fissile mass in the upper container is located at the bottom of the container. The fissile mass units form a cylinder with an optimum height-to-diameter (H/D) ratio of 1 and a total mass of 2 times that allowed per container.

Worst-case reflection conditions that may occur during storage, handling, and disposal are also considered in the two-container model. The stack of two containers is tightly reflected by 300 centimeters of either concrete, MgO, or salt to provide infinite reflection. The concrete is modeled to represent above-ground handling and storage in concrete buildings; the MgO represents close reflection by the MgO supersacks in the underground repository and the salt represents the salt walls. Thus, the two-container model ensures subcriticality for a localized configuration of concentrated fissile material due to close proximity under full reflection conditions.

The placement of a two-container stack into the infinite array model is evaluated in Section C.5 of Appendix C. The system reactivity is statistically equivalent to the tightly reflected two-drum model results. Thus, the two-container model provides the worst-case, credible model for localized high fissile concentration. (See Sections 5.3.2 and 5.4 for further discussion.) Thus, the subcritical results for both the infinite array models and the two-containers models under normal and credible abnormal conditions ensure that a criticality accident at the WIPP due to the storage, handling, and disposal of CH waste containers is not credible.

5.2 Material Compositions

The material compositions used in the MCNP models are summarized in this section.

5.2.1 Fissile Waste Mixture

The majority of the fissile material to be disposed of at the WIPP is ^{239}Pu and is the only fissile component considered in the analysis. Other fissile isotopes are allowed at the WIPP, but all are reported as equivalent grams of ^{239}Pu known as FGE. The moderator component of the fissile mixture used in the criticality analyses is dependent on waste category. In summary, the moderating material in fully compacted waste streams consists of pure polyethylene. For partially compacted waste, the moderator is modeled as a polyethylene-water mixture, which is 70% by volume polyethylene and 30% by volume water. For all other non-compacted waste streams, the moderator is modeled as a mixture of polyethylene and water, which is 25% by volume polyethylene and 75% by volume water.

For calculations with MCNP5, the ^{239}Pu density used in determining source mixtures is 19.848 g/cm^3 (*Handbook of Chemistry and Physics* [32] and *Standard Composition Library* [33]) for alpha-phase plutonium metal with a molecular weight of 239.05 (*Nuclides and Isotopes* [34] and [35]). Polyethylene is

modeled at its theoretical density of 0.923 g/cm^3 or 0.93 g/cm^3 (both values for 100% dense polyethylene given in the *Standard Composition Library* [33]).

Calculations performed using MCNP6.2 utilized the following densities and molecular weights. The ^{239}Pu density used in determining source mixtures is 19.84 g/cm^3 with a molecular weight of 239.0522 (*Nuclides and Isotopes* [35]). The theoretical densities for polyethylene, water, and beryllium are 0.92 g/cm^3, 0.9982 g/cm^3, and 1.85 g/cm^3, respectively (*SCALE 6.3.3 User's Manual* [36]) and the elemental atomic weights were taken from the same reference.

through Table 5-4 tabulate the fissile mass mixture compositions as a function of H/Pu ratio over the optimum range for the compacted and direct-loaded (non-compacted) waste categories used in this NCSE.

Table 5-1. Mixture Parameters for Fully Compacted Waste Versus Hydrogen/Plutonium Ratio

H/Pu Ratio	^{239}Pu Conc. (g/L)	Mixture density (g/cm^3)	Wt.% H	Wt.% C		Wt.% Pu
^{239}Pu Mixed with 100% By Volume Polyethylene (MCNP5)						
700	44.8428	0.9658	13.7045	81.6522		4.6433
750	41.8596	0.9629	13.7471	81.9057		4.3472
800	39.2485	0.9604	13.7845	82.1289		4.0866
850	36.9441	0.9582	13.8178	82.3268		3.8555
900	34.8953	0.9563	13.8474	82.5035		3.6491
950	33.0617	0.9545	13.8741	82.6623		3.4637
1000	31.4112	0.9529	13.8981	82.8057		3.2962
1050	29.9177	0.9515	13.9200	82.9358		3.1442
1100	28.5598	0.9502	13.9399	83.0545		3.0056
^{239}Pu Mixed with 100% By Volume Polyethylene (MCNP6.2)						
600	52.1276	0.9697	13.5988	80.0870	0.93862	5.3756
700	44.6975	0.9626	13.7041	80.7068	0.94589	4.6433
800	39.1214	0.9573	13.7841	81.1779	0.95141	4.0866
900	34.7822	0.9532	13.8469	81.5482	0.95575	3.6491
1000	31.3094	0.9499	13.8977	81.8469	0.95925	3.2962
1100	28.4672	0.9471	13.9394	82.0929	0.96213	3.0056
1200	26.0981	0.9449	13.9744	82.2990	0.96455	2.7620
1300	24.0930	0.9430	14.0042	82.4742	0.96660	2.5550
1400	22.3740	0.9413	14.0298	82.6250	0.96837	2.3768
1500	20.8839	0.9399	14.0521	82.7561	0.96991	2.2219

Table 5-2. Mixture Parameters for Partially Compacted Waste Versus Hydrogen/Plutonium Ratio (MCNP6.2)

H/Pu Ratio	^{239}Pu Conc. (g/L)	Mixture Density (g/cm^3)	Wt.% H	Wt.% O	Wt.% C-12	Wt.% C-13	Wt.% Pu
^{239}Pu Mixed with 70% By Volume Polyethylene and 30% By Volume H_2O							
600	49.7062	0.9908	12.6911	26.7748	54.8742	0.64313	5.0168
700	42.6205	0.9841	12.7827	26.9681	55.2703	0.64777	4.3311
800	37.3030	0.9790	12.8523	27.1149	55.5711	0.65130	3.8104
900	33.1651	0.9750	12.9069	27.2302	55.8074	0.65407	3.4014
1000	29.8536	0.9719	12.9510	27.3231	55.9979	0.65630	3.0717
1100	27.1434	0.9693	12.9872	27.3996	56.1547	0.65814	2.8003
1200	24.8843	0.9672	13.0176	27.4637	56.2860	0.65968	2.5729
1300	22.9723	0.9653	13.0434	27.5182	56.3977	0.66098	2.3797
1400	21.3332	0.9638	13.0657	27.5651	56.4937	0.66211	2.2135
1500	19.9124	0.9624	13.0850	27.6058	56.5772	0.66309	2.0690

Table 5-3. Mixture Parameters for Direct-loaded, Non-compacted Waste Versus Hydrogen/Plutonium Ratio and ^{240}Pu Content (MCNP5)

H/Pu Ratio	^{239}Pu Conc. (g/L)	Mixture Density (g/cm^3)	Wt.% H	Wt.% O	Wt.% C	Wt.% ^{239}Pu	Wt.% ^{240}Pu
325 FGE Mixed with 25% By Volume Polyethylene and 75% By Volume H_2O, 0 g ^{240}Pu							
800	34.614	1.0123	11.5331	65.5653	19.4823	3.4193	0
900	30.774	1.0087	11.5771	65.8153	19.5566	3.0509	0
1000	27.699	1.0057	11.6125	66.0167	19.6165	2.7542	0
1100	25.184	1.0033	11.6417	66.1824	19.6657	2.5101	0
1200	23.088	1.0014	11.6661	66.3212	19.7070	2.3058	0
1300	25.184	0.9997	11.6868	66.4390	19.7420	2.1322	0
1400	23.088	0.9982	11.7046	66.5403	19.7721	1.9829	0
340 FGE Mixed with 25% By Volume Polyethylene and 75% By Volume H_2O and 5 g ^{240}Pu							
800	34.613	1.0128	11.5273	65.5323	19.4726	3.4175	0.0503
900	30.773	1.0091	11.5719	65.7858	19.5479	3.0496	0.0448
1000	27.700	1.0061	11.6078	65.9900	19.6085	2.7531	0.0405
1100	25.185	1.0037	11.6374	66.1580	19.6585	2.5092	0.0369
1200	23.089	1.0017	11.6621	66.2987	19.7003	2.3050	0.0339
1300	21.315	1.0000	11.6832	66.4182	19.7358	2.1315	0.0313
1400	19.794	0.9985	11.7012	66.5210	19.7663	1.9823	0.0292

Table 5-3. Mixture Parameters for Direct-loaded, Non-compacted Waste Versus Hydrogen/Plutonium Ratio and ^{240}Pu Content (MCNP5)

H/Pu Ratio	^{239}Pu Conc. (g/L)	Mixture Density (g/cm^3)	Wt.% H	Wt.% O	Wt.% C	Wt.% ^{239}Pu	Wt.% ^{240}Pu
360 FGE Mixed with 25% By Volume Polyethylene and 75% By Volume H_2O with 15 g ^{240}Pu							
800	34.611	1.0137	11.5167	65.4720	19.4546	3.4144	0.1423
900	30.771	1.0099	11.5624	65.7318	19.5318	3.0471	0.1270
1000	27.699	1.0068	11.5992	65.9411	19.5940	2.7511	0.1146
1100	25.184	1.0043	11.6295	66.1133	19.6452	2.5075	0.1045
1200	23.088	1.0023	11.6549	66.2575	19.6880	2.3036	0.0960
1300	21.314	1.0005	11.6764	66.3800	19.7244	2.1303	0.0888
1400	19.793	0.9990	11.6950	66.4854	19.7558	1.9813	0.0826
380 FGE Mixed with 25% By Volume Polyethylene and 75% By Volume H_2O with 25 g ^{240}Pu							
800	34.609	1.0145	11.5072	65.4181	19.4386	3.4116	0.2244
900	30.770	1.0106	11.5539	65.6835	19.5175	3.0448	0.2003
1000	27.698	1.0075	11.5915	65.8973	19.5810	2.7493	0.1809
1100	25.183	1.0049	11.6225	66.0733	19.6333	2.5060	0.1649
1200	23.087	1.0028	11.6484	66.2207	19.6771	2.3023	0.1515
1300	21.313	1.0010	11.6704	66.3459	19.7143	2.1292	0.1401
1400	19.793	0.9995	11.6894	66.4537	19.7463	1.9803	0.1303

Table 5-4. Mixture Parameters for Direct-loaded, Non-Compacted Waste Versus Hydrogen/Plutonium Ratio in CCOs (MCNP5)

H/Pu	^{239}Pu Conc. (g/L)	Mixture Density (g/cm^3)	Wt.% H	Wt.% O	Wt.% C	Wt.% Pu
380 FGE Mixed with 25% By Volume Polyethylene and 75% By Volume H_2O						
500	55.543	1.0328	11.2947	64.3117	19.0156	5.3779
600	46.308	1.0240	11.3968	64.8934	19.1876	4.5221
700	39.706	1.0177	11.4709	65.3153	19.3124	3.9013
800	34.751	1.0130	11.5272	65.6354	19.4070	3.4304
900	30.896	1.0094	11.5713	65.8866	19.4813	3.0609

5.2.2 Reflector Material in Waste Container

The reflector material around the fissile mixture used in the criticality analyses was varied to maximize reactivity of the two-container model or the array model. The reflector compositions modeled to meet this objective are discussed in the applicable appendix for the waste type analyzed. For waste types limited to less than or equal to 1 wt% of special reflector materials, beryllium at 1% of the maximum weight loading of the container is spread through the reflector region.

5.2.3 Container Materials of Construction

U.S. Department of Transportation 17C and 17H specifications require only that the drums be constructed of low carbon or stainless steel (304L), while the 100-gallon drum and the SWB are constructed of ASTM A 569 [9] low carbon steel. Other low carbon steels, such as ASTM A516 and A1011 are used in the shielded containers. Scoping studies have shown that differences between modeling the wall as 304L versus ASTM A 569 does not have a statistically significant effect on the MCNP result. All drum structural components are modeled with ASTM A 569 low carbon steel (*Handbook of Chemistry and Physics* [32]) at a density of 50% of nominal. In a few cases, 60% density was used as noted in the case description. Because the WIPP repository is situated in a series of thick salt beds, the environment could cause a degradation of the steel drum wall over long periods of time. If credit is taken for the nominal drum wall thickness (i.e., nominal wall density) in the analyses, the wall thickness becomes a controlled parameter. To avoid imposing controls on the thickness and nature of the drum walls, a reduced density of 50 to 60% of nominal is assumed in all criticality safety calculations. The shielded container, however, is an exception where all steel is modeled as ASTM A 569 at theoretical density; the higher density results in a higher reactivity due to the thickness of the lid and bottom and the contiguous lead reflector in the wall. As another conservatism, no credit was taken for the additional steel layers of the compacted waste pucks (see Figure 2-9) as the thickness of the steel in the compacted puck is uncontrolled and difficult to quantify. The specification for ASTM A 569 low carbon steel modeled is given in Table 5-5. Due to the differences in isotopic abundances used in the MCNP6.2 validation, input values for both MCNP5 and MCNP6.2 are given.

Table 5-5. Material Composition for ASTM A 569 Low Carbon Steel

Element/ Isotope	Wt. Fraction	MCNP5 Library Specification	MCNP5 Wt. Fraction	MCNP6.2 Library Specification	MCNP6.2 Wt. Fraction
Density 7.86 g/cm^3					
C	0.0015	6000.60c	0.0015	6012.00c	1.4830E-03
				6013.00c	1.7000E-05
P	0.00035	15031.60c	0.00035	15031.00c	3.5000E-04
S	0.0004	16000.60c	0.0004	16032.00c	3.7861E-04
				16033.00c	3.1258E-06
				16034.00c	1.8178E-05
				16035.00c	8.9732E-08
Mn	0.006	25055.60c	0.006	25055.00c	6.0000E-03
Fe	0.99175	26054.60c	0.058513	26054.00c	5.5990E-02
		26056.60c	0.90963	26056.00c	9.1143E-01
		26057.60c	0.020827	26057.00c	2.1425E-02
		26058.60c	0.0027769	26058.00c	2.9013E-03

The lead in the shielded containers is modeled at its theoretical density of 11.344 g/cm^3. Lead consists of four naturally occurring isotopes: ^{204}Pb, ^{206}Pb, ^{207}Pb, and ^{208}Pb, at the abundances given in Table 5-6.

Table 5-6. Material Composition for Lead

Element/ Isotope	MCNP6.2 Library Specification	Natural Atom Fraction
Density 11.344 g/cm^3		
^{204}Pb	82204.00c	0.014
^{206}Pb	82206.00c	0.241
^{207}Pb	82207.00c	0.221
^{208}Pb	82208.00c	0.524

5.2.4 Reflector Material Outside the Waste Container

To simulate the waste storage, handling, and disposal configurations at WIPP, three different reflectors are used to bound the waste container configurations: concrete, MgO, and salt. Ordinary concrete, at a density of 2.35 g/cm^3 from *Handbook of Health Physics and Radiological Health* [37], is used in MCNP5 models as one of the reflecting materials for the two-container models to bound above-ground temporary storage. The composition of this concrete is summarized in Table 5-7. Cases executed using MCNP6.2 use the material Ordinary Concrete (NBS 04) from PNNL-15870, Rev. 2, *Compendium of Material Composition Data for Radiation Transport Modeling* [38], which also has a density of 2.35 g/cm^3. This composition is similar to that used in prior revisions but with an expanded isotopic breakdown. The composition is summarized in Table 5-8.

Salt is used as a reflector for the underground array models. Salt is taken as NaCl with a density of 2.165 g/cm^3 with the atomic weights of sodium and chloride being 22.9898 and 35.4527, respectively [32]. Including the MgO on top of the waste stacks in the model has been shown to increase the reactivity. The specification for the MgO backfill in DOE/WIPP-07-3372, *Waste Isolation Pilot Plant Documented Safety Analysis* (DSA), Chapter 2 [39] states that the supersack containing the MgO is a hexagon nominally 155 centimeters (61 inches) across the flats and 64.8 centimeters (25.5 inches) high. The minimum density of MgO is given as 1.39 ± 0.08 g/cm^3 (87 ± 5 pounds/ft^3). A single supersack is filled with either 1,361 ± 22.7 kilograms (3,000 ± 50 pounds) or 1,905 ± 22.7 kilograms (4200 ± 50 pounds) MgO. The MgO is modeled as a continuous layer 62.23 centimeters high at a density of 1.45 g/cm^3 based on a previous version of the specification. At this density and thickness, a hexagon 155 centimeters across the flats would hold 1,881.7 kilograms of MgO. Thus the modeled MgO mass is slightly less than the largest mass loading but this will have a minimal effect on reactivity as salt is modeled above the MgO at a thickness that is infinite for neutrons. In addition, racks of MgO supersacks may also be placed amongst the waste containers in the underground array or MgO may spill from the supersacks. Thus, full reflection of the two-container model by MgO is considered to bound these conditions. Also, by modeling full reflection by MgO, any future change in the MgO super-sack configuration is bounded. The two-container model is also fully reflected by salt to bound reflection by the salt walls and the possibility of salt falling between containers.

Table 5-7. Material Composition for Concrete (MCNP5)

Element/ Isotope	MCNP5 Library Specification	Wt. Fraction	Element/ Isotope	MCNP5 Library Specification	Wt. Fraction
Density 2.35 g/cm^3					
H	1001.60c	0.0056	K	19000.60c	0.0192
O	8016.60c	0.4981	Ca	20000.60c	0.0829
Na	11023.60c	0.0171	^{54}Fe	26054.60c	0.000725
Mg	12000.60c	0.0026	^{56}Fe	26056.60c	0.011377
Al	13027.60c	0.0457	^{57}Fe	26057.60c	0.000263
Si	14000.60c	0.3151	^{58}Fe	26058.60c	0.000035
S	16000.60c	0.0013	–	–	–

Table 5-8. Material Composition for Concrete (MCNP6.2)

Element/ Isotope	MCNP6.2 Library Specification	Wt. Fraction	Element/ Isotope	MCNP6.2 Library Specification	Wt. Fraction
Density 2.35 g/cm^3					
^{1}H	1001.00C	5.5580E-03	^{32}S	16032.00C	1.2144E-03
^{16}O	8016.00C	4.9808E-01	^{33}S	16033.00C	1.0026E-05
^{23}Na	11023.00C	1.7101E-02	^{36}S	16036.00C	2.8782E-07
^{24}Mg	12024.00C	1.9994E-03	^{40}Ca	20040.00C	8.0172E-02
^{25}Mg	12025.00C	2.6368E-04	^{42}Ca	20042.00C	5.6181E-04
^{26}Mg	12026.00C	3.0190E-04	^{43}Ca	20043.00C	1.2002E-04
^{27}Al	13027.00C	4.5746E-02	^{44}Ca	20044.00C	1.8975E-03
^{28}Si	14028.00C	2.8949E-01	^{46}Ca	20046.00C	3.8040E-06
^{29}Si	14029.00C	1.5225E-02	^{48}Ca	20048.00C	1.8557E-04
^{30}Si	14030.00C	1.0382E-02	^{54}Fe	26054.00C	6.9994E-04
^{39}K	19039.00C	1.7880E-02	^{56}Fe	26056.00C	1.1394E-02
^{40}K	19040.00C	2.3008E-06	^{57}Fe	26057.00C	2.6784E-04
^{41}K	19041.00C	1.3565E-03	^{58}Fe	26058.00C	3.6270E-05

5.3 Container Array Results

5.3.1 Baseline Disposal Array Calculations

Calculations were performed to determine the reactivity effect due to the interaction of multiple containers in the underground repository as described in Section 5.1.13. A sample array model is represented in Figure 5-1 for illustration. The array calculations for each container type are discussed in more detail in the appendices of this NCSE.

The baseline array reactivity results, as summarized in Table 5-9, show that the array reactivity is quite low. The evaluation of non-compacted waste in seven-packs of 55-gallon drums bounds four-packs of 85-

gallon drums and three-packs of 100-gallon drums as these smaller packs have increased spacing between them and adjacent containers in the array. The 100-gallon drum three-pack was explicitly modeled containing machine-compacted waste and the array reactivity was slightly lower than the seven-pack array of 55-gallon drums containing the same waste type. The three-packs were modeled in a tight-packed lattice, which is conservative compared to the layout that would occur with other waste containers present that have a larger footprint as shown in Figure 2-4. Also, the larger diameter of the 100-gallon drum allows more internal reflection of the fissile material from the compacted waste, which has a smaller effect for non-compacted waste as the array is most reactive with the internal reflector region of the drum voided. Disposal of machine-compacted waste in 85-gallon drums is bounded by the evaluations of smaller 55-gallon drums and larger 100-gallon drums, which account for both the tighter packing of the array and the larger internal reflector volume in the drum. The taller TDOP containers are bounded by the SWB analysis, as the SWBs stack three high, whereas a single TDOP is approximately the height of two SWBs but has the same FGE limit. Although the shielded containers will be emplaced in three, two, or single container configurations, a seven-pack array was modeled as it is conservative and does not adversely affect the FGE loading limit. Consequently, this model accounts for areas where two three-packs of shielded containers could be placed next to one another.

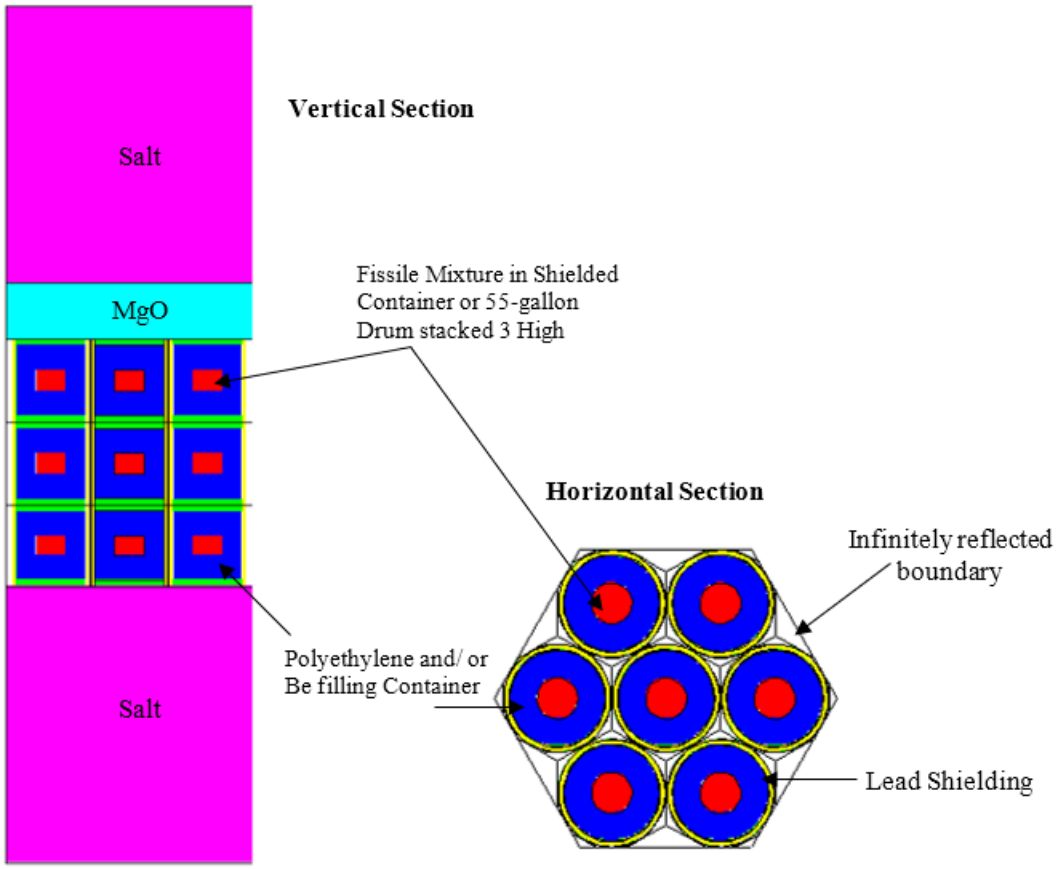


Figure 5-1. Sample Array Model Layout showing Shielded Containers

Table 5-9. Summary of Underground Array Calculation Results

Container Type	Applicable Appendix Section	Container FGE Limit	Pack FGE Limit[a]	Maximum $k_{eff} + 2\sigma$
Direct-loaded Waste Containing ≤ 1 wt% Special Reflectors				
55-gallon drums (which bound 85- and 100-gallon drums)	A.2.1	200	650	0.90096
Shielded containers SC-30G1	H.2.1	200	N/A	0.90677
Shielded containers SC-30G2	H.2.1	200	N/A	0.86968
Shielded containers SC-30G3	H.2.1	200	N/A	0.81128
Shielded containers SC-55G1	H.2.1	200	N/A	0.76692
Shielded containers SC-55G2	H.2.1	200	N/A	0.78240
Pipe overpacks in 55-gallon drums [c]	D.2.1	200	N/A	0.89471
SWBs (which bound TDOPs and SLB2s)	A.2.2	325 with 0 g ^{240}Pu 340 with 5 g ^{240}Pu 360 with 15 g ^{240}Pu 380 with 25 g ^{240}Pu	N/A	0.86759 0.87487 0.87889 0.88393
CCOs	G.2.1	380	N/A	0.94545
Direct-loaded Waste Containing > 1 wt% Special Reflectors				
55-gallon drums (which bound 85- and 100-gallon drums)	B.2.1	100 + 100 kg Be	N/A	0.89169
SWBs (which bound TDOPs)	B.2.2	100	N/A	0.80815
Pipe overpacks in 55-gallon drums [c]	D.2.1	140	N/A	0.93050
Machine-compacted Waste Containing ≤ 1 wt% Special Reflectors				
100-gallon drums [b]	C.2.1	200	600	0.86166
55-gallon drums [b]	C.2.2	200	600	0.86230
Shielded containers SC-30G1	H.2.1	200	N/A	0.86235
Shielded containers SC-30G2	H.2.1	200	N/A	0.86225
Shielded containers SC-30G3	H.2.1	200	N/A	0.86226
Shielded containers SC-55G1	H.2.1	200	N/A	0.86173
Shielded containers SC-55G2	H.2.1	200	N/A	0.86168
SWBs (which bound TDOPs)	C.2.3	200	N/A	0.86162
Pipe overpacks in 55-gallon drum [c]	D.2.1	200	N/A	0.89471

(a) Pack is defined as a seven-pack of 55-gallon drums, pipe overpacks or CCOs, a four-pack of 85-gallon drums, a three-pack of 100-gallon drums. All containers marked N/A are only limited by the container FGE limit.

(b) Note that in the array model, compacted waste drums are subcritical at 200 FGE/drum without requirements on compaction density or design spacing.

(c) Note that in the normal condition array model, pipe overpacks are subcritical when moderated and reflected by full density polyethylene, representative of machine compacted waste, with no limit on polyethylene content This was the only configuration modeled since it bounds direct-loaded waste.

To determine the effect of lead reflection from the shielded containers on other non-shielded waste containers in a mixed array, an array with shielded containers around 55-gallon drums was also modeled as shown in Figure 5-2. The outer hexagonal surface around the shielded containers is infinitely reflected to model an infinite array. As before, the fissile mass is modeled as a cylinder located in the center of each drum or container and the containers are stacked three tiers high with MgO and salt reflection. As discussed in Section H.2.2, the presence of shielded containers of non-compacted or machine compacted waste in the array slightly reduces reactivity from the 55-gallon drum array as the lead reduces interaction between containers.

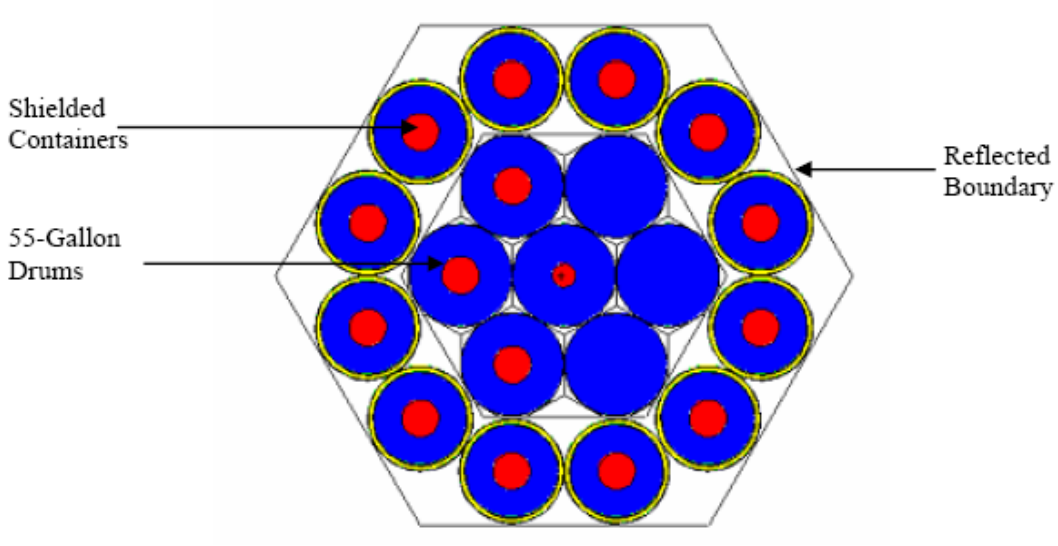


Figure 5-2. Drum Array with Shielded Containers, X-Y Plane

5.3.2 Conservatisms in Baseline Disposal Array Calculations

Conservatisms in this NCSE include not only modeling the base array at greater than or equal to the transportation package fissile limit for each waste assembly in the array, but also include:

- taking no credit for slipsheets between waste assemblies;
- taking credit for only part of the metal (which acts as a poison) in the waste containers;
- configuring the fissile material as ^{239}Pu in a concentrated, optimally moderated geometry as opposed to being distributed through the waste container;
- configuring the fissile material as ^{239}Pu in an optimally moderated geometry when free liquid is prohibited in the waste containers in both the shipping container SARs and DOE/WIPP-02-3122, *Transuranic Waste Acceptance Criteria for the Waste Isolation Pilot Plant* (WIPP WAC) [40];
- modeling beryllium at higher densities than would be considered realistic in debris waste.

Additional calculations were performed for machine-compacted waste to study a revised base-case condition in the underground repository array using more realistic models. The details of these calculations are documented in Addendum 1 to SAIC-1171-001, *Nuclear Criticality Safety Evaluation for*

Storage of Machine Compacted Transuranic Waste Products at the Waste Isolation Pilot Plant [41] and are summarized below.

Machine-compacted waste drums are analyzed at two compaction densities: 100% compaction and 70% dense compaction (see Appendix C). These densities were chosen to correspond to the polyethylene densities evaluated in the criticality analyses for shipment of compacted waste in a TRUPACT-II or HalfPACT shipping container. Addendum 1 to SAIC-1171-001 [41] determined a limit of 170 FGE per drum of fully compacted waste and 200 FGE per drum for 70% dense compacted waste. These limits were based on analysis that evaluated the fissile material in optimized cylinders for the two-container model and spheres for the array models. These models, while bounding, can be viewed as unnecessarily conservative. The fissile content of waste proposed for compaction, in general, is low and in the form of contamination, dust, metal oxide, etc., such that it has low density. The underground repository array was found to be significantly less reactive than the two-drum model such that there are no density restrictions on polyethylene for compacted waste in the array case, and the three-pack or seven-pack assembly limit is 600 FGE. In reality, each drum assembly is limited to a maximum of 325 FGE, which is the FGE limit in the HalfPACT and TRUPACT-II shipping containers used to transport waste to the WIPP. This further reduces the reactivity in the storage or disposal configurations at WIPP, as shown in the following sections. A comparison of the baseline array results and the more realistic model results is given in Table 5-10.

The more realistic models were considered in supplemental calculations. In one set of calculations, the geometric arrangement of the mass within the drums remains consistent with the array model discussed in Section 5.3.1 (i.e., fissile material is concentrated in a fissile cylinder at optimum H/Pu ratio), but the fissile mass of the three-pack of 100-gallon drums was reduced to the TRUPACT-II limit of 325 FGE. The mass in each drum was varied keeping the three-pack at less than or equal to 325 FGE and the maximum reactivity calculated was 0.8352.

Variations on the geometric configuration of the fissile mass were also evaluated to study the reactivity reduction if the ^{239}Pu is homogeneously distributed throughout the drums in two manners: (1) mixed homogeneously with beryllium and polyethylene and spread uniformly throughout the volume of the drum, or (2) configured as more realistic compacted pucks with the plutonium, beryllium, and polyethylene uniformly distributed in a single compacted puck drum. Other conservatisms are also removed from the base array model such that 100% of the steel wall is modeled, the slipsheets between layers of containers are added, the design separation provided by the rolling hoops on drums is credited and the exterior height of the drum is increased to include the band clamp, and 3 wt% ^{240}Pu is modeled with the ^{239}Pu. The system eigenvalue is significantly reduced as shown in Table 5-10. Overbatched cases were also modeled in this configuration by modeling an extra 200 FGE 100-gallon drum in the middle tier. For 55-gallon drums, the middle tier contains extra 200 FGE and 125 FGE drums for a total seven-pack mass of 650 FGE. Even with these significant overbatches, the array reactivity remains below 0.4.

The largest reduction in k_{eff} comes from homogenizing the fissile material throughout the drum. A homogeneous distribution of the fissile material is ordinarily not a conservative representation, but may be a more reasonable base-case representation for debris TRU waste. While localized hot spots can occur, it is unlikely that the hot spots will be as severe as the bounding cases presented in Table 5-9. Modeling the fissile material concentrated in a cylinder mixed with the right amount of polyethylene to create optimum moderation is not realistic, but is conservative.

Table 5-10. Comparison of Baseline Array and Realistic Array Results for Machine-Compacted Waste

Case	Maximum Container FGE Limit	Pack FGE Limit[a]	Maximum $k_{eff} + 2\sigma$
Baseline Array Results[a] (MCNP6.2)			
100-gallon drums	200	600	0.86166
55-gallon drums	200	600	0.86230
More Realistic Model Results[b] (MCNP5)			
FGE in 3-packs of 100-gallon drums reduced to TRUPACT-II shipping limit	170	325	0.8352
Fissile material spread throughout drums	200 + 6 g ^{240}Pu	325 + 9.75 g ^{240}Pu	100 gal - 0.2885 55 gal - 0.3463
Fissile material spread throughout 100-gallon drums with middle tier overbatched	200 + 6 g ^{240}Pu	325 + 9.75 g ^{240}Pu 525 in middle tier	0.3158
Fissile material spread throughout 55-gallon drums with middle tier overbatched	200 + 6 g ^{240}Pu	325 + 9.75 g ^{240}Pu 650 in middle tier	0.3828
Fissile material in 1 cylindrical puck representing a machine-compacted drum in the larger drum	200 + 6 g ^{240}Pu	325 + 9.75 g ^{240}Pu	100 gal - 0.3736 55 gal - 0.4937

(a) From Table 5-9.

(b) From Addendum 1 to SAIC-1171-001 [41].

5.4 Two-Container Model Results

The array model evaluates the fissile contents centered in each waste container representing average fissile spacing based on the random nature of the waste. However, although highly unlikely, it is possible that the fissile material could be placed closer together in two adjacent containers. The two-container model, as described in Section 5.1.14, was created to evaluate this possibility. A sample two-container model with SWBs is represented in Figure 5-3. The two-container calculations for each container type are discussed in more detail in the appendices.

As expected, the two-container results are much higher than the array reactivity results for some container types as shown by the results in Table 5-11. Note that the taller TDOP container is bounded by the SWB analysis, as both containers have the same FGE limit.

As discussed in the appendices, the cases performed with MCNP5 originally had a USL of 0.97. Later an administrative margin of 0.01 was included in the USL, which reduced the value to 0.96. Newer cases were performed with MCNP6.2, which has a USL of 0.9659 per Section 4.2.2. Table 5-11 summarizes the results of modeling to determine the spacing between the fissile contents in the two containers that reduces the $k_{eff} + 2\sigma$ value below the applicable USL. These calculations are discussed in detail in the appendix for the appropriate container loading. The separation needed in all cases is no greater than 1.5 centimeters (0.4 inches). This separation will easily be achieved in reality and it is not credible for multiple instances of the two-container configuration to be present nearby in a container array for the following reasons:

- The container is not likely to be completely filled to the lid and if it is full when loaded, settling is likely to occur during transportation and handling such that some gap will exist.

- The fissile material is not likely to remain at the top of the container of non-compacted waste due to its high density and gravity effects.

- In compacted waste drums, all of the fissile mass must be in the uppermost compacted puck drum in the bottom drum and all of the fissile mass must be in the lowermost compacted puck drum in the upper drum. The steel of the compacted drum, which has not been included in the model, is likely to provide some spacing and the neutron absorbing steel of the puck drum will also reduce reactivity. Also, although compaction of the drum concentrates the fissile material, the volume of the optimally moderated fissile material (approximately 5 L at 200 FGE) is <10% of the volume of the puck drum (assuming 4 puck drums per 100-gallon drum); as such the laws of entropy do not support creating an optimal Pu mixture during compaction.

- The drums provide more spacing inherent in the design of the lid and bottom than has been modeled.

- Full and even loading to the top of an SWB, TDOP, or SLB2 is highly unlikely due to its large volume.

- Also, the fissile material in the two stacked containers must be perfectly positioned in x and y such that it is directly above/below the fissile material in the other container. The probability of this occurring in two drums is very low and decreases for the larger SWB, TDOP, or SLB2 containers.

The placement of a two-drum model of compacted waste into the infinite array model is evaluated in Section C.5 of Appendix C. Because the three-high stack of drums was infinitely reflected, this model results in two adjacent 2-drum configurations. The system reactivity is statistically equivalent to the tightly reflected two-drum model results. Thus, the two-container model provides the worst-case, credible model for localized high fissile concentration. Combinations of two different container types have also been evaluated in the two-container model configuration. The details and results of these calculations are given in Appendix E. As expected, placing two different containers together results in an effective "averaging" of the reactivity of the two containers, and has a lower reactivity than the model with the most reactive containers of the same type.

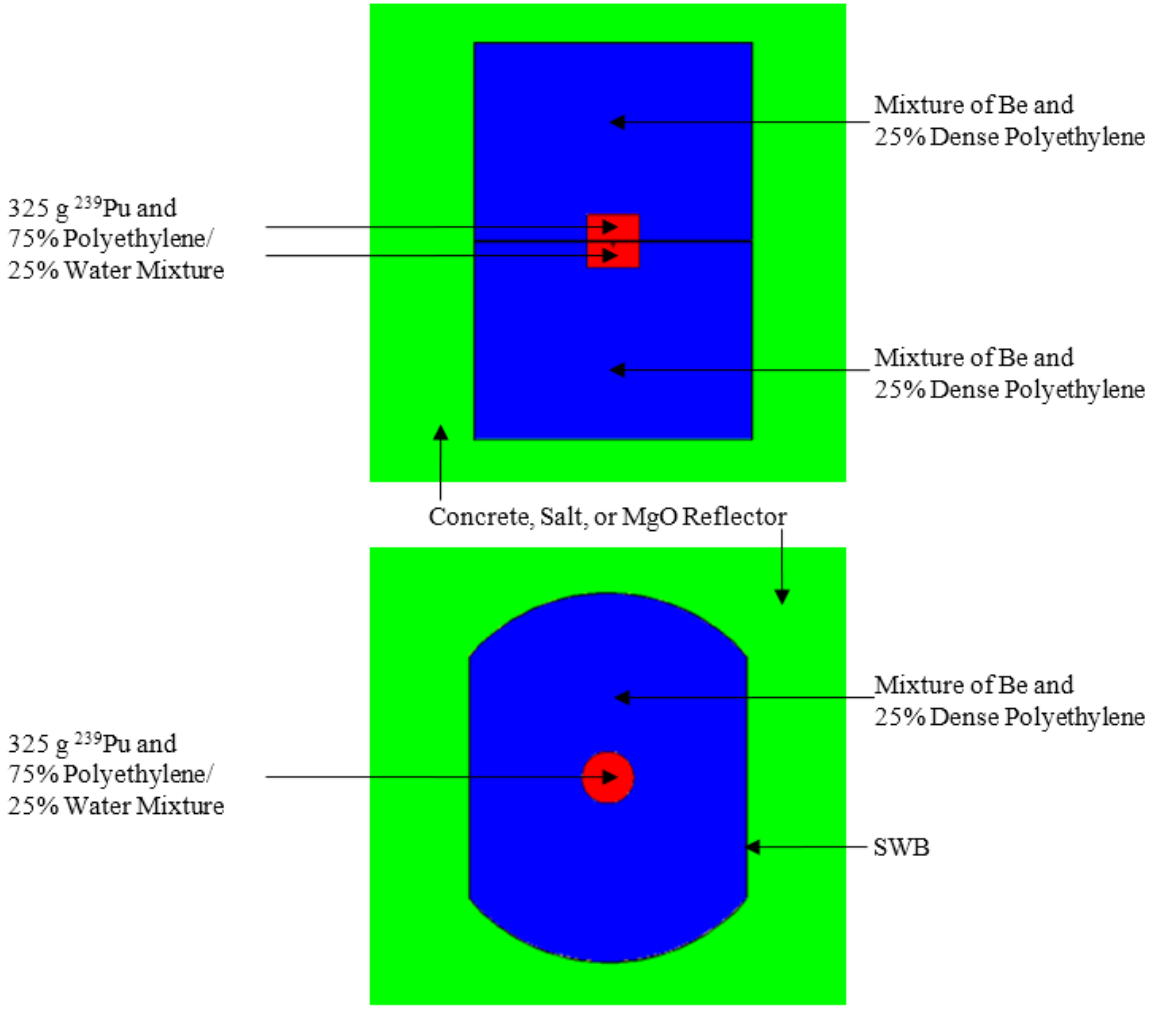


Figure 5-3. Sample Two-Container Model Layout with the SWB

Table 5-11. Summary of Two-Container Calculation Results

Container Type	Applicable Appendix Section	Container FGE Limit	Maximum $k_{eff} + 2\sigma$	Non-Credited Separation Included in Model (cm)
Direct-loaded Waste Containing ≤ 1 wt% Special Reflectors				
55-gallon drums (which bound 85- and 100-gallon drums)	A.3.1	200	0.88622	0
SWBs (bounds TDOPs)	A.3.2	325 with 0 g ^{240}Pu 340 with 5 g ^{240}Pu 360 with 15 g ^{240}Pu 380 with 25 g ^{240}Pu	0.95295 0.95618 0.95697 0.95805	1.25
SLB2 with an SWB (SLB2s not stacked)	A.3.3	325 with 0 g ^{240}Pu 340 with 5 g ^{240}Pu 360 with 15 g ^{240}Pu 380 with 25 g ^{240}Pu	0.95117 0.95415 0.95422 0.95649	0
Shielded containers	H.2.3	200	0.76200 (b)	0
Pipe overpacks in 55-gallon drums (a)	D.2.2	200	0.81136	0
CCOs	G.2.2	380	0.7255	0
Direct-loaded Waste Containing > 1 wt% Special Reflectors				
55-gallon drums (which bound 85- and 100-gallon drums)	B.3.1	100 + 100 kg Be	0.92707	0
SWBs (bounds TDOPs)	B.3.2	100	0.92098	0
Pipe overpacks in 55-gallon drums (a)	D.2.2	140	0.87029	0
Machine-compacted Waste				
100-gallon drums without design spacing	C.3.1	170	0.95696 (b)	0
100-gallon drums with design spacing	C.3.1	200	0.92859 (b)	0
Partially compacted 100-gallon drums	C.3.2	200	0.95673 (b)	0
55-gallon drums without design spacing	C.3.3	170	0.96145 (b)	0
55-gallon drums with design spacing	C.3.3	200	0.95476 (b)	0
Partially compacted 55-gallon drums	C.3.3	200	0.96168 (b)	0
Shielded containers	H.2.3	200	0.87335 (b)	0
Direct-loaded SWBs (bound TDOPs)	C.4.1	200	0.96279 (b)	1
Pipe overpacks in 55-gallon drums (a)	D.2.2	200	0.81136	0

(a) Note that in the normal condition two-container model, pipe overpacks are subcritical when moderated and reflected by full density polyethylene, representative of machine compacted waste, with no limit on polyethylene content. This was the only configuration modeled since it bounds direct-loaded waste.

(b) This case was run in MCNP6.2, which has a USL of 0.9659. The other cases in the table were run with MCNP5, which has a USL of 0.96.

5.5 Overpacking Configurations

As per Section 2.2, nine different container types are currently approved for disposal of CH waste at the WIPP and include 55-gallon drums, 85-gallon drums, 100-gallon drums, SWBs, TDOPs, SLB2s, CCOs, pipe overpacks and shielded containers. If during or after receipt by the WIPP any of these containers are identified as damaged, the container may be placed inside another intact container so long as the appropriate limits are satisfied. For example, as shown in Table 5-12, based on the container dimensions, a 55-gallon drum could be overpacked in an 85-gallon drum, 100-gallon drum, SWB, TDOP, or SLB2. Table 5-13 summarizes the potential overpack combinations based on geometry.

Table 5-12. Summary of Approximate Container Dimensions

Container	Approximate Dimensions
55-gallon drum	R=29 cm; h=85 cm
85-gallon drum	R=38 cm; h=89 cm (short) R=36 cm; h=102 cm (tall)
100-gallon drum	R=38 cm; h=86 cm
SWB	L=175 cm; W=132 cm; h=93 cm
TDOP	R=90 cm; h=186 cm
SLB2	L=265 cm; W=165 cm; h=168 cm
Shielded Container	Varies (refer to Appendix H)

Table 5-13. Container Overpack Matrix

Container	Potential Overpack Container						
	55-gallon drum	85-gallon drum	100-gallon drum	SWB	TDOP	SLB2	Shielded Container
55-gallon drum	NO	YES	YES	YES	YES	YES	NO
85-gallon drum	NO	NO	NO	YES	YES	YES	NO
100-gallon drum	NO	NO	NO	YES	YES	YES	NO
SWB	NO	NO	NO	NO	YES	YES	NO
TDOP	NO	NO	NO	NO	NO	NO	NO
SLB2	NO	NO	NO	NO	NO	NO	NO
Shielded Container	NO	YES	YES	YES	YES	YES	NO
POC	NO	YES	YES	YES	YES	YES	NO
CCO	NO	YES	YES	YES	YES	YES	NO

Review of Table 5-12 shows that some overpack containers have sufficient volume for multiple damaged containers. Therefore, all overpacking configurations shall first be designated as either “one-to-one” or “multiple-to-one” as discussed in the following sections.

5.5.1 One-to-One Overpacking

Under the one-to-one designation, a single smaller container is overpacked into a single larger container and the appropriate mass limit(s) of the **smaller** container shall apply. FGE limits are based on the characterized content WIPP WAC [40], which provides confidence in tracking the amount of FGE. In addition, no loose material is allowed in the overpacking (i.e., larger) container around the overpacked (i.e., smaller) container. This methodology simply increases the spacing around the smaller container, therefore making it less reactive with adjacent containers than was previously analyzed. For example, consider a non-compacted > 1 wt% special reflector damaged pipe overpack assembly containing 140 FGE overpacked in a 100-gallon drum. Even though the pipe overpack exceeds the limit for a non-compacted mass with > 1 wt% special reflector in the 100-gallon drum, the pipe overpack is now in a container with a larger footprint and thus is less reactive than the evaluated condition. Thus the one-to-one overpack configuration is acceptable.

5.5.2 Multiple-to-One Overpacking

Under the multiple-to-one designation, two (or more) smaller containers could potentially be loaded into a single larger container. Consequently, multiple-to-one overpacking only applies to the SWB, TDOP, and SLB2 containers. The TDOP, as the name implies, has sufficient volume for ten 55-gallon drums. While this is advantageous for storage efficiency, if based on geometry alone, an overpacking container could also be potentially loaded with excessive payloads. For example, if ten damaged 55-gallon drums each meeting the 55-gallon drum direct loaded with ≤ 1 wt% special reflector limit of 200 FGE were loaded into a TDOP, the total FGE would be 2000 FGE and more than six times the TDOP limit of 325 FGE (or more than five times the 380 FGE limit with 25 grams of ^{240}Pu).

In order to prevent a situation like a TDOP with ten 200 FGE 55-gallon drums as described above, the appropriate mass limit(s) of the **larger** overpacking container shall apply to the multiple-to-one overpacking container. As with the one-to-one designation, FGE limits are based on the characterized content provided by the waste generator. The overpacking container will be entered into the WWIS database that tracks all containers in the underground. The WWIS has error checking capabilities, which will provide confidence that the FGE limit is met. In addition, no loose material is allowed in the overpacking (i.e., larger) container around the overpacked (i.e., smaller) containers. Uncontainerized fissile material is not readily available at WIPP to add to container as all fissile material remains in the drum or larger container it was shipped in. This methodology effectively divides the mass within the larger container compared to a single mass, thereby making it less reactive than was analyzed. For example, consider again ten damaged direct loaded (with ≤ 1 wt% special reflector) 55-gallon drums totaling 325 FGE overpacked in a TDOP. Not only will additional spacing reduce the reactivity of the system as previously discussed, since the bounding analysis is based on a single 325 FGE mass and the greatest mass in a 55-gallon drum is 200 FGE, the most reactive configuration would be if one drum contained 200 FGE and another single adjacent drum contained 125 FGE. This would still divide the fissile mass and reduce the reactivity of the system compared to the single previously analyzed mass of 325 FGE in a TDOP. Therefore, any configuration of overpacked containers totaling less than 325 FGE would be acceptable.

6.0 Parameters

The following parameters are controlled for criticality safety of CH waste containers at the WIPP. The contingent events resulting from the loss of each controlled parameter are also given below. The contingent events flow from the hazard evaluation tables given in Appendix F. These upsets are evaluated in detail in Section 7.0.

6.1 Mass

Fissile mass limits are required to maintain the reactivity below the USL; thus mass is controlled. As a contingent condition, an overload to 150% of the mass limit is modeled in one container per stack in the underground array and the stack infinitely reflected.

6.2 Geometry

The geometry of the fissile region is not controlled. The fissile region is modeled as a sphere or as a cylinder at an H/D ratio of 1. These two geometries minimize neutron leakage and present a worst-case condition.

6.3 Moderation

Even though free liquids are not allowed in the waste containers per the HalfPACT and TRUPACT-II SARs [3], [2] or the WIPP WAC [40], optimum moderation of the fissile region was modeled with polyethylene and water varying the H/Pu ratio to determine the most reactive state. Within the container but outside of the fissile region, moderation is shown to reduce reactivity per Section 7.6. Exterior to the container, interstitial moderation is modeled to represent sprinkler activation or flooding as a contingency event in Section 7.5. Thus, moderation is not controlled.

6.4 Interaction

Interaction is controlled in that the underground repository array is limited to containers stacked three tiers high, where a drum or SWB occupies one tier and a TDOP or SLB2 occupies two tiers. The above-ground array is bounded by the underground array and is also limited to three tiers high for criticality safety (although it is restricted to two tiers high for other reasons). Interaction between containers is not controlled as they are modeled in contact with one another.

Interaction is also controlled by the container, which determines the distance between fissile masses. Containers approved for transportation to WIPP in the TRUPACT-II, HalfPACT, or TRUPACT-III are evaluated. The 55-, 85-, 100-gallon drums, SWBs, TDOPs, SLB2s, CCOs, shielded containers, and pipe overpack configurations described in the DSA [39] are approved for disposal at WIPP. Containers are modeled in contact with one another in an infinite array. Typically, the bottom of one container is placed on top of another with only the thickness of the lid or bottom modeled and any recesses ignored. In some cases, mass limits are also given based on crediting some portion of the inherent vertical spacing between drum contents afforded by the design of the recess in the bottom or lid of a drum or spacers that may be placed within the drum to maintain the credited spacing, such that geometry is controlled. This vertical design spacing was only credited in the two-container model where the worst-case fissile mass locations are modeled by concentrating the fissile material in the top of the lower drum and the bottom of the upper drum to maximize interaction. The vertical spacing is ignored in the more realistic array model. Thus, the loss of the design spacing has been modeled in the normal condition array and is not further evaluated.

Four loss of interaction control contingencies are evaluated: (1) dropping containers from the waste hoist in Section 7.1, (2) overstacking the entire array to four tiers high in Section 7.2, (3) underground roof falling resulting in container compaction in Section 7.3, and (4) crushing of the containers on the waste array face as a result of impact by the 41-ton forklift in Section 7.7.

6.5 Neutron Absorption

The only neutron absorber modeled is the steel of the container. The wall, lid, and bottom of each container type were modeled at full thickness but the steel was modeled at 50-60% of its theoretical value. Section 2.1.2 of the CH-TRAMPAC [5] requires that the integrity of the payload container shall be visually inspected prior to transport to ensure that payload container is in good and unimpaired conditions (e.g., no significant rusting and is of sound structural integrity), where modeling 50-60% of the steel in the wall is conservative. Thus, neutron absorption is controlled by the transportation requirement. No credible contingency event was identified that would damage more than 50-60% of the wall thickness over a significant surface area. Therefore, upsets in this parameter are bounded by the normal condition using only 50-60% of the steel wall thickness. Note that in the shielded container, the thick steel and/or lead act as reflectors and thus, are modeled at theoretical density.

6.6 Reflection

6.6.1 Internal Container Reflection

Mass limits on special reflector materials, namely beryllium, within the container are required to maintain system reactivity below the USL. Unless specifically evaluated, special reflector materials are limited to less than or equal to 1 wt% of the payload. Mass limits were set for containers with this restriction in Appendix A. An upset condition of exceeding the beryllium restriction was modeled by placing twice as much beryllium in one or more container per stack. A high beryllium content payload with up to 100 kilograms of beryllium in drums was also evaluated in Appendix B. The corresponding upset condition evaluated one container per stack filled with beryllium as the worst-case credible condition.

Another restriction on internal container reflection occurs in the compacted waste payload. Mass limits were evaluated with 100% polyethylene around the fissile material (100% theoretical packing) and with a maximum of 70% polyethylene, based on a generator site restricting their compaction accordingly. This reduction in compaction was only modeled in the two-container models. The higher mass limit with 100% dense polyethylene is modeled in the more realistic array model, such that the upset event has been modeled in the normal condition array and is not further evaluated.

6.6.2 External Container Reflection

The external reflection is modeled conservatively compared to actual conditions and is not controlled. In the underground repository, the modeled array is infinite in the x and y directions and reflected by 300-centimeter-thick salt on the top and bottom. The MgO supersack is modeled as a continuous layer of theoretical density MgO directly on top of the container array and the salt modeled directly on top of that. Scoping calculations confirmed that including the MgO has a significant positive effect on reactivity and modeling it as a continuous layer instead of discrete supersacks on top of individual containers provides conservatism. In the two-container model, the reflectors that the containers may come in contact with (concrete, MgO, and salt), are modeled tight fitting around the containers at infinite thickness. This configuration is considerably more reactive than the actual condition where the container may be in a corner of a concrete hot cell or salt panel. This tight-fitting reflector around the two-container model also simulates interstitial salt or MgO that could be present between waste containers in the event of a roof fall during the operational phase of a disposal room or panel.

6.7 Volume

Volume is not credited in any of the analysis and is not controlled.

6.8 Enrichment

Enrichment is not controlled. All fissile material is modeled as ^{239}Pu, which is conservative as there are always other less reactive isotopes present with ^{239}Pu including ^{240}Pu, a strong neutron absorber. There are higher mass limits that credit the ^{240}Pu content for the SWB, TDOP, or SLB2 but the waste generator must confirm that ^{240}Pu content is present in the package. Also, the largest FGE limit of 380 is 17% greater than the 325 FGE limit without ^{240}Pu. Thus, an upset where the ^{240}Pu content is not met is bounded by the 50% FGE overbatch upset evaluated in Section 7.4.1. Uranium-235 and ^{233}U can be shipped under these limits using FGE as defined in the CH-TRAMPAC [5]. The FGE values account for the differences in minimum critical mass between ^{239}Pu and these isotopes.

6.9 Concentration

Concentration is not controlled. The fissile concentration was unrestricted and optimized by varying the H/Pu ratio and consequently the plutonium concentration in the fissile region.

7.0 Contingency Evaluation

Credible abnormal conditions that could occur during waste storage, handling, and disposal of CH waste containers at the WIPP are assessed in this section. Appendix F contains a hazard evaluation to identify the conditions that could lead to a loss of the controlled parameters from Section 6.0. Because of the conservatism in the models used, no contingencies are considered for variations in packing fraction, container wall thickness, reflector parameters, or fissile moderation parameters because the analyses in Section 5.0 along with its subsections determined the worst credible cases for these parameters. The limits and controls needed to render the postulated contingent conditions unlikely are presented in Section 9.0.

The contingency evaluation is based on perturbations of the worst-case normal or nominal configuration infinite array models described in Section 5.3.1. The two-container models are sufficiently conservative to bound any contingency of more realistic or expected conditions involving interaction between small numbers of containers. The array models consider each drum assembly at a fissile loading over 500 FGE, which is greater than the current TRUPACT-II or HalfPACT fissile limit of 325 FGE. The contingencies evaluated in this section are applied to the array models with the fissile material centered in each container. With random placement of the fissile unit in each container, the average center-to-center separation in either the horizontal or vertical direction will be statistically the same as that of the array with all fissile masses centered in the containers.

7.1 Loss of Confinement of Fissile Material

The bounding CH event that results in a loss of confinement is the unlikely failure of the waste hoist such that the CH containers are breached when the load falls down the waste shaft into the waste shaft sump. However, the failure of the waste hoist has been evaluated in the DSA [39] to be beyond extremely unlikely due to the robust design of the waste hoist with redundant brakes and six ropes.

7.2 Exceeding Disposal Array Vertical Stacking Limit

7.2.1 Exceeding Array Vertical Stacking Limit in the Underground Repository

By design, the WIPP panels are mined to a ceiling height that will accommodate up to the nominal height of three 55- or 100-gallon drums or three SWBs. This configuration allows adequate space for the MgO supersack to be placed on top of the waste column and still allow adequate space for the airflow rate

required by the HWFP [1]. Waste handling procedures at WIPP administratively control waste stacks in the disposal array to be stacked no greater than the equivalent of three drum assemblies or three SWBs. However, ground control activities to ensure mine safety have resulted in areas of the disposal rooms being mined to a height greater than 13 feet, such that it is possible to stack greater than three tiers high and emplace the MgO on top of the stack.

To determine the impact on the disposal array reactivity if an overstacking event occurred in the repository, a fourth tier of containers is added to the following arrays:

1. Direct-loaded 55-gallon drums containing less than or equal to 1 wt% special reflectors as described in Section A.2.1;

2. Direct-loaded 55-gallon drums containing greater than 1 wt% special reflectors as described in Section B.2.1;

3. Direct-loaded shielded containers containing less than 1 wt% special reflectors as described in Section H.2.1;

4. 100-gallon drums of fully compacted waste as described in Section C.2.2;

5. 12-inch unshielded pipe overpack assemblies as described in Section D.2.1; and

6. CCO assemblies as described in Section G.2.1.

The SLB2 is not analyzed stacked two high as the fissile material would be significantly separated in the tall containers plus there is significant spacing between containers provided by the forklift pockets. The results of the base array and the overstacked array are compared in Table 7-1. A larger reactivity increase over the three-tier array is seen for non-compacted waste than for compacted waste as the higher polyethylene density in the compacted waste acts to isolate the fissile material in the various tiers. The cases with high special reflector content also exhibit a large increase for the four-tier array as the array model considers the plutonium spread through the beryllium at the optimum Be/Pu ratio of 20,000. If the 100 kilograms of beryllium in each drum were modeled purely as a reflector around the fissile material, as in the SWB model with high special reflector content, it would isolate the fissile material in the tiers from one another and little increase would be seen as demonstrated in the compacted waste results. All results are below the documented MCNP USL(s) except for the loading with high beryllium content. That result exceeds 0.96 but is less than 0.97, which is the USL without the administrative margin. Overstacking of the entire array without noticing the error, while at the same time placing the MgO supersack on top of the fourth tier, would require multiple operator errors. Also, although areas of disposal rooms have been mined to a height greater than 13 feet, the entire disposal panel being mined to a height that allows room to create an infinite four-tier array with MgO is unlikely. As such, a four-tier array of drums containing 100 FGE and 100 kilograms of beryllium was modeled without the MgO supersack but with the drums in contact with the salt ceiling. As shown in Table 7-1, the $k_{eff} + 2\sigma$ value is less than 0.89. The four-tier drum array height is 11.1 feet without the MgO supersack and 13.15 feet with the supersack emplaced on top of the drums. Based on the significant reduction in reactivity without the supersack on top of the array and the small clearance between the worst-case mining height and the four-tier array with MgO, it is not considered credible to create an infinite overstacked array that would result in a critical configuration. In addition, note that each drum in the array is modeled at the FGE limit (whereas the average FGE per drum currently emplaced in the underground is significantly lower than the limit). As this upset remains subcritical and the loss of other controlled parameters, such as mass, would require a concurrent and

independent change in process conditions, the double contingency principle is met. See Section 7.10 for the evaluation of concurrent upsets to justify that a criticality accident is not credible.

Table 7-1. Evaluation of Stacking Containers Four-tiers High in the Underground Repository

Container and Waste Loading	Array Height	$k_{eff} + 2\sigma$	Filename (Section)
55-gallon drums of direct-loaded waste with ≤ 1 wt% special reflectors	3 tiers	0.90096	dac0026 (A.2.1)
	4 tiers	0.94913	dac4h22 (A.4.1)
55-gallon drums of direct-loaded waste with > 1 wt% special reflectors	3 tiers	0.89169	a20kb (B.2.1)
	4 tiers with MgO	0.96628[(a)]	a420kb (B.3.3)
	4 tiers without MgO	0.88973[(b)]	a420kbm (B.3.3)
Shielded containers of direct-loaded waste with ≤1 wt% special reflectors	3 tiers	0.90677	SC30G1a10nprn (H.2.1)
	4 tiers	0.92609	SC30G1f10n (H.3.1)
Shielded container of fully compacted waste	3 tiers	0.86235	SC30G1a10MC (H.2.1)
	4 tiers	0.86217	SC30G1f09MC (H.3.1)
100-gallon drums of fully compacted waste	3 tiers	0.86166	aray118 (C.2.1)
	4 tiers	0.86174	aray420 (C.6.1)
Pipe overpacks in 55-gallon drums with ≤ 1 wt% special reflectors with machine compacted waste [(c)]	3 tiers	0.89471	pa20018pf (D.2.1)
	4 tiers	0.89480	pa20098pf (D.3.1)
Pipe overpacks in 55-gallon drums with > 1 wt% special reflectors [(c)]	3 tiers	0.93050	pa14016pf (D.2.1)
	4 tiers	0.93204	pa14094pf (D.3.1)
CCOs	3 tiers	0.94545	hx800mgo380fge (G.2.1)
	4 tiers	0.95898	u4ts750hx380fge (G.3.1)

(a) WIPP-099, *Extent of Condition Review for WIPP-016, Rev. 7* [42] re-evaluated this scenario with MCNP6.2 and the result was below the USL. Result given is from MCNP5 calculation.

(b) Modeled with the MgO supersack removed from the infinite four-tier high array in MCNP5.

(c) Note that in the normal condition array model, pipe overpacks are subcritical when moderated and reflected by full density polyethylene, representative of machine compacted waste, with no limit on polyethylene content. This was the only configuration modeled since it bounds direct-loaded waste.

7.2.2 Exceeding Interim Drum Storage Array Stacking Limit

Waste containers may be stored above ground while awaiting processing and/or transport to the underground facility. Stacking in above-ground storage arrays is administratively limited to the height of two containers. Waste containers are required to be stored on facility pallets in the WHB. The load limit of the facility pallet is such that drums/SWBs will not be stacked higher than two containers. Up to four CH drum assemblies or SWBs are stored on a pallet. Only two TDOPs are stored on a pallet. The pallet will accommodate only one SLB2 and only two packs of three or less of shielded containers based on pallet limitations. Overstacking on the surface is unlikely even though forklifts are capable of stacking containers higher. The surface stacking configuration is designed to minimize any additional handling prior to placing waste on the waste shaft conveyance for transfer to the underground. Any overstacking event is bounded by the calculations for overstacking in the underground repository discussed in Section 7.2.1 (recall that concrete reflection is comparable to salt and/or MgO reflection).

7.3 Underground Roof Fall

A roof fall impacting all of the containers in the array during the operational phase of a disposal panel is unlikely due to the historic behavior of the salt repository and WIPP's safe mining practices. (The DSA [39] considers a roof fall breaching 30 waste assemblies as an anticipated event but this analysis considers the unlikely event of a roof fall impacting the entire infinite array or waste assemblies.) If a roof falls, vertical compaction of 15 inches to the bottom tier of drums is postulated in PLG-1167, *Analysis of Roof Fall and Methane Gas Explosions in Closed Rooms and Panels* [43]. For machine-compacted waste and waste with unlimited Be content, the result is bounded by the normal condition models since the reflector density considered in these models is already as high as can be physically achieved. A number of runs were performed to evaluate this scenario for non-compacted waste. The runs modeled direct-loaded 55-gallon drums stacked three high. The first case evaluates 650 grams of ^{239}Pu optimally moderated per seven-pack with three 200-gram ^{239}Pu drums and one 50-gram ^{239}Pu drum. The second case evaluates 100 grams of ^{239}Pu optimally moderated with 100 kilograms of beryllium per drum. In both cases, runs were performed with and without the 15 inches of compaction of the bottom row. The compaction was modeled by reducing the height of the bottom row of drums by 15 inches and then centering the fissile material in the shortened drum. The results with and without compaction are summarized in Table 7-2. The compaction has a small effect on the reactivity of the array and all results remain below the USL of 0.96. In addition to compaction due to roof fall, it is possible that the MgO sacks could break such that MgO would fall between drums in an assembly or between columns of waste assemblies. This condition is bounded by the full MgO reflection evaluated around the two-container models as the MgO would provide reflection and act to decouple the fissile masses in the array. Again, a large roof fall is not expected during the operational pre-closure phase of a disposal room or panel. The underground roof fall contingency for the CCO is modeled as crushing all of the void space between the containers and the plywood dunnage located at the top of the drum as well as the plywood dunnage on the bottom of the bottom row. This results in a total compaction of 14.88 inches and is further discussed in Appendix G. This upset was not evaluated with shielded containers because the thick lead/steel walls would limit compaction of the container wall and four-tier stack calculations in Section 7.2.1 demonstrate that their is little interaction from one tier to the next due to the thick container lids and bottoms. As this upset remains subcritical and the loss of other controlled parameters, such as mass, would require a concurrent and independent change in process conditions, the double contingency principle is met. See Section 7.10 for the evaluation of concurrent upsets to justify that a criticality accident is not credible.

Table 7-2. Evaluation of Compaction caused by Roof Fall in the Underground Repository

Container and Waste Loading	Compaction	$k_{eff} + 2\sigma$	Filename (Section)
55-gallon drums of direct-loaded waste with ≤ 1 wt% special reflectors	None	0.90096	dac0026 (A.2.1)
	15 in. in bottom row	0.92034	daccp24 (A.4.4)
55-gallon drums of direct-loaded waste with > 1 wt% special reflectors	None	0.89169	a20kb (B.2.1)
	15 in. in bottom row	0.89792	ac20kb (B.3.6)
CCOs	None	0.94545	hx800mgo380fge (G.2.1)
	4.46-5.96 in. per row for a total of 14.88 in.	0.95856	uugrf750hx380fge (G.3.5)

7.4 Exceeding Mass Limits

7.4.1 Exceeding the Fissile Mass Limit for a Container

Since WIPP does not open CH waste containers, there is no potential for adding fissile material to a CH container during normal operations at WIPP. (Overpacking of a damaged container at WIPP is an approved process and is analyzed separately in Section 7.4.2.) It was demonstrated in Sections 5.3 and 5.4 that if all the drums in waste assemblies were loaded to their maximum allowable limits, the system would remain below the USL. As a result, the accumulation of a critical configuration in the underground disposal room array can only occur if waste exceeding the WIPP WAC [40] fissile limits is sent to WIPP.

Exceeding the fissile mass for a container is unlikely as non-destructive analysis (NDA) is performed at the waste generator site and confirmed prior to preparing containers for shipment to WIPP. CH-TRAMPAC [5] requirements indicate that the mass estimate must include two times the uncertainty in the NDA measurement. This estimate is then compared to the container FGE limit to determine compliance with the WIPP WAC [40]. Generator sites that perform waste characterization activities for shipment to WIPP participate in the Performance Demonstration Program (PDP) to comply with the WIPP WAC. The PDP serves as a quality control check for data generated in the characterization of waste destined for WIPP. The PDP evaluates analyses of TRU radionuclides using NDA techniques. The PDP is designed to test NDA techniques for both drummed waste and boxed waste for the TRU Waste Characterization Program. The TRU Sites and Transportation Division within the DOE-Carlsbad Field Office (CBFO) is the review and approval authority for all PDP activities as discussed in DOE/CBFO-01-1005, *Performance Demonstration Program Plan for Nondestructive Assay of Drummed Wastes for the TRU Waste Characterization Program* [44] and DOE/CBFO-01-1006, *Performance Demonstration Program Plan for Nondestructive Assay of Boxed Wastes for the TRU Waste Characterization Program* [45]). In addition, the underground disposal fissile mass limits are often higher than the limits for transport of the containers in the TRUPACT-II or HalfPACT shipping containers. To simulate a fissile mass overbatching event, one container in a three-tier stack is evaluated as overbatched by 50% of its nominal value. Thus, one drum out of every nine 100-gallon drums (11%), one out of every twenty-one 55-gallon drums, POCs or CCOs (5%), or one SWB out of every three (33%) exceeds the WIPP WAC. Also, all containers around the overbatched container are filled to the underground repository requirements, which would require exceeding the current total payload mass limits for the HalfPACT and TRUPACT-II shipping package, with the exception of SWBs shipped in the HalfPACT. Thus, exceeding the as-modeled condition is not considered credible.

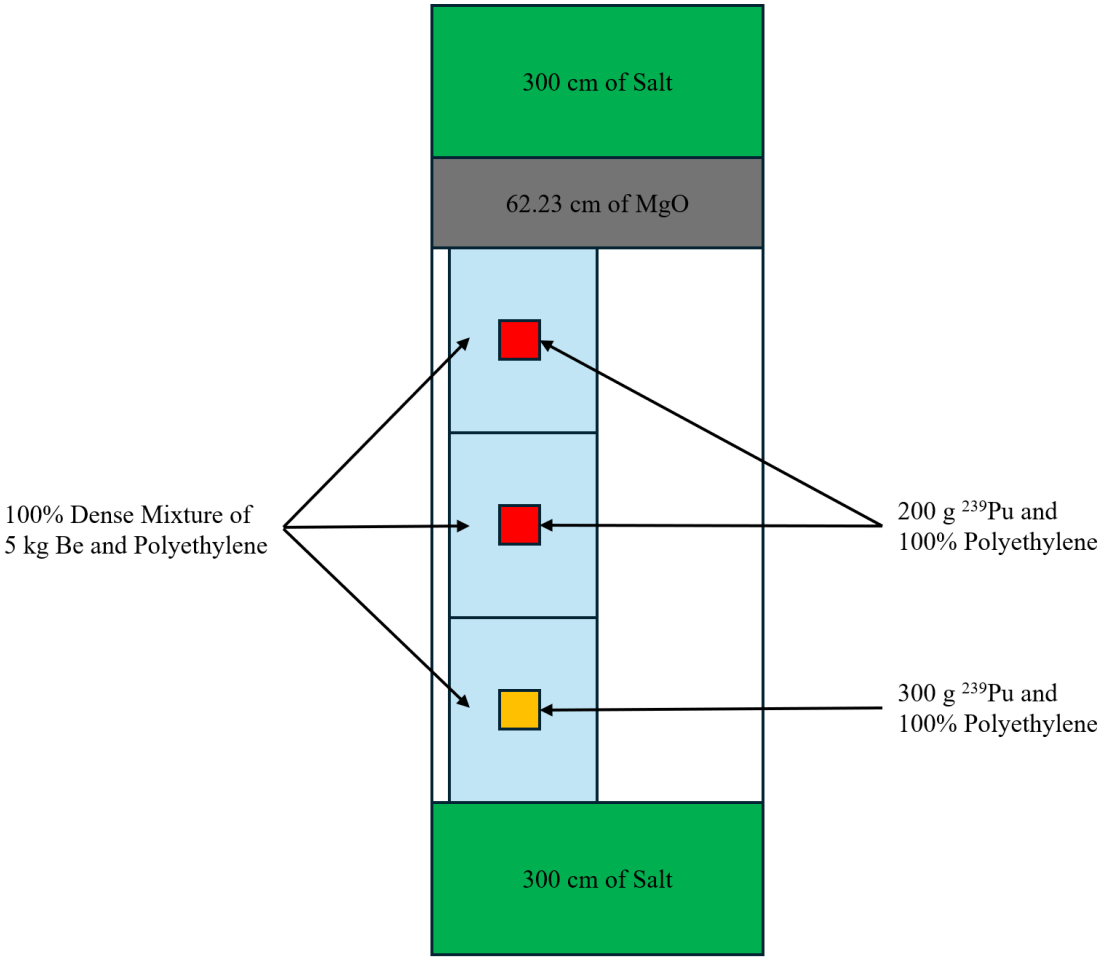
From a modeling perspective, one container in the bottom or middle tier is overbatched and the stack is infinitely reflected on the lateral surfaces as in the base array model described in Section 5.1.13. As noted above, this is highly conservative as it results in one of twenty-one 55-gallon drums, POCs or CCOs (5%), one of nine 100-gallon drums (11%), or one of three SWBs (33%) being overbatched. Figure 7-1 illustrates the model configuration used in the fissile mass overbatching event for compacted waste in 100-gallon drums.

The results of the overbatching contingency are tabulated in Table 7-3. The computational results indicate that the double-contingency requirement for the ^{239}Pu mass content in the containers is met as multiple overbatching events will not result in the USL being exceeded. As discussed earlier, the waste generator is required to control the canister FGE loading by the WIPP WAC [40] and by the DOT and U.S. Nuclear Regulatory Commission package licensing requirements for the TRUPACT II, HalfPACT and TRUPACT III shipping containers. The following points are made from a probabilistic viewpoint with respect to overbatching:

- A misbatched CH container can be made by human error, misidentification of containers, instrument miscalibration, or some other process upset. However, not all misbatched CH containers will be above the NCS fissile loading limit as fissile material is valuable and generally not considered waste unless only small quantities are present or the fissile material has been recovered to the extent practical. Containers below the NCS limits remain subcritical.

- The criticality models used in this NCSE are based on optimally moderated fissile materials in pure form in optimum shapes to minimize neutron loss. The reflector materials in the drums/canisters are also modeled at the maximum credible densities to maximize reactivity. Even small deviations from these optimum conditions result in a significant reduction in reactivity.

As this upset remains subcritical and the loss of other controlled parameters, such as interaction (stack height), would require a concurrent and independent change in process conditions, the double contingency principle is met. See Section 7.10 for the evaluation of concurrent upsets to justify that a criticality accident is not credible.



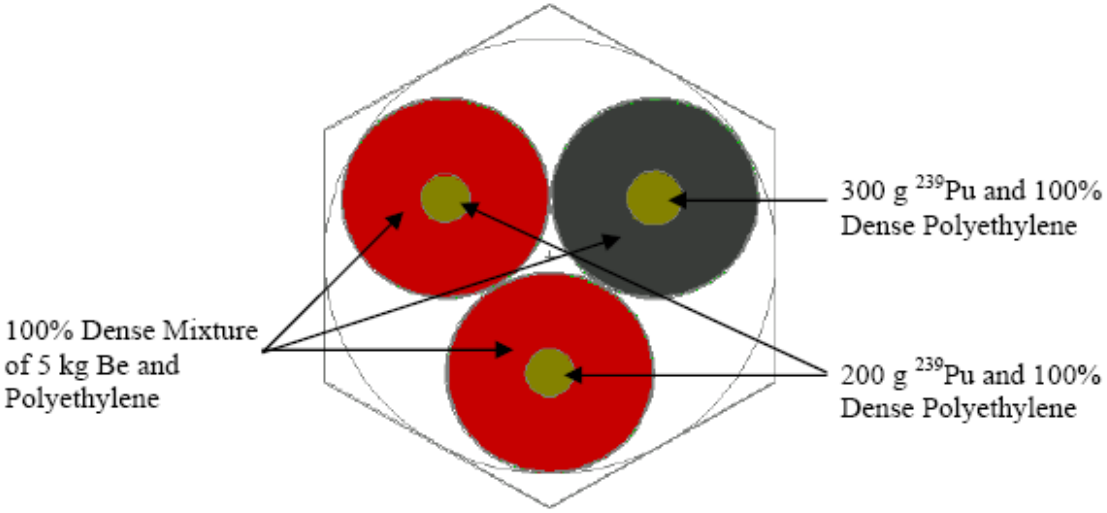


Figure 7-1. Example Array Model for ^{239}Pu Overbatching in 100-gallon Drum Event

Table 7-3. Fissile Gram Equivalent Overbatching Contingency Results

Container and Waste Loading	Overbatch Scenario	$k_{eff} + 2\sigma$	Filename (Section)
55-gallon drums of direct-loaded waste with ≤ 1 wt% special reflectors	None	0.90096	dac0026 (A.2.1)
	1 drum at 300 FGE, 7-pack limit of 650 FGE maintained	0.91148	dacdb24 (A.4.2)
Shielded containers of direct-loaded waste with ≤ 1 wt% special reflectors	None	0.90677	SC30G1a10nprn (H.2.1)
	1 drum at 300 FGE	0.92055	SC30G1c10NPRn (H.3.2)
SWBs of direct-loaded waste with ≤ 1 wt% special reflectors (bounds SLB2s)	None	0.88393	2psna12 (A.2.2)
	1 SWB at 570 FGE with 37.5 g ^{240}Pu	0.94356	2pswo11 (A.4.2)
55-gallon drums of direct-loaded waste with > 1 wt% special reflectors	None	0.89169	a20kb (B.2.1)
	1 drum at 150 FGE with 100 kg Be	0.90388	ao15kb (B.3.4)
SWBs of direct-loaded waste with > 1 wt% special reflectors (bounds TDOPs)	None	0.80815	aswb10f (B.2.2)
	All SWBs at 150 FGE	0.90953	oswb08f (B.3.4)
100-gallon drums of fully compacted waste	None	0.86166	aray118 (C.2.1)
	1 drum at 300 FGE	0.94940	aray218 (C.6.3)
55-gallon drums of fully compacted waste	None	0.86230	ara5518 (C.2.2)
	1 drum at 300 FGE	0.94996	ara5558 (C.6.2)
Shielded containers of fully compacted waste	None	0.86235	SC30G1a10MC (H.2.1)
	1 drum at 300 FGE	0.94979	SC30G1c09MCC (H.3.2)
SWBs of fully compacted waste	None	0.86162	ar1000_200 (C.2.3)
	1 SWB at 300 FGE	0.94507	aro800_300 (C.6.4)
Pipe overpacks in 55-gallon drums with ≤ 1 wt% special reflectors and compacted waste	None [a]	0.89471	pa20018pf (D.2.1)
	1 drum at 300 FGE [b]	0.96428	pa20016pm (D.3.2)

Pipe overpacks in 55-gallon drums with direct-loaded waste with > 1 wt% special reflectors	None [(a)]	0.93050	pa14016p (D.2.1)
	1 drum at 210 FGE [(c)]	0.93483	pa14014pn (D.3.2)
CCOs	None	0.94545	hx800mgo380fge (G.2.1)
	1 CCO at 570 FGE	0.95300	uob800hx570fge500hx (G.3.2)

(a) Note that in the normal condition array model, pipe overpacks are subcritical when moderated and reflected by full density polyethylene, representative of machine compacted waste, with no limit on polyethylene content. This was the only configuration modeled for the normal condition since it bounds direct-loaded waste.

(b) For the compacted waste configuration. The fissile mass in the overpack is moderated by 100% by volume polyethylene with the remainder of the pipe filled with 86% dense polyethylene. This results in a polyethylene limit of 33.9 kg for compacted waste. Since direct-loaded waste has a maximum polyethylene content of 25 volume %, this case bounds direct-loaded waste and no polyethylene mass limit is needed.

(c) The polyethylene packing fraction needed to be reduced to 25% by volume, representative of direct-loaded waste, in this overbatch case. Thus machine-compacted waste is not allowed in pipe overpacks with > 1 wt% special reflectors.

7.4.2 Overpacking Overbatches

For one-to-one overpacking, since only one container can be physically loaded into the overpacking container an overbatch with an extra container in the overpack is not possible. Overbatching in the container itself is addressed by the foregoing analyses and mass limits for the individual waste containers and is also applicable to one-to-one single container overpacking with no loose material outside of the inner container within the larger overpacking container. As discussed in Section 5.5.1, a single smaller container overpacked in a larger container is less reactive than the single smaller container by itself since the configuration occupies a larger footprint than the Individual smaller container.

Multiple-to-one overpacking performed on-site at WIPP introduces a contingency not previously analyzed. As discussed in Section 5.5.2, multiple-to-one overpacking essentially results in dividing the mass from a single unit as previously analyzed where the divided mass is less reactive. Consider again the scenario of 55-gallon drums in a TDOP with non-compacted ≤ 1 wt% special reflector waste. The limit of the configuration is the larger container (TDOP) limit of up to 325 FGE (with 0 grams of ^{240}Pu). Since one 55-gallon drum may contain up to 200 FGE, a conservative overbatch scenario would be if one 200 FGE container were included in the TDOP in addition to the 325 FGE in the other drums for a total of 525 FGE. However, this scenario is bounded by the seven-pack 55-gallon drum analysis that allows up to 650 FGE. The same argument holds for containers in four- and three-packs, and similar arguments apply to machine compacted drums with pack limits of 600 FGE. Shielded containers and pipe components have no pack limits and each container is evaluated at that limit such that as many containers as fit into the TDOP/SWB is bounded by the analysis of each of those containers. Likewise, there are no pack limits for containers with > 1 wt% special reflectors. And finally, two SWBs in a TDOP would be the same as two SWBs evaluated under normal conditions. The limits of the larger containers are summarized in Section 9.0 with the additional control that no loose material may be included within the larger overpacking container. Thus, this upset condition is bounded by exceeding the container fissile mass as evaluated in Section 7.4.1.

7.4.3 Exceeding the Beryllium Mass Limit for a Container

The beryllium overbatching contingency is similar to the fissile mass overbatching event in that at least one drum in the modeled three-tier stack of containers exceeds its beryllium mass limit. For example, containers with a 5-kilogram beryllium limit are evaluated as double batched to 10 kilograms and the high beryllium drums with a 100-kilogram limit are evaluated as overbatched to 150 kilograms. The results of the overbatching contingency are tabulated in Table 7-4, which shows that the system eigenvalue is well

below the USL. As expected, double batching the beryllium has only a minor effect. As this upset remains subcritical and the loss of other controlled parameters, such as mass, would require a concurrent and independent change in process conditions, the double contingency principle is met. See Section 7.10 for the evaluation of concurrent upsets to justify that a criticality accident is not credible.

Table 7-4. Beryllium Overbatching Contingency Results

Container and Waste Loading	Overbatch Scenario	$k_{eff} + 2\sigma$	Filename (Section)
55-gallon drums of direct-loaded waste with ≤ 1 wt% special reflectors	None	0.90096	dac0026 (A.2.1)
	1 drum at 10 kg Be	0.90056	dacbb24 (A.4.3)
55-gallon drums of direct-loaded waste with > 1 wt% special reflectors	None	0.89169	a20kb (B.2.1)
	1 drum filled with Be (> 300 kg)	0.88842	ae20kb (B.3.5)
Shielded containers of direct-loaded waste with ≤ 1 wt% special reflectors	None	0.90677	SC30G1a10nprn (H.2.1)
	All containers at 6 kg Be	0.90472	SC30G1d10BeOBn (H.3.3)
Shielded container of fully compacted waste	None	0.86235	SC30G1a10MC (H.2.1)
	All containers at 6 kg Be	0.86358	SC30G1d10MCn (H.3.3)
100-gallon drums of fully compacted waste	None	0.86166	aray118 (C.2.1)
	1 drum at 10 kg Be	0.86230	aray318 (C.6.5)

7.5 Sprinkler Activation in the Waste Handling Building

The WHB is equipped with a fire sprinkler system. This contingency addresses activation of the sprinkler system resulting in interspersed moderation between the waste containers. (Water ingress into a container is included in the normal condition analysis as the fissile material is optimally moderated by water and/or polyethylene. See also the discussion of excess liquid in a waste container in the next section.) Although containers are only stacked two high above ground, a three-tier stack of seven-packs of 55-gallon drums is modeled for conservatism. The ceiling and floor are modeled as 2-foot-thick concrete, while the sides are mirrored for infinite reflection as shown in Figure C-15, in Appendix C. The cases are evaluated at the maximum mass limits and optimum H/Pu ratio for the base array. Thus, the 55-gallon drums of non-compacted waste are modeled with 200 FGE in three drums, 50 FGE in one drum, and three drums empty; the fissile material is moderated at an H/Pu ratio of 1,300 per Section A.2.1 and 55-gallon drums of machine compacted waste are modeled with 200 FGE in three of the 55-gallon drums in the seven-pack at an H/Pu ratio of 900 per Section C.2.2. Water mist from sprinkler activation is allowed to fill the interstitial spaces between the containers. The water density is varied from 0.05 to 1 g/cm^3, and the results are shown in Figure 7-2. Interstitial water reduces the reactivity of an array of non-compacted waste containers, but has little effect on containers of compacted waste as the high-density polyethylene in the drum isolates the fissile masses in the drums from one another. The same result would be true for containers with > 1 wt% special reflectors as the beryllium provides isolation and for shielded containers as the thick steel/lead walls also provide isolation. These results can also be extrapolated to other containers of direct-loaded waste, as all are larger in size such that the interstitial moderation will be further from the fissile material and will exhibit a similar trend in reactivity. All results are significantly below the USL and the addition of interstitial water reduces reactivity. These calculations are summarized from Appendix C for machine-compacted waste and Appendix A for direct-loaded waste.

Water ingress into the WIPP underground is observed at the shafts but not in the disposal area during the operational period. The same reactivity trend would occur if water somehow was available in the underground repository, and the k_{eff} would not increase above the analyzed dry condition. The results for the water density effect on the reactivity also bound the effects of spraying water onto waste containers from fire hose connections. The same reactivity trend would occur and the k_{eff} would not increase above the dry condition. Thus, this upset is not a criticality safety concern.

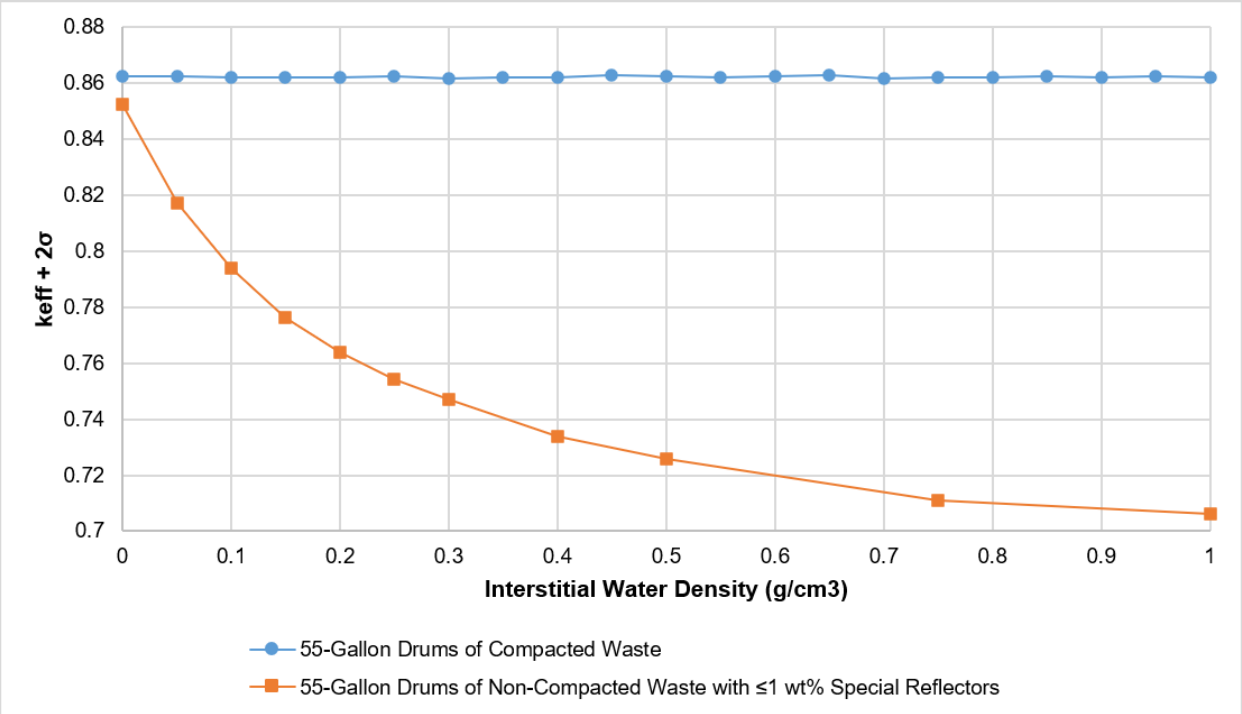


Figure 7-2. Results with Interstitial Water Between Containers

7.6 Excess Liquid in Waste Containers

This contingency evaluates more than 1% liquid present in the waste container, which could occur from a generator site error or water intrusion into the containers. Although the underground is not subject to flooding, the analysis considers all containers in the underground array containing excess water at various densities up to point where water fills all void space in the container. Only non-machine-compacted waste with loose polyethylene dunnage mixed with 1% special reflector material is considered since waste forms with large quantities of special reflector materials or machine-compacted waste will be less reactive if water is substituted for the special reflector material or the polyethylene. The H/Pu ratio in the fissile material is varied at each water density considered to ensure the optimum condition is modeled.

The calculation results are summarized in Table 7-5 for 55-gallon drums of direct-loaded waste with less than or equal to 1 wt% special reflector materials. These cases are documented in detail in Appendix A. Additionally, Appendix A gives the results of similar calculations for direct-loaded waste in SWB arrays. The results for SWBs follow a similar pattern as given in Table 7-5 for 55-gallon drums, with the fully flooded SWB at the highest reactivity but well below the USL at 0.91742.

This contingency is also applied to the CCO and simulates an abnormal state where CCOs contain an excess of liquid that fills the void dunnage as a result of generator site error or water seepage into the

container. These cases are documented in detail in Section G.3.3 of Appendix G. The results show that reactivity for the fully flooded cases is significantly lower than the normal CCO calculations. Thus, this upset is not a criticality safety concern.

Table 7-5. Excess Liquid in 55-gallon Drum Contingency Results

Container and Waste Loading	Water Density in 25% Dense Polyethylene Reflector (% of theoretical)	$k_{eff} + 2\sigma$	Filename (Section)
55-gallon drums of direct loaded waste with ≤ 1 wt% special reflectors	0	0.74767	dac2526 (A.2.1)
	18.75	0.76707	dacw026 (A.4.6)
	37.5	0.78482	dacw062 (A.4.6)
	56.25	0.80061	dacw102 (A.4.6)
	75	0.81173	dacw142 (A.4.6)

7.7 Forklift Accident Crushes Containers

This contingency simulates an accident condition where the 41-ton waste handling forklift impacts an array of seven-packs of 55-gallon drums in the underground repository. The 41-ton forklift is not used to move CH containers, but is used to move the lead shielded facility cask containing RH waste and the shielded, heavy portions of the horizontal emplacement retrieval equipment as described in the DSA [39]. The 41-ton forklift can also be used to move other large, heavy equipment from the waste hoist. The forklift is not normally near the CH container waste face because the RH canisters are typically emplaced into boreholes in the salt walls before the CH containers are emplaced nearby. The RH horizontal emplacement waste handling equipment is typically placed between the CH container face and the approaching 41-ton forklift. The DSA considers a forklift accident that breaches 16 waste assemblies an anticipated event. This analysis considers the unlikely event where the forklift accident breaches all of the assemblies in the modeled infinite array. This evaluation bounds impacts between smaller forklifts and CH waste containers as smaller forklifts would impact less containers with less force.

The 55-gallon drum of direct-loaded waste was chosen for this contingency because the 55-gallon drum is the smallest CH waste container and thus, will create the tightest array when crushed. This container and waste type also does not have significant internal reflection that would reduce interaction between the fissile masses. The high-density polyethylene in machine compacted waste, the high beryllium content in waste with a large amount of special reflectors, and the thick lead/steel walls in the shielded container all reduce interaction. To simulate the effects of a high-energy impact of the 41-ton forklift on the waste drums, some of the air volume is expelled from the 55-gallon drums leaving the drums permanently deformed. In particular, the volume of the 55-gallon drums is reduced to 75% of its initial volume in the model. Since some air is expelled, the internal reflector mass around the moderated fissile mass will compress and the density will increase. Thus, the polyethylene, which makes up the bulk of the dunnage around the fissile mass, is compressed from a maximum of 25 to 33% of its theoretical density. Furthermore, the model evaluates the geometry of the 55-gallon drums as deformed into an elliptical shape with the ratio of the major to minor axes being 2. In this configuration, the elongated fissile mass and internal reflector waste in the 55-gallon drums are moved closer together and become more reactive. In order to minimize the distance between fissile masses in the array, the model uses a rectangular array since the waste packages and drums are elliptical cylinders. Finally, to maximize the reactivity state of the system and at the same time not restrict the number of seven-packs involved in the accident, mirror boundary conditions are used on three of the four lateral boundaries simulating an infinite array. The

fourth boundary uses a reflector made up of 200 centimeters of lead to bound the lead shielding on the RH facility cask and the steel structure of the forklift. In the vertical plane, MgO supersacks are placed on top of the 55-gallon drums and the whole stack is then reflected by 300 centimeters of salt above and below. Figure 7-3 shows a top view of the model used in the analysis.

Two drum configurations were considered. The first configuration evaluates three 200-FGE drums as impacted by the forklift and the whole seven-pack stack is crushed and displaced into the surrounding seven-packs. The resulting arrangement is a 3-by-3 array with three 200-FGE drums in the first row, one 50-FGE drum in the middle of the second row with one non-fissile bearing drum on either side, and one non-fissile bearing drum in the middle of the last row with one 200-FGE drum on either side. The two 200-FGE drums in the last row originate from the surrounding seven-packs. The boundaries that are not reflected by lead are infinitely reflected to model an infinite array of crushed seven-packs. Figure 7-3 shows the top view of the drums in this configuration. The second configuration is similar to the first except the fissile contents in the drums in the first and last rows are exchanged. Finally, to maximize the interaction effects, a computation was also performed where the polyethylene in the internal reflector was removed and only the beryllium remained in the reflector zone of the "crushed" drums.

Figure 7-4 summarizes the results of the contingency calculation with further details given in Section A.4.7 of Appendix A. The maximum system eigenvalue was 0.89501 and occurred when the polyethylene was removed from the crushed drums thereby increasing the interaction amongst the close fissile masses. This value is below the base 55-gallon drum array $k_{eff} + 2\sigma$ value of 0.90096 as given in Section A.2.1. The reduction in k_{eff} results from the fact that front face of the waste is reflected by lead instead of other fissile waste drums in the base infinite array model. Thus, a criticality accident from a loss of interaction control caused by the impact of a large object, such as a 41-ton forklift, with an array of CH containers is not credible.

This contingency was applied to the CCO container and is discussed in detail in Section G.3.4 of Appendix G. The maximum system $k_{eff} + 2\sigma$ was 0.94307, which is below the normal condition maximum eigenvalue of 0.94545. The same reason for the drop in k_{eff} in the direct loaded 55-gallon drum array is responsible for the drop in k_{eff} in the CCO array and one face of the CCO array is reflected by lead instead of other fissile waste drums. Thus, a criticality accident from a loss of interaction control caused by the impact of a large object, such as a 41-ton forklift, with an array of CCOs is not credible.

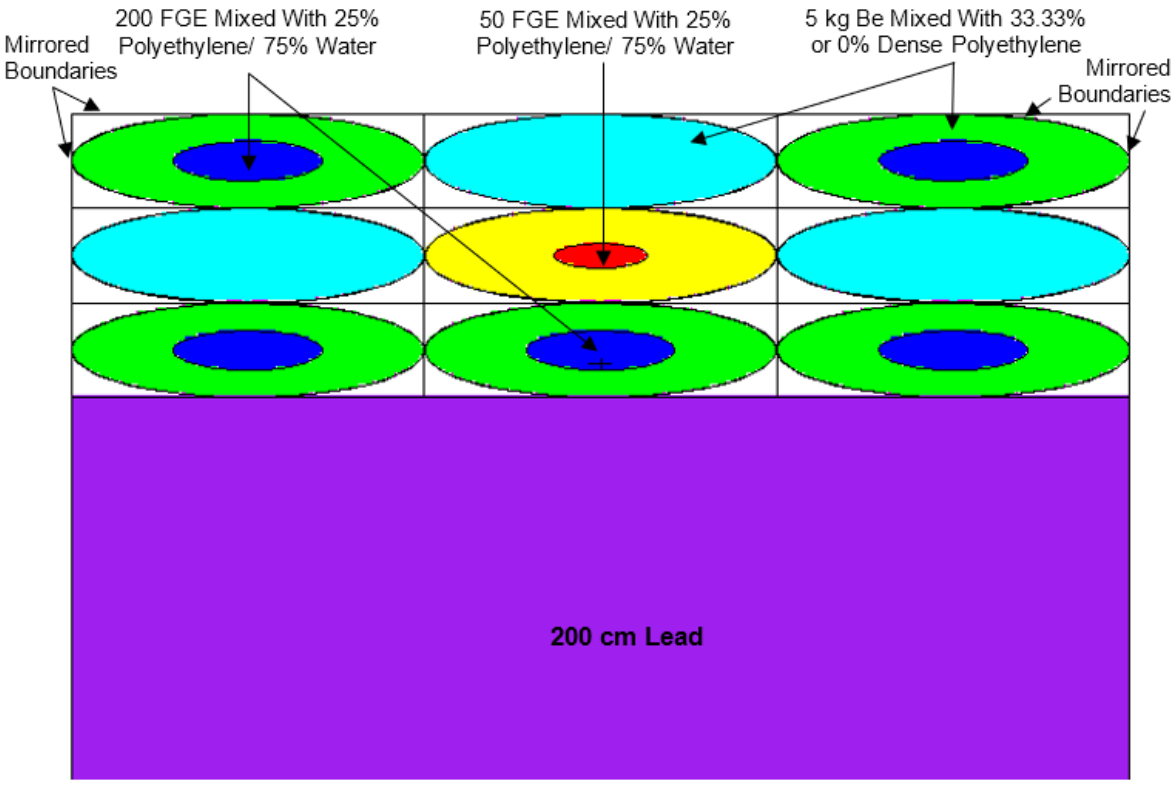


Figure 7-3. Top View of Model for the 41-ton Forklift Impact with an Array of 55-gallon Drum Seven-packs

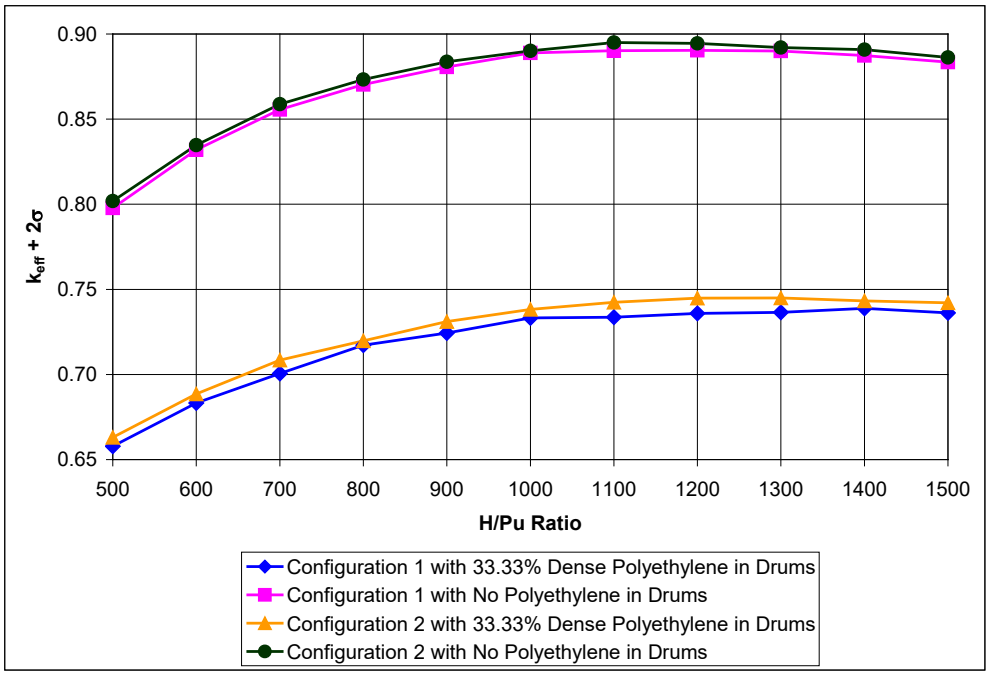


Figure 7-4. System Reactivity Resulting from a 41-ton Forklift Impact with 55-gallon Drums Seven-packs

7.8 Ejection of Material from Drum

This contingency evaluates an accident where a drum ejects a portion of its contents onto the floor and surrounding containers. This release could be caused by an overpressurization or deflagration. This release causes a percentage of the drums contents to be thrown from the drum. The event would result in a lower k_{eff} than normal operation for the array case because material is removed from the container and spread out in a noncentralized area around the container. This reduces the fissile material in the drum and changes the geometry into a less favorable shape, which results in a lower k_{eff}.

7.9 Natural Phenomena Events

This contingency evaluates natural phenomena events such as an earthquake, high wind, or tornado. Specifically, an earthquake could result in the toppling of stacked waste containers inside the WHB and cause a loss of confinement of material. Waste containers in the WHB are stacked up to two tiers high on facility pallets for transport to the underground. The earthquake could cause stacked waste containers to fall and may result in a spill of contents on the WHB floor. The floor of the WHB is a flat concrete surface with no sumps for potential pooling of spilled material and would result in a slab configuration of the contents released from the waste container. As stated in Section 5.3, fissile material is modeled in a concentrated optimally moderated geometry and no spacing is modeled between intact containers. The toppling of stacked containers would result in more spacing between containers after the fall than analyzed and a spill, if it occurred, will disperse some of the fissile material from the container into a less compact, less reactive geometry on the floor. Thus, the material will not combine into one large mass and support a criticality accident, but instead result in a less reactive configuration than analyzed.

7.10 Contingency Analysis Conclusion

The previous subsections have justified that the double contingency principle is met as each contingent condition is shown to remain subcritical. The base case arrays are modeled such that the fissile content for each drum or shielded container is nominally twice that allowed by the shipping packages. The contingency upset conditions are evaluated additively to the base cases. However, to demonstrate that a criticality event is not credible, combinations of events must be evaluated. First, note that the load drop in the shaft is shown not to be a credible event, and the sprinkler activation, water intrusion, and forklift crushing contingencies each resulted in a reduction in array reactivity. Thus, none of these events need to be further analyzed. Also, roof fall is extremely unlikely in the active operational phase prior to closure of the panel, which is the scope of this NCSE. The highest risk is judged to result from a container that exceeds the fissile mass limit being placed in a four-tier high array. The over-stacking contingency discussed in Section 7.2 was modeled with each drum assembly containing almost twice the fissile mass allowed in the transportation package and each CCO and SWB at the transportation package mass limit. This configuration is extremely unlikely based on the actual conditions. Further, a mining or waste handling error to this extent to allow a whole panel of containers to be stacked four high with MgO on top is also not credible. In reality, only limited areas would be mined higher than normal to allow a four-tier array. Also, the 55-gallon drum array modeled four high without MgO on top, which is still conservative compared to the mined height, showed little reactivity change compared to the three-high array. Thus, an overbatched container in a four-tier array will have a comparable reactivity to that given in the over-batching evaluation in Section 7.4 and the array will remain subcritical even with both upset conditions. Furthermore, the fissile material is evaluated in a single, optimally moderated mass in each container, which is unrealistic for debris waste. As demonstrated in Section 5.3.2, this is an very conservative modeling approach as k_{eff} drops drastically when the fissile material is modeled spread throughout the waste container. Thus, a criticality accident at the WIPP is deemed not credible and a criticality detection system is not required.

8.0 Beyond Design Basis Events

Flooding of the underground repository is beyond the design basis of the WIPP facility. Regardless, interstitial moderation between containers is analyzed in Section 7.5 and flooding of the containers in Section 7.6. Both events are shown to not result in an increase in array reactivity above the USL. In addition, all contingent events were analyzed and it was shown that a resulting criticality accident is not credible.

The waste hoist failure is considered not credible as discussed in Section 7.1. If the waste hoist failure occurred and the load was dropped, the contents could fall into the sump and become moderated. However, the size of the load is physically restricted to a single SLB2, four SWBs, or four packs of drums. For a multiple container load, the impact would tend to disperse the containers, such that even if they were breached, it is improbable that the fissile contents would combine into one large mass. In addition, a full array of flooded containers has been shown to remain below the USL such the limited load would remain subcritical if the containers were moderated by the sump water. Overall, the risk of a criticality accident from a load drop from the waste hoist is low; therefore, further analysis is not warranted.

Section 7.4 evaluates credible overbatch scenarios. The fissile material in one container per stack is overbatched by 50% of the limit or the special reflector material is overbatched by 100% of the limit in one container per stack. All contents of the other containers in the array are modeled at their fissile and special reflector limits. Overbatching by higher amounts is not considered credible, but is discussed here as a beyond design basis event. The fissile material is modeled in an optimally moderated, compact configuration, which is highly conservative because the nature of waste is that the fissile material is dispersed through the waste matrix as pure forms of fissile material would tend to be recovered for use. Calculations in Section 5.3.2 showed that spreading the fissile material more realistically throughout the waste container reduces k_{eff} to below 0.4. Also, liquids are not allowed in waste containers to provide moderation of the fissile material. The multiplication factor of the array drops significantly as the fissile material is dispersed in the container as seen in the study discussed in Section 5.3.2. In addition, the average FGE content in non-compacted drums in the underground repository is less than 50 FGE such that a full array of containers anywhere near the fissile limits is very unlikely. Consequently, further consideration of larger overbatch events is not warranted.

9.0 Design Features and Administratively Controlled Limits and Requirements

A summary of the credited design features and administrative limits and requirements for criticality safety are provided in the following sections.

9.1 Design Features

The M&O Contractor maintains configuration control at the WIPP facility. Revision to significant design features requires an unreviewed safety question determination to verify that the change will remain within the approved safety basis. For the purposes of this evaluation, the waste container type is the design feature that provides spacing between the fissile contents of the TRU waste. All containers currently approved for shipment to the WIPP in the TRUPACT-II, HalfPACT or TRUPACT-III shipping casks have been evaluated. Changes in container design or the addition of a new container type will need to be evaluated before it can be received, stored, handled, or disposed of at the WIPP.

9.2 Administrative Limits and Requirements

The controls below are required to ensure that a criticality accident is not credible for CH waste containers at the WIPP.

1. Container arrays are limited to three tiers, where a drum, pipe overpack, shielded container, CCO or SWB occupies one tier and a TDOP or SLB2 occupies two tiers.

2. Waste approved for shipment to and disposal at WIPP are required to meet the WIPP WAC [40]. The WAC shall contain the CH container limits in Table 9-1.

3. If onsite overpacking is required, all one-to-one overpacking configurations shall maintain the appropriate limit(s) of the smaller overpacked container from Table 9-1. All multiple-to-one overpacking configurations from Table 5-13 shall maintain the appropriate limit(s) of the larger overpacking container from Table 9-1. Loose material around the overpacked container(s) shall not be placed into the overpacking container.

Table 9-1. Summary of Limits Imposed on Contact-Handled Waste

Container Type	Fissile Mass Limit[a]	Container Geometry Requirements	Non-Fissile Material Limits[b]
Non-compacted Waste Containing ≤ 1 wt% Special Reflectors (Direct Loaded or Overpacked)			
55-, 85-, 100-gallon drums	≤ 200 FGE per drum ≤ 650 FGE per pack[c]	None	Special reflector mass ≤ 1 wt%
Shielded containers	≤ 200 FGE per container	Shielded container nominal dimensions per Appendix H	Special reflector mass ≤ 1 wt%
SWB, TDOP or SLB2	≤ 325 FGE with 0 g ^{240}Pu ≤ 340 FGE with 5 g ^{240}Pu ≤ 360 FGE with 15 g ^{240}Pu ≤ 380 FGE with 25 g ^{240}Pu	None	Special reflector mass ≤ 1 wt%
Pipe overpack assembly	≤ 200 FGE per pipe component	Applies to standard, S100, S200 and S300 pipe overpack assemblies per Appendix 1.3.1 of the TRUPACT-II SAR [2]	Special reflector mass ≤ 1 wt%
CCOs	≤ 380 FGE per CCO	None	Special reflector mass ≤ 1 wt%
Non-compacted Waste Containing > 1 wt% Special Reflectors (Direct Loaded or Overpacked)			
55-, 85-, 100-gallon drums	≤ 100 FGE per container	None	Special reflector mass ≤ 100 kg per container
SWB or TDOP	≤ 100 FGE per container	None	None
Pipe overpack assembly	≤ 140 FGE per pipe component	Applies to standard, S100, S200 and S300 pipe overpack assemblies per Appendix 1.3.1 of TRUPACT-II SAR [2]	None
55-, 85-, 100-gallon drum overpacked in SWB or TDOP (no loose material in the SWB or TDOP)	≤ 100 FGE per container 1 container per SWB or TDOP	None	Special reflector mass ≤ 100 kg per container

Table 9-1. Summary of Limits Imposed on Contact-Handled Waste

Container Type	Fissile Mass Limit[a]	Container Geometry Requirements	Non-Fissile Material Limits[b]
Machine-compacted Waste[b] (Direct Loaded or Overpacked)			
Partially compacted waste in 55-, 85-, or 100-gallon drums	≤ 200 FGE per drum ≤ 600 FGE per pack[c]	None	Packing fraction of drum contents ≤ 70% Special reflector mass ≤ 1 wt%
Fully compacted waste in 55-, 85-, or 100-gallon drums without design vertical spacing	≤ 170 FGE per drum[e] ≤ 600 FGE per pack[c]	None	Special reflector mass ≤ 1 wt%
Fully compacted waste in 55-, 85-, or 100-gallon drums with design vertical spacing	≤ 200 FGE per drum[e] ≤ 600 FGE per pack[c]	Minimum 0.5-in. spacing[d] between drum content and exterior top and bottom must be maintained, even if a smaller drum were placed on top of the drum	Special reflector mass ≤ 1 wt%
Pipe overpack assembly	≤ 200 FGE per pipe component	Applies to standard, S100, S200, and S300 pipe overpack assemblies per Appendix 1.3.1 of the TRUPACT-II SAR [2]	Special reflector mass ≤ 1 wt% Plastic mass < 33.9 kg
Shielded containers	≤ 200 FGE per container[e]	Shielded container nominal dimensions per Appendix H	Special reflector mass ≤ 1 wt%
CCOs	≤ 380 FGE per CCO	None	Special reflector mass ≤ 1 wt% Plastic mass ≤ 2,000 grams
Fully compacted waste in SWB or TDOP without limitation on inner configuration	≤ 200 FGE per SWB or TDOP[e]	None	Special reflector mass ≤ 1 wt%

(a) Fissile mass shall include 2 times the error in the measurement.

(b) The limit for polyethylene density for non-compacted waste is < 20%; for partially (machine) compacted waste is > 20% and ≤ 70%; and for fully (super) compacted waste is > 70%.

(c) Pack is defined as a seven-pack of 55-gallon drums, a four-pack of 85-gallon drums, or a three-pack of 100-gallon drums.

(d) 0.5-in. spacing modeled for 85- and 100-gallon drums whereas only 0.3 in. was modeled for 55-gallon drums. Requirement set at largest value of 0.5 in. for all cases for consistency.

(e) The limit also applies to partially compacted waste.

9.3 Assumptions

The assumptions below support the design of the waste containers:

1. A 40% to 50% reduction in wall density for all thin-walled containers is assumed to avoid placing controls on wall thickness and the nature of the wall material. This assumption is called out in Section 5.2.3. Visual inspection of payload containers is described in Section 1.4 and Section 2.1.2 of the CH-TRAMPAC [5] as a method of compliance with payload requirements. The WIPP WAC [40] gives requirements for acceptance criterion for containers and a container integrity checklist. The checklist states that operators are to visually examine 100% of the payload container exterior to

determine if the payload container meets the criteria of the WIPP WAC. Examination criteria include questions such as is the container obviously degraded, is there any potentially significant rust or corrosion, are there any split seams, is the container bulged and includes a discussion of the criteria for each question. Thus, the WIPP WAC requirements support this assumption.

2. Deleted.

3. Deleted.

4. A 1.25 cm spacing between SWBs in the two-container model is assumed to stay below the administrative USL. The scenario is conservatively modeled to have the lower fissile material suspended tightly against the lid of the SWB. Crediting a separation distance is reasonable given the unlikelihood that optimally moderated fissile masses in two stacked SWBs would be oriented such that the fissile mass in the lower SWB would be tight up against the lid and directly opposite a second fissile mass in the upper SWB. This assumption is called out in Section A.3.2 and C.4.1 for direct loaded and compacted waste two-container SWB models. This assumption is also supported by the passive design feature on container design in Section 9.1.

10.0 Conclusions

This NCSE has evaluated the handling, storage, and disposal processes for the various CH waste containers allowed at the WIPP. Each waste container and loading is evaluated in the infinite array model and the two-container model, which provides the worst-case, credible model for localized high fissile concentration. (See Sections 5.3.2 and 5.4 for further discussion.) Thus, the subcritical results for both the infinite array models and the two-containers models ensure that a criticality accident at the WIPP due to the storage, handling, and disposal of CH waste containers is not credible. The limits on fissile mass and special reflectors meet or exceed the limits on containers allowed to be transported to the facility in the TRUPACT-II, HalfPACT, or TRUPACT-III shipping packages. The double-contingency principle is met as demonstrated in the contingency analysis of Section 7.0. With the controls listed in Section 9.0, no credible accidental criticality scenarios exist for the WIPP as justified in Sections 7.10 and 8.0. Therefore, there is no need for a criticality accident alarm system or a criticality detection system.

11.0 References

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Appendix A Direct-Loaded Waste Containing Less Than or Equal to 1 Weight Percent Special Reflectors

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Note: Appendix A is unaffected by Revision 8 and no changes were made from the previous revision. Original signatures are on file with WIPP-016 Revision 7.

Note: An extent of condition was performed to Revision 7 of this NCSE to confirm all established limits, assumptions, and judgements were adequately analyzed. For non-compacted waste, Section 5.1.1 of WIPP-016, Revision 7, evaluates the 55-gallon drum array as bounding the 85-gallon and 100-gallon drum arrays from a criticality safety perspective and therefore only models the 55-gallon drum array. WIPP-099 (*Extent of Condition Review for WIPP-016, Rev. 7*) provides additional supportive analysis to justify this assumption. This analysis will be incorporated into a future revision of this NCSE.

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Introduction

This appendix focuses on direct-loaded waste containers containing less than or equal to 1 weight percent (wt%) of special reflector material. Special reflector materials are those that have been shown to increase reactivity above that of a 25% polyethylene/75% water-reflected system and must be limited when mass loading limits are based on this polyethylene/water reflection combination. Containers with no limit on special reflector materials are discussed in Appendix B. Because 1 wt% is considered a contamination level, the special reflector material is modeled homogeneously distributed throughout the container outside of the fissile region. The material modeled is beryllium, which has been shown to result in the highest reactivity when reflecting a plutonium system (*Reactivity Effects of Moderator and Reflector Materials on a Finite Plutonium System* [Neeley et al. 2004]) and the mass modeled is 1 wt% of the maximum weight of the container. Sample MCNP5 input file listings for the models contained in this appendix are included in Section A.7.

A.1 Direct-Loaded Waste Configurations

A.1.1 55-gallon Drums

The direct-loaded 55-gallon drums are modeled with 200 grams of ^{239}Pu mixed with a polyethylene-water moderator, which is 25% by volume polyethylene and 75% by volume water. A mixture of beryllium and polyethylene fills the remainder of the drum reflecting the fissile mass. Polyethylene is modeled at a packing fraction of 25% as determined to bound the packing fraction of direct-loaded (non-machine compacted) waste in the *TRUPACT-II Safety Analysis Report* (DOE-CBFO 2020a). Consequently, the polyethylene density in the reflector is 0.93 g/cm^3 × 0.25 = 0.23 g/cm^3. The amount of beryllium is based on 1 wt% of the maximum gross container loading limit of 1,000 pounds (*Contact-Handled Transuranic Waste Authorized Methods for Payload Control (CH-TRAMPAC)* [DOE-CBFO 2020b]) or 4.55 kilograms, which is rounded up to 5 kilograms beryllium per 55-gallon drum. The beryllium is modeled as homogeneously mixed throughout the polyethylene reflector. The beryllium density varies slightly with the H/Pu ratio as the fissile volume changes but is approximately 0.024 g/cm^3 in the 55-gallon drum. Note that beryllium is slightly more reactive modeled in the reflector than in the moderator as discussed in Section 6.4.3.2.2 of the TRUPACT-II SAR.

The 55-gallon drum dimensions given in Table 2-1 are used in the MCNP5 models. The drum walls are carbon steel (*Standard Specification for Steel, Carbon (0.15 Maximum, Percent), Hot-Rolled Sheet and Strip Commercial* [ASTM A 569]), which is modeled with the composition given in Table 5-5. The theoretical density of carbon steel is 7.86 g/cm^3, but is modeled at 50% of this value, or 3.93 g/cm^3, to allow for fabrication tolerances, localized wall thinning or other degradation, etc. Section 2.1.2 of the CH-TRAMPAC (DOE-CBFO 2020b) requires that the integrity of the container be visually inspected prior to transport to ensure there is no significant rusting such that the 50% value is conservative.

A.1.2 Standard Waste Box

The direct-loaded SWB is modeled with ^{239}Pu and ^{240}Pu as per Section 5.1.3 mixed with polyethylene-water, which is 25% by volume polyethylene and 75% by volume water. A mixture of beryllium and polyethylene fills the remainder of the SWB reflecting the fissile mass. Polyethylene is modeled at a packing fraction of 25% as determined to bound the packing fraction of direct-loaded (non-machine compacted) waste in the TRUPACT-II SAR (DOE-CBFO 2020a). The amount of beryllium is based on 1 wt% of the maximum SWB gross weight of 4,000 pounds (DOE-CBFO 2020b), which equates to 18.14 kilograms of beryllium per SWB. The beryllium is modeled as homogeneously mixed throughout the polyethylene reflector. The beryllium density varies slightly with the H/Pu ratio as the fissile volume

changes, but is approximately 0.0095 g/cm^3. Note that beryllium is slightly more reactive modeled in the reflector than in the moderator as discussed in TRUPACT-II SAR.

The SWB dimensions given in Table 2-3 are used in the MCNP5 model. The carbon-steel (ASTM A 569) container wall is modeled at full thickness; however, the carbon steel is only modeled at 50% of the theoretical density, or 3.93 g/cm^3, to allow for fabrication tolerances, localized wall thinning, or other degradation. The composition of carbon steel used in the models is given in Table 5-5.

A.1.3 Standard Large Box 2

The SLB2 is a large box designed for transport in the TRUPACT-III shipping container. The SLB2 dimensions are discussed in Section 2.2. The SLB2 FGE limit is 325 grams of ^{239}Pu with no ^{240}Pu credited and higher FGE limits are also given with ^{240}Pu credited as per Section 5.1.4 and consistent with the FGE limits for the SWB. The maximum amount of beryllium allowed in the SLB2 is 1 wt% (47.7 kilograms) of the SLB2 gross weight. The beryllium is modeled as homogeneously mixed throughout the polyethylene reflector. The beryllium density varies slightly with the H/Pu ratio as the fissile volume changes but is approximately 0.0064 g/cm^3. Note that beryllium is slightly more reactive modeled in the reflector than in the moderator as discussed in TRUPACT-II SAR.

The SLB2 dimensions given in Table 2-4 are used in the MCNP5 computational model. Following suit with the analyses carried out for the 55-gallon drums and the SWBs, the SLB2 is modeled with carbon steel (ASTM A 569) container walls at full thickness, but at 50% of the theoretical density to account for fabrication tolerances, localized wall thinning, or other degradation. The composition of carbon steel used in the models is given in Table 5-5.

A.2 MCNP5 Direct-Loaded Waste Array Models

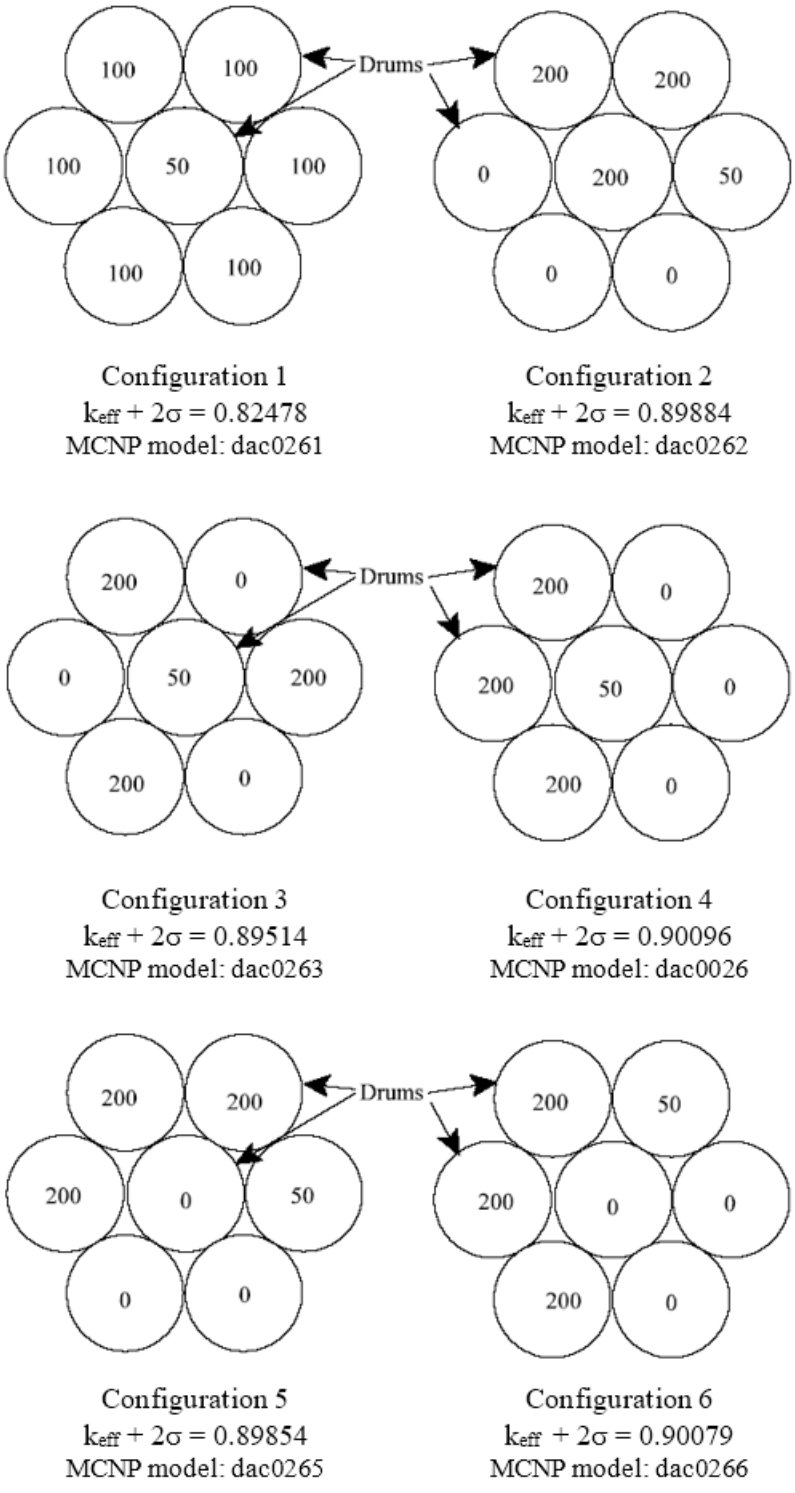
A.2.1 55-gallon Drum Array Model

This section evaluates the disposal array using direct-loaded 55-gallon drums containing particulate beryllium. The particulate beryllium in the drum is considered to be in the form of contamination from compounds such as beryllium oxide or as metal fines or shavings from machining processes. The beryllium material is not in the form of large metal shapes.

The fissile limit on single direct-loaded drums is 200 grams of ^{239}Pu per drum maximum. However, underground array calculations with 200 FGE in each drum are supercritical. A fissile limit is also needed for each seven-pack of drums. A seven-pack limit of 650 FGE, or twice the TRUPACT-II fissile limit of 325 FGE, is analyzed. To determine the effect of the distribution of the fissile material within the seven-pack, six different configurations were examined. The configurations and the resultant $k_{eff} + 2\sigma$ values are displayed in Figure A-1.

These calculations include 5 kilograms of beryllium per drum and model the fissile region at an H/Pu ratio of 1,300. The non-fissile bearing drums also contain 5 kilograms of beryllium spread throughout the drum. (The calculations have the same parameters as file dac0026 in Table A-1 as described in the next paragraph.) Per these results, a more concentrated fissile region within the seven-pack yields a higher reactivity. Placing the 200-FGE drums on the outside of the seven-pack is more reactive than placing them in the center as this increases interaction with the adjacent seven-packs in the infinite array. Configuration 4 is the most reactive, although the arrangements where the fissile mass is concentrated into the fewest drums all have very similar reactivity, and will be used in the subsequent calculations.

Next, a computational analysis was performed where the fissile concentration in the drums in configuration 4 was varied. The fissile material is modeled as a cylinder with an H/D ratio of 1 centered in each drum and the H/Pu ratio is varied. The fissile moderator composition is again 25% by volume polyethylene and 75% by volume water, but the polyethylene dunnage (internal reflector material) composition was varied from 0 to 25% of the theoretical density to determine the sensitivity of the seven-pack array reactivity to this parameter, which affects the interaction of the fissile masses in the array. The beryllium content is held constant at 5 kilograms per drum and is spread homogeneously throughout the drum around the fissile cylinder. The beryllium is not modeled as a moderator based on the results in Chapter 6 of the TRUPACT-II SAR (DOE-CBFO 2020a), which indicates that increasing amounts of beryllium moderation reduces the reactivity when the package is limited to 1 wt% special reflectors. The non-fissile drums in the seven-pack are filled with the same polyethylene density as the fissile bearing drums plus 5 kilograms of beryllium spread throughout the drum. Table A-1 and Figure A-2 give the reactivity of the infinite underground array of 55-gallon drums. The results show that the array reactivity drops sharply with the addition of even 5% polyethylene outside of the fissile region and then increases slightly as more polyethylene is added. Thus, the array is most reactive when interaction is maximized, but the maximum $k_{eff} + 2\sigma$ value is well below the USL of 0.96 at 0.90096. Thus, the fissile limit per seven-pack of 650 FGE with maximum drum contents of 200 FGE and 5 kilograms of beryllium per drum will remain subcritical in the underground storage array.



Note: grams ^{239}Pu modeled shown in each drum. All cases modeled at an H/Pu ratio of 1300 with 5 kg Be.

Figure A-1. 650 Fissile Gram Equivalent Seven-pack Distribution Patterns in Array Model of Direct-loaded Drums

Table A-1. MCNP5 Results for Underground Array of Seven-packs Limited to 650 FGE/Pack

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	File-name	H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	File-name
No Polyethylene					**15% Dense Polyethylene**				
800	0.87891	0.00078	0.88047	dac0016	800	0.70011	0.00086	0.70183	dac1516
900	0.88979	0.00080	0.89139	dac0018	900	0.71363	0.00084	0.71531	dac1518
1000	0.89600	0.00073	0.89746	dac0020	1000	0.72465	0.00079	0.72623	dac1520
1100	0.89889	0.00077	0.90043	dac0022	1100	0.72932	0.00077	0.73086	dac1522
1200	0.89913	0.00071	0.90055	dac0024	1200	0.73502	0.00075	0.73652	dac1524
1300	0.89966	0.00065	0.90096	dac0026	1300	0.73820	0.00072	0.73964	dac1526
1400	0.89480	0.00065	0.89610	dac0028	1400	0.74110	0.00074	0.74258	dac1528
1500	0.89085	0.00064	0.89213	dac0030	1500	0.73906	0.00074	0.74054	dac1530
1600	0.88760	0.00067	0.88894	dac0032	1600	0.73707	0.00070	0.73847	dac1532
1700	0.88122	0.00059	0.88240	dac0034	1700	0.73613	0.00071	0.73755	dac1534
1800	0.87414	0.00061	0.87536	dac0036	1800	0.73448	0.00065	0.73578	dac1536
5% Dense Polyethylene					**20% Dense Polyethylene**				
800	0.71580	0.00081	0.71742	dac0516	800	0.70715	0.00084	0.70883	dac2016
900	0.73081	0.00079	0.73239	dac0518	900	0.71957	0.00071	0.72099	dac2018
1000	0.74217	0.00072	0.74361	dac0520	1000	0.72898	0.00081	0.73060	dac2020
1100	0.75102	0.00072	0.75246	dac0522	1100	0.73474	0.00085	0.73644	dac2022
1200	0.75556	0.00075	0.75706	dac0524	1200	0.73652	0.00079	0.73810	dac2024
1300	0.75669	0.00073	0.75815	dac0526	1300	0.74166	0.00074	0.74314	dac2026
1400	0.76108	0.00069	0.76246	dac0528	1400	0.74020	0.00075	0.74170	dac2028
1500	0.76212	0.00071	0.76354	dac0530	1500	0.74078	0.00070	0.74218	dac2030
1600	0.76087	0.00067	0.76221	dac0532	1600	0.73870	0.00076	0.74022	dac2032
1700	0.75957	0.00070	0.76097	dac0534	1700	0.73727	0.00067	0.73861	dac2034
1800	0.75724	0.00065	0.75854	dac0536	1800	0.73360	0.00072	0.73504	dac2036
10% Dense Polyethylene					**25% Dense Polyethylene**				
800	0.70065	0.00081	0.70227	dac1016	800	0.71594	0.00082	0.71758	dac2516
900	0.71335	0.00079	0.71493	dac1018	900	0.72550	0.00086	0.72722	dac2518
1000	0.72506	0.00082	0.72670	dac1020	1000	0.73576	0.00085	0.73746	dac2520
1100	0.73187	0.00077	0.73341	dac1022	1100	0.74215	0.00080	0.74375	dac2522
1200	0.73779	0.00072	0.73923	dac1024	1200	0.74464	0.00074	0.74612	dac2524
1300	0.74097	0.00077	0.74251	dac1026	1300	0.74625	0.00071	0.74767	dac2526
1400	0.74309	0.00073	0.74455	dac1028	1400	0.74524	0.00065	0.74654	dac2528
1500	0.74256	0.00068	0.74392	dac1030	1500	0.74273	0.00075	0.74423	dac2530
1600	0.74379	0.00071	0.74521	dac1032	1600	0.74300	0.00065	0.74430	dac2532
1700	0.74103	0.00067	0.74237	dac1034	1700	0.73862	0.00069	0.74000	dac2534
1800	0.74066	0.00064	0.74194	dac1036	1800	0.73505	0.00059	0.73623	dac2536

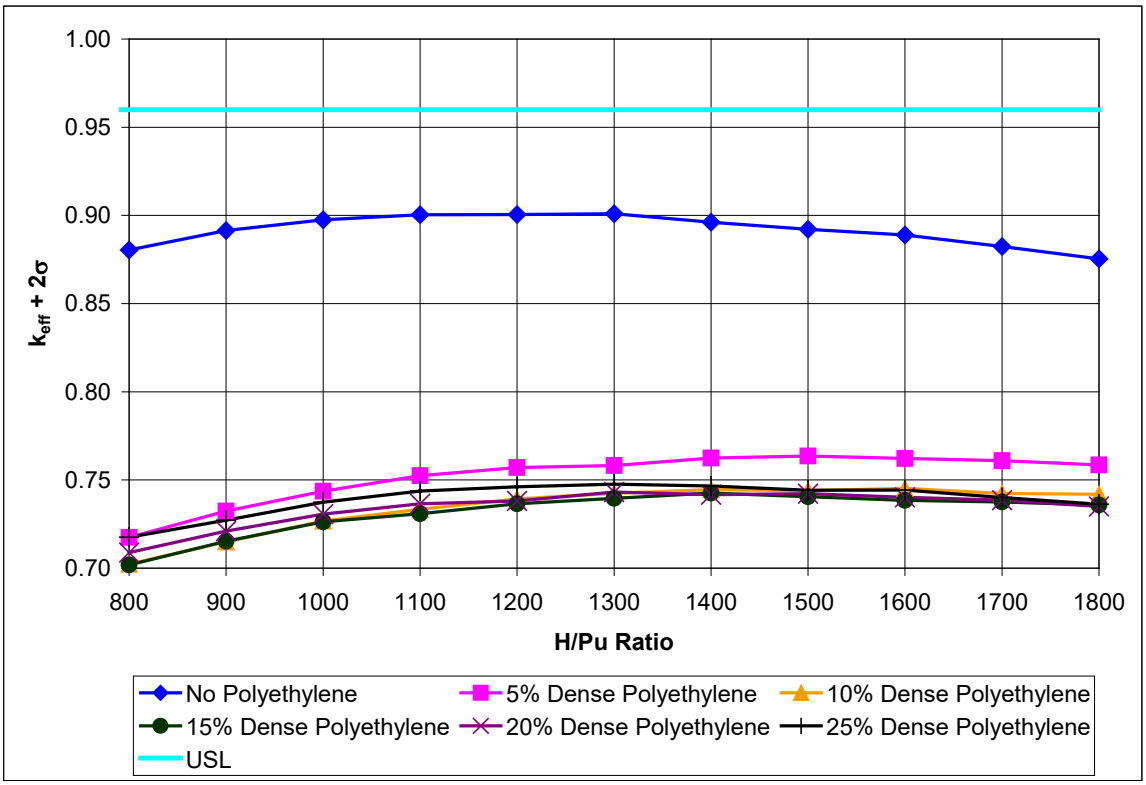


Figure A-2. Underground Array Reactivity for Direct-loaded 55-gallon Drums at 650 Fissile Gram Equivalents per Seven-pack as a Function of Polyethylene Dunnage Density

A.2.2 Standard Waste Box Array Model

The SWB underground array model includes a three-tier stack of SWBs as illustrated in Figure A-3. A close-fitting hexagon is placed around the SWB stack and the sides of hexagon infinitely reflected to simulate a tight-packed array that is infinite in x and y. The compositions of the fissile mass (plutonium and moderator mixture) are taken from Table 5-3. The fissile masses were modeled as cylindrical units with an H/D ratio of 1, and the mass located in the center of the SWB. The cylinder radius is given in Table A-2. Based on the 55-gallon results from the previous section, the reflector consisted of beryllium only spread throughout the container to maximize reactivity. For verification the most reactive case was evaluated with a mixture of beryllium and 25% polyethylene. As shown by the SWB array results in Table A-2 and Figure A-4, beryllium reflection without the 25% dense polyethylene is most reactive. A maximum reactivity of 0.88393 occurs for 380 FGE with 25 grams of ^{240}Pu at an H/Pu ratio of 1,200, which is well below the USL of 0.96.

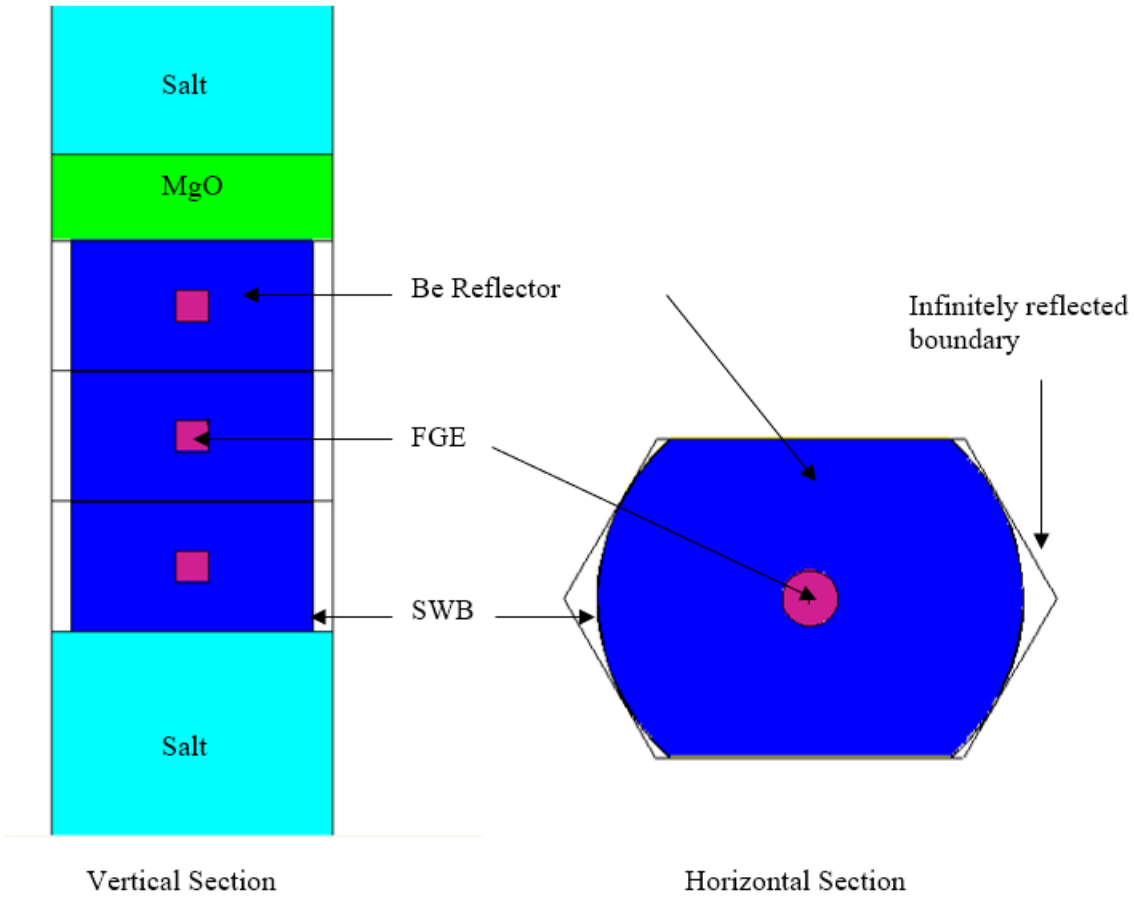


Figure A-3. Sample SWB Array Model Layout

Table A-2. MCNP5 Results for Underground Array of Standard Waste Box Containers

H/Pu Ratio	Cylinder Radius	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
325 FGE with 0 g ^{240}Pu					
900	11.4328	0.85268	0.00054	0.85376	n0swa09
1000	11.8898	0.86099	0.00053	0.86205	n0swa10
1100	12.3142	0.86579	0.00048	0.86675	n0swa11
1200	12.7112	0.86667	0.00046	0.86759	n0swa12
1300	13.0848	0.86608	0.00049	0.86706	n0swa13
1400	13.4382	0.86577	0.00051	0.86679	n0swa14
340 FGE with 5 g ^{240}Pu					
900	12.0701	0.85902	0.00039	0.85980	0psna09
1000	12.5009	0.86716	0.00053	0.86822	0psna10
1100	12.9039	0.87067	0.00052	0.87171	0psna11
1200	13.2831	0.87385	0.00051	0.87487	0psna12
1300	13.6419	0.87312	0.00050	0.87412	0psna13
1400	13.9827	0.87162	0.00049	0.87260	0psna14
360 FGE with 15 g ^{240}Pu					
900	12.3024	0.86360	0.00055	0.86470	1psna09
1000	12.7415	0.87108	0.00054	0.87216	1psna10
1100	13.1522	0.87605	0.00052	0.87709	1psna11
1200	13.5388	0.87789	0.00050	0.87889	1psna12
1300	13.9044	0.87761	0.00045	0.87851	1psna13
1400	14.2518	0.87682	0.00047	0.87776	1psna14
380 FGE with 25 g ^{240}Pu					
900	12.5263	0.86905	0.00055	0.87015	2psna09
1000	12.9734	0.87697	0.00053	0.87803	2psna10
1100	13.3915	0.88092	0.00052	0.88196	2psna11
1200	13.7851	0.88281	0.00056	0.88393	2psna12
1300	14.1574	0.88292	0.00043	0.88378	2psna13
1400	14.5111	0.88210	0.00047	0.88304	2psna14
380 FGE with 25 g ^{240}Pu and Mixed 25% Polyethylene/18.14 kg Be reflection					
900	12.5263	0.84417	0.00055	0.84527	2pswa09
1000	12.9734	0.84992	0.00056	0.85104	2pswa10
1100	13.3915	0.85093	0.00054	0.85201	2pswa11
1200	13.7851	0.85289	0.00053	0.85395	2pswa12
1300	14.1574	0.85166	0.00052	0.85270	2pswa13
1400	14.5111	0.84798	0.00050	0.84898	2pswa14

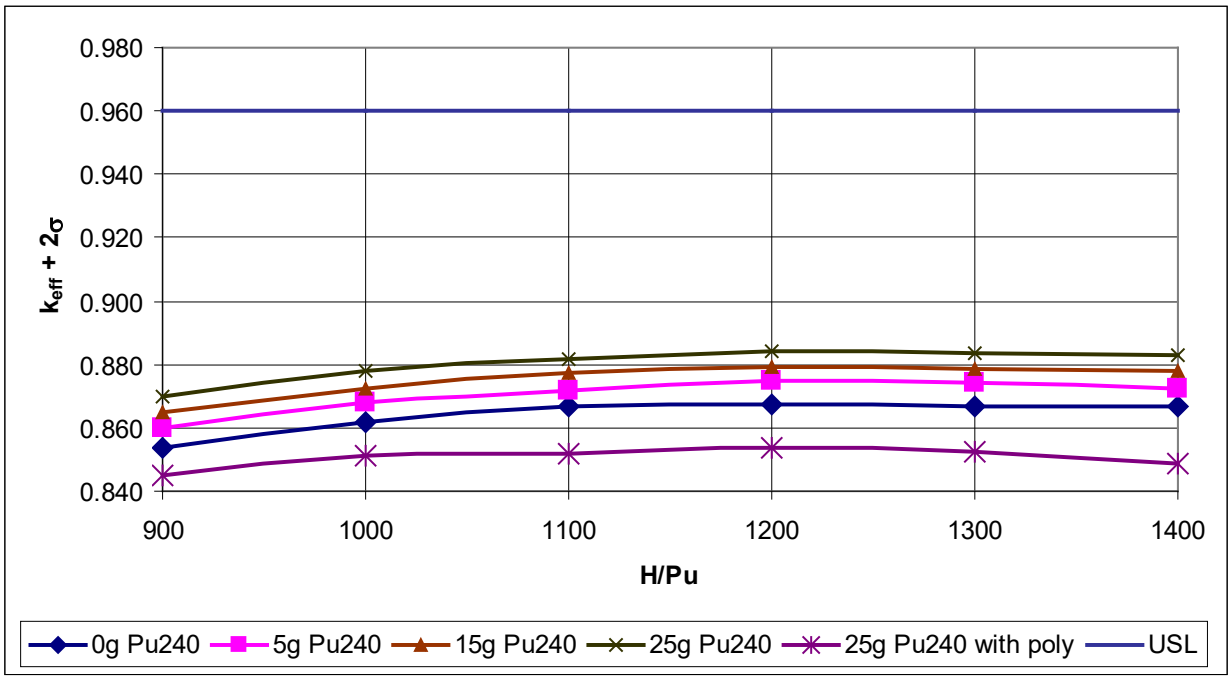


Figure A-4 Underground Array Reactivity for Standard Waste Box Containers

A.2.3 Standard Large Box 2 Array

The SLB2 is a larger container than the SWB but the total fissile mass is restricted to the same as that of a SWB. Since the SLB2 has more reflector volume around the fissile mass and the distance between the masses in adjacent containers is greater, the interaction between SLB2s is less than between SWBs. Thus, an SLB2 array is bound by the SWB array analysis in the previous subsection and a SLB2 array is not explicitly modeled.

A.3 MCNP5 Two-container Direct-loaded Waste Models

The geometry of the two-container model positions the fissile mass at the top of the bottom container and at the bottom of the top container. Consequently, the fissile regions are only separated by the container lid and bottom and any inherent spacing that may be built into the lid or bottom. The fissile mass in each container is modeled as a cylinder with an H/D ratio of 0.5 whereas resulting cylinder in the two containers has an optimum H/D ratio of 1. Figure A-5 shows SWBs in the modeled two-container configuration. The 55-gallon drums and SWBs of direct-loaded waste are evaluated in this configuration.

Three types of materials are analyzed as tight reflectors around the containers: concrete, MgO, and salt. In each case, the material is 300 centimeters thick on all sides of the container stack, effectively creating an infinite reflector. Concrete and salt are analyzed to represent reflection from above-ground facility structures and the underground repository, respectively. MgO is also analyzed because MgO may be placed in columns in the underground disposal array in addition to on top of the three-high container stacks. The material compositions used for these reflector materials are described in Section 5.2.4.

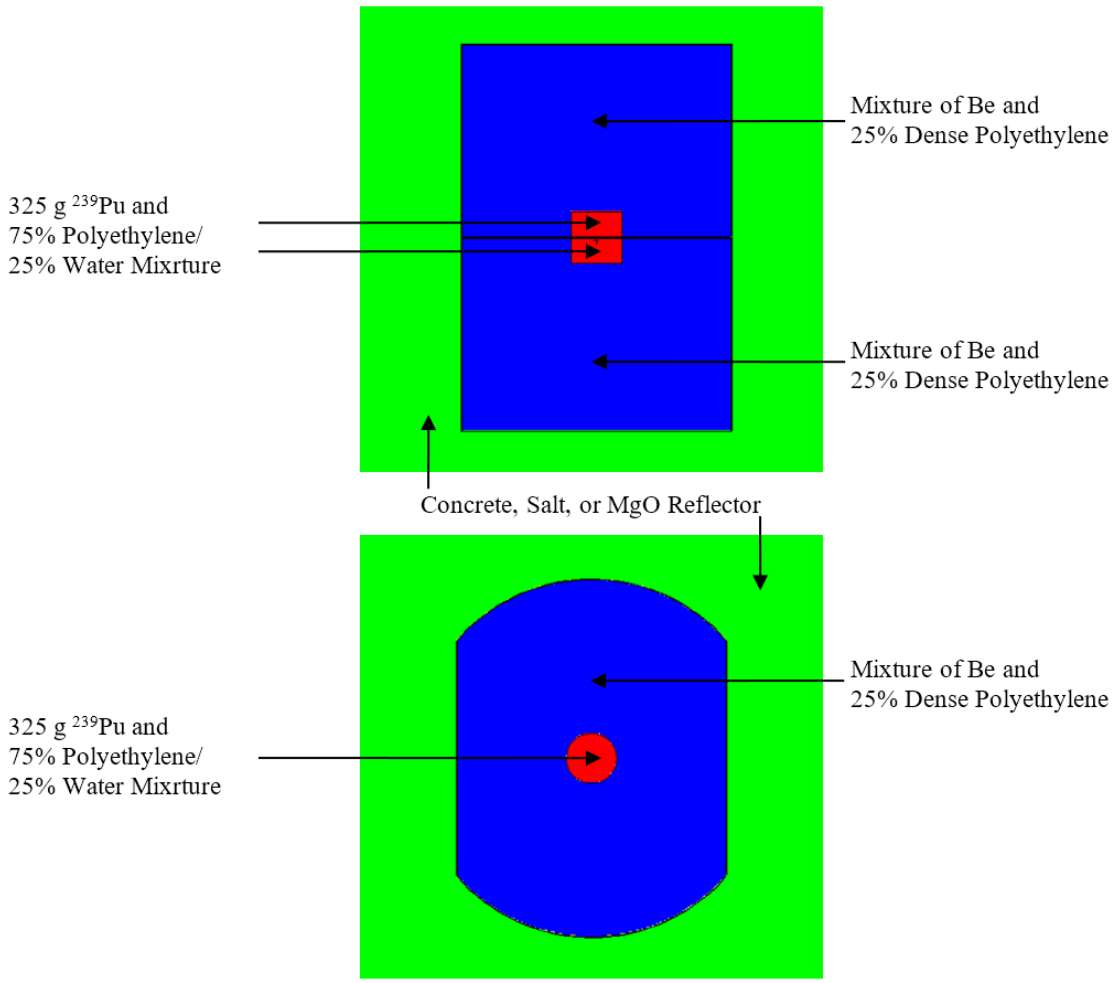


Figure A-5. Example Two-Container Model Configuration Showing Two SWBs

A.3.1 55-gallon Drum Two-Container Model

The parameters for the fissile material input into MCNP5 are given in Table 5-3 and Table A-3 for the 55-gallon drum two-container model. The fissile material is modeled in a cylinder with an H/D ratio of 0.5 such that the combined fissile masses in the two containers have an optimized H/D ratio of 1. The results for the model as a function of H/Pu ratio in the fissile region are also given in Table A-3. All cases are well below the USL with the highest $k_{eff} + 2\sigma$ value being less than 0.89. Thus, 55-gallon drums containing 200 FGE will remain subcritical in the two-container configuration.

Table A-3. MCNP5 Results for 55-gallon Drum Two-Container Model at 200 FGE

H/Pu Ratio	Reflector	Cylinder Radius & Height (cm)	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
800	Concrete	12.25214	0.87265	0.00096	0.87458	c55g800
900	Concrete	12.74192	0.87910	0.00094	0.88098	c55g900
1000	Concrete	13.19668	0.88398	0.00095	0.88588	c55g100
1100	Concrete	13.62210	0.88241	0.00094	0.88429	c55g110
1200	Concrete	14.02248	0.88183	0.00088	0.88359	c55g120
800	MgO	12.25214	0.87461	0.00098	0.87657	m55g800
900	MgO	12.74192	0.88228	0.00096	0.88420	m55g900
1000	MgO	13.19668	0.88433	0.00094	0.88622	m55g100
1100	MgO	13.62210	0.88402	0.00094	0.88590	m55g110
1200	MgO	14.02248	0.88194	0.00087	0.88369	m55g120
800	Salt	12.25214	0.87256	0.00101	0.87459	s55g800
900	Salt	12.74192	0.87796	0.00096	0.87988	s55g900
1000	Salt	13.19668	0.88087	0.00093	0.88272	s55g100
1100	Salt	13.62210	0.88250	0.00090	0.88431	s55g110
1200	Salt	14.02248	0.88076	0.00088	0.88251	s55g120

A.3.2 Standard Waste Box Two-Container Model

The parameters for the fissile material input into MCNP5 for the two-container SWB model was given previously in Table 5-3. Table A-4 shows the initial SWB results with a 50% dense wall, where many of the cases exceed the USL of 0.97. Two alternatives can be evaluated to address the cases that are above the USL. First, consider the assumed steel degradation of 50%. If the degradation were slightly less, such as 40%, more steel would be present to reduce the interaction of the two fissile masses. Table A-5 shows that crediting 60% of the steel wall, which still allows for 40% degradation, maintains the reactivity below the USL without administrative margin of 0.97 for all cases.

Second, consider the conservative modeling assumption that the fissile mass in the lower container will be suspended in the SWB tightly against the lid. A parametric study on the separation distance between the fissile masses was performed to determine the sensitivity of the reactivity to this distance. The results given in Table A-6 are for an MgO-reflected two-container model. (Only MgO was considered as the calculations showed that the various reflectors resulted in statistically identical results.) These results indicate that k_{eff} is reduced significantly with small separation distances. For example, an additional one-centimeter of separation between the fissile masses reduces the $k_{eff} + 2\sigma$ value below the USL of 0.96 for an FGE with 325 with no ^{240}Pu. Crediting a separation distance is reasonable given the unlikelihood that optimally moderated fissile masses in two stacked SWBs would be oriented such that the fissile mass in the lower SWB would be tight up against the lid and directly opposite a second fissile mass in the upper SWB. Figure A-6 illustrates a separation distance of 1.25 centimeters. As shown in Table A-7 and Table A-8 and plotted in Figure A-7 and Figure A-8, a separation of 1.25 centimeters is sufficient to maintain the SWBs in a two-container configuration below the USL with the highest $k_{eff} + 2\sigma$ value being 0.95805 (380 FGE with 25 grams of ^{240}Pu, MgO reflection, H/Pu ratio of 1000).

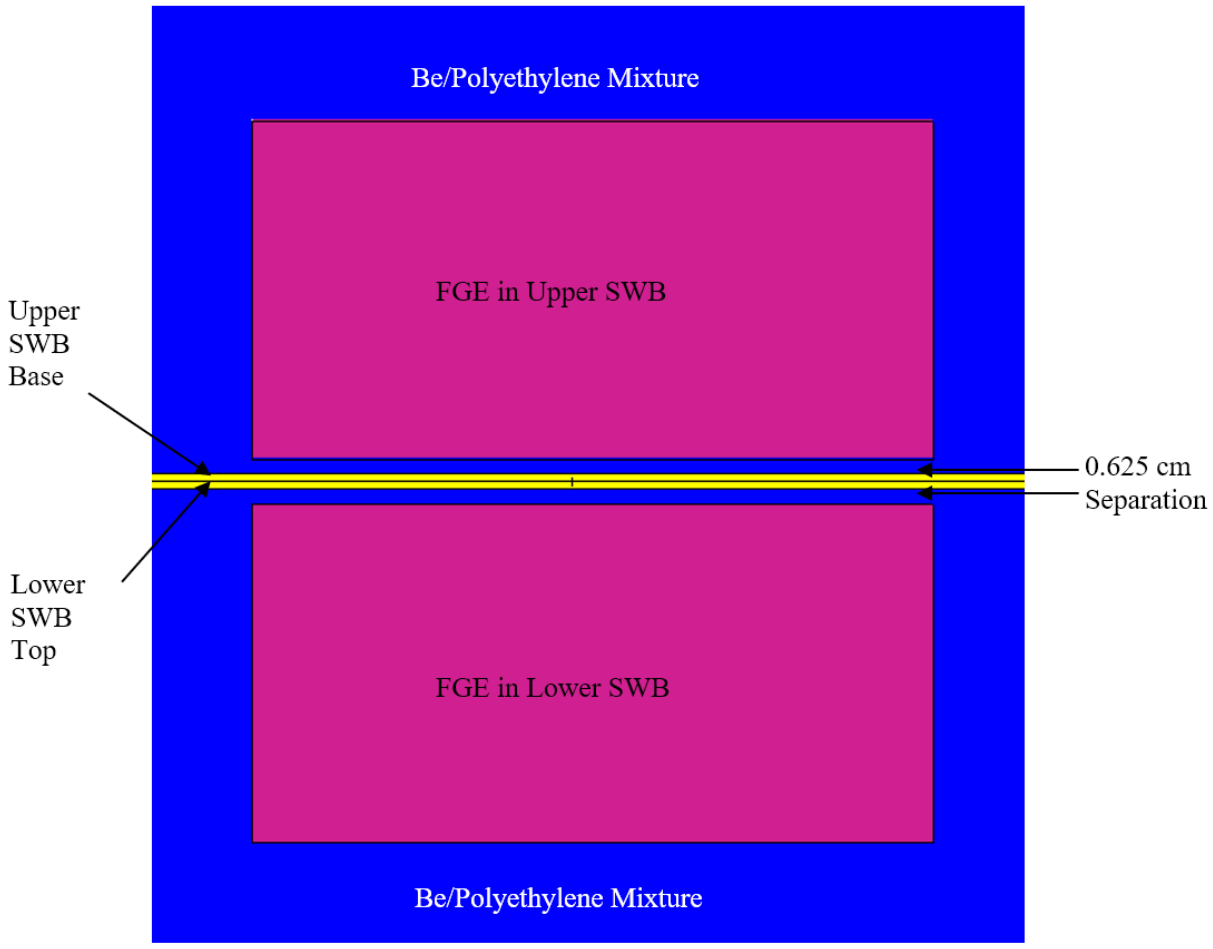


Figure A-6. Centimeter Additional Separation between Fissile Mass in SWB Two-Container Model

Table A-4. Results for Two-Container SWB Model at 325 FGE with 50% Steel Wall Density Modeled

H/Pu Ratio	Reflector	Cylinder Radius (cm)	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
325 FGE with 0 g ^{240}Pu						
700	Concrete	13.7785	0.96278	0.00097	0.96473	cswb700
800	Concrete	14.4044	0.97092	0.00097	0.97286	cswb800
900	Concrete	14.9803	0.97115	0.00093	0.97300	cswb900
1000	Concrete	15.5149	0.96861	0.00094	0.97049	cswb100
1100	Concrete	16.0151	0.96868	0.00093	0.97053	cswb110
1200	Concrete	16.4858	0.96268	0.00090	0.96449	cswb120
700	MgO	13.7785	0.96234	0.00101	0.96437	mswb700
800	MgO	14.4044	0.96827	0.00095	0.97017	mswb800
900	MgO	14.9803	0.97189	0.00097	0.97382	mswb900
1000	MgO	15.5149	0.97183	0.00094	0.97372	mswb100
1100	MgO	16.0151	0.96878	0.00087	0.97051	mswb110
1200	MgO	16.4858	0.96289	0.00089	0.96467	mswb120

Table A-4. Results for Two-Container SWB Model at 325 FGE with 50% Steel Wall Density Modeled

H/Pu Ratio	Reflector	Cylinder Radius (cm)	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
700	Salt	13.7785	0.96236	0.00104	0.96444	sswb700
800	Salt	14.4044	0.96899	0.00096	0.97091	sswb800
900	Salt	14.9803	0.97318	0.00094	0.97505	sswb900
1000	Salt	15.5149	0.96911	0.00092	0.97095	sswb100
1100	Salt	16.0151	0.96755	0.00089	0.96934	sswb110
1200	Salt	16.4858	0.96231	0.00088	0.96406	sswb120

Table A-5. Results for Two-Container SWB Model at 325 FGE with 60% Steel Wall Density Modeled

H/Pu Ratio	Reflector	Cylinder Radius (cm)	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
325 FGE with 0 g ^{240}Pu						
700	Concrete	13.7785	0.95809	0.00105	0.96019	cswb706
800	Concrete	14.4044	0.96746	0.00089	0.96924	cswb806
900	Concrete	14.9803	0.96816	0.00070	0.96957	cswb906
1000	Concrete	15.5149	0.96823	0.00068	0.96960	cswb106
1100	Concrete	16.0151	0.96525	0.00088	0.96701	cswb116
1200	Concrete	16.4858	0.95944	0.00083	0.96111	cswb126
700	MgO	13.7785	0.96082	0.00105	0.96291	mswb706
800	MgO	14.4044	0.96671	0.00100	0.96872	mswb806
900	MgO	14.9803	0.96774	0.00086	0.96947	mswb906
1000	MgO	15.5149	0.96905	0.00036	0.96976	mswb106
1100	MgO	16.0151	0.96501	0.00093	0.96686	mswb116
1200	MgO	16.4858	0.96166	0.00088	0.96343	mswb126
700	Salt	13.7785	0.96075	0.00103	0.96281	sswb706
800	Salt	14.4044	0.96569	0.00098	0.96765	sswb806
900	Salt	14.9803	0.96785	0.00080	0.96946	sswb906
1000	Salt	15.5149	0.96750	0.00086	0.96921	sswb106
1100	Salt	16.0151	0.96487	0.00090	0.96668	sswb116
1200	Salt	16.4858	0.96114	0.00089	0.96291	sswb126

Table A-6. Parametric Study on Separation Distance in MgO Reflected Two-Container SWB Model

Distance Between Fissile Masses (cm)	Optimum H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
325 FGE with 0 g ^{240}Pu					
0	1000	0.96905	0.00036	0.96976	mswb106
0.5	900	0.96305	0.00057	0.96419	swm0518
1.0	1000	0.95656	0.00053	0.95762	swm1020
1.5	900	0.94872	0.00057	0.94986	swm1518
2.0	1000	0.94158	0.00053	0.94264	swm2020

Table A-7. MCNP5 Results for Two-Container Model of SWBs with MgO Reflection and 1.25 cm Separation Distance

H/Pu Ratio	Cylinder Radius (cm)	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
325 FGE with 0 g ^{240}Pu					
700	13.7785	0.93991	0.00099	0.94189	00sm207
800	14.4044	0.94697	0.00098	0.94893	00sm208
900	14.9803	0.94944	0.00095	0.95134	00sm209
1000	15.5149	0.95103	0.00096	0.95295	00sm210
1100	16.0151	0.94949	0.00090	0.95129	00sm211
1200	16.4858	0.94389	0.00085	0.94559	00sm212
340 FGE with 5 g ^{240}Pu					
700	13.9874	0.94341	0.00101	0.94543	0psm207
800	14.6228	0.94880	0.00100	0.95080	0psm208
900	15.2074	0.95355	0.00092	0.95539	0psm209
1000	15.7501	0.95424	0.00097	0.95618	0psm210
1100	16.2578	0.95220	0.00090	0.95400	0psm211
1200	16.7357	0.94924	0.00090	0.95104	0psm212
360 FGE with 15 g ^{240}Pu					
700	14.2567	0.94058	0.00097	0.94252	1psm207
800	14.9044	0.94947	0.00099	0.95145	1psm208
900	15.5001	0.95212	0.00093	0.95398	1psm209
1000	16.0533	0.95519	0.00089	0.95697	1psm210
1100	16.5708	0.95229	0.00093	0.95415	1psm211
1200	17.0578	0.95028	0.00094	0.95216	1psm212
380 FGE with 25 g ^{240}Pu					
700	14.5162	0.94159	0.00105	0.94369	2psm207
800	15.1756	0.94922	0.00100	0.95122	2psm208
900	15.7822	0.95275	0.00099	0.95473	2psm209
1000	16.3454	0.95627	0.00089	0.95805	2psm210
1100	16.8723	0.95441	0.00095	0.95631	2psm211
1200	17.3682	0.94952	0.00088	0.95128	2psm212

Table A-8. Results for Two-Container 380 FGE with 25 g ^{240}Pu FGE SWB Model 50% Steel Wall Density Modeled

H/Pu Ratio	Reflector	k_{eff}	σ	k_{eff} + 2σ	Filename
380 FGE with 25 g ^{240}Pu					
700	Concrete	0.94147	0.00098	0.94343	2psc207
800	Concrete	0.94951	0.00095	0.95141	2psc208
900	Concrete	0.95433	0.00097	0.95627	2psc209
1000	Concrete	0.95446	0.00093	0.95632	2psc210
1100	Concrete	0.95352	0.00080	0.95512	2psc211
1200	Concrete	0.95053	0.00091	0.95235	2psc212
700	MgO	0.94159	0.00105	0.94369	2psm207
800	MgO	0.94922	0.00100	0.95122	2psm208
900	MgO	0.95275	0.00099	0.95473	2psm209
1000	MgO	0.95627	0.00089	0.95805	2psm210
1100	MgO	0.95441	0.00095	0.95631	2psm211
1200	MgO	0.94952	0.00088	0.95128	2psm212
700	Salt	0.94032	0.00097	0.94226	2pss207
800	Salt	0.95014	0.00098	0.95210	2pss208
900	Salt	0.95592	0.00086	0.95764	2pss209
1000	Salt	0.95588	0.00094	0.95776	2pss210
1100	Salt	0.95466	0.00094	0.95654	2pss211
1200	Salt	0.95119	0.00090	0.95299	2pss212

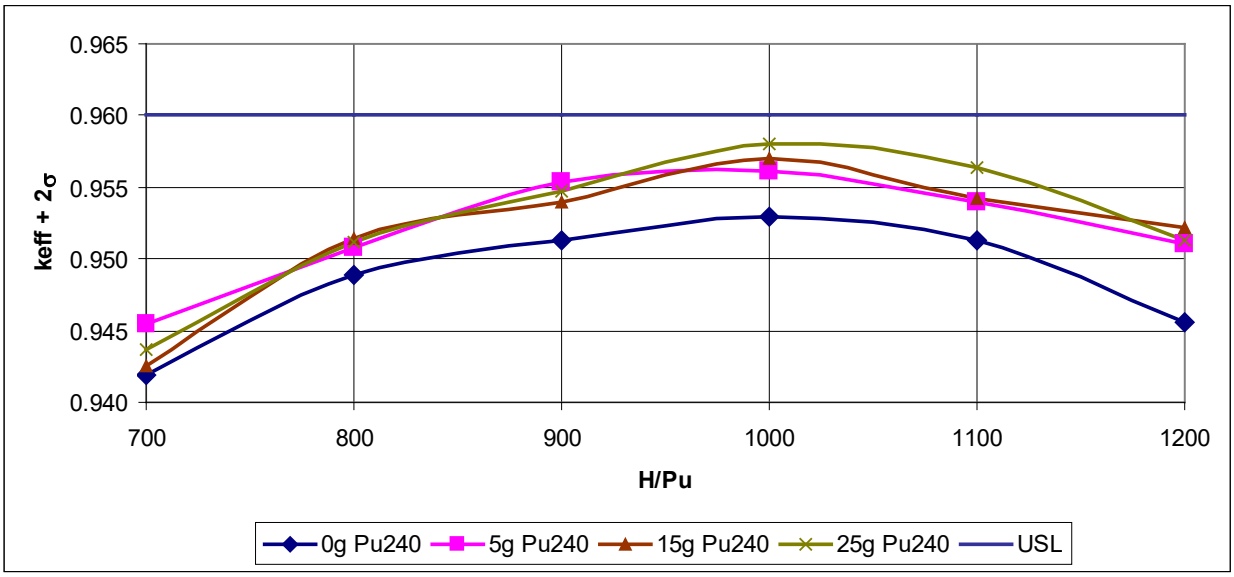


Figure A-7. Reactivity for Standard Waste Box Containers in Two-Container Model with MgO Reflection

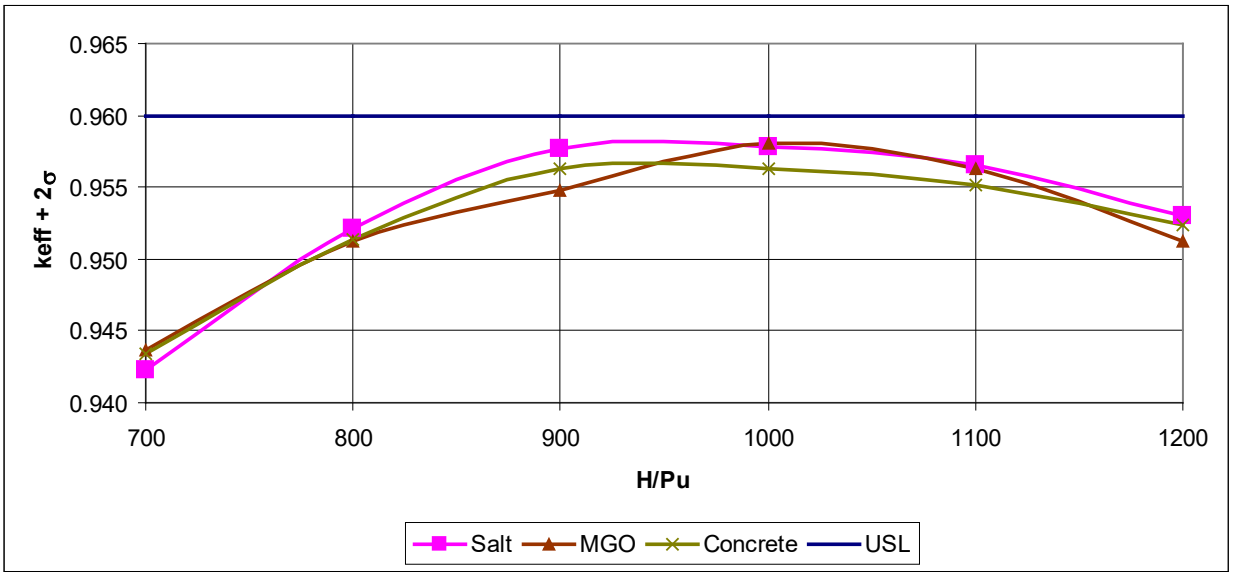


Figure A-8. Maximum Reactivity for SWBs in Two-Container Model with Different Reflectors

A.3.3 Standard Large Box 2 Two-Container Model

The SLB2 two-container model evaluates an SWB stacked on top of an SLB2 as shown in Figure A-9. This configuration was selected since a two-container SLB2 stack is not feasible due to the height of the SLB2. Note that instead of positioning the SWB on the SLB2 vertical centerline, the FGE masses are located off center as close to the corner as possible to maximize reflection while maintaining position on the SWB axial centerline. In addition, the 1.5" design spacing that would normally be present between the SWB and the SLB2 (due to bumpers on the SLB2 lid) is conservatively replaced with a 1 cm separation between the upper FGE and the SWB base. Crediting a 1 cm gap is reasonable given the unlikelihood that optimally moderated fissile masses would be oriented such that the fissile mass in the SLB2 would be tight up against the lid and directly opposite a second fissile mass in the SWB. The fissile mass in each container is modeled as a cylinder with an H/D ratio of 0.5 such that the resulting cylinder in the two containers has an optimum H/D ratio of 1. A 50% dense wall at full thickness is modeled to account for possible wall degradation.

The fissile units in both containers are modeled at their FGE limits (per Sections 5.1.3 and 5.1.4) moderated by a polyethylene-water mixture that is 75% by volume water and 25% by volume polyethylene. The internal reflector composition for the SLB2 is a mixture of 47.7 kilograms of beryllium mixed with 25% dense polyethylene. A similar composition is used for the SWB internal reflection state, but with a lower beryllium content (18.14 kilograms). The H/Pu ratio in the fissile material was varied in the model with concrete external reflection; then to account for the other external reflectors that exist during handling and disposal, the reflector was changed to MgO and salt in the optimally moderated case. The k_{eff} value was comparable with each reflector material. The results of the SLB2-SWB two-container computations are summarized in Table A-9, Table A-10, Figure A-10 and Figure A-11. All cases are below the USL.

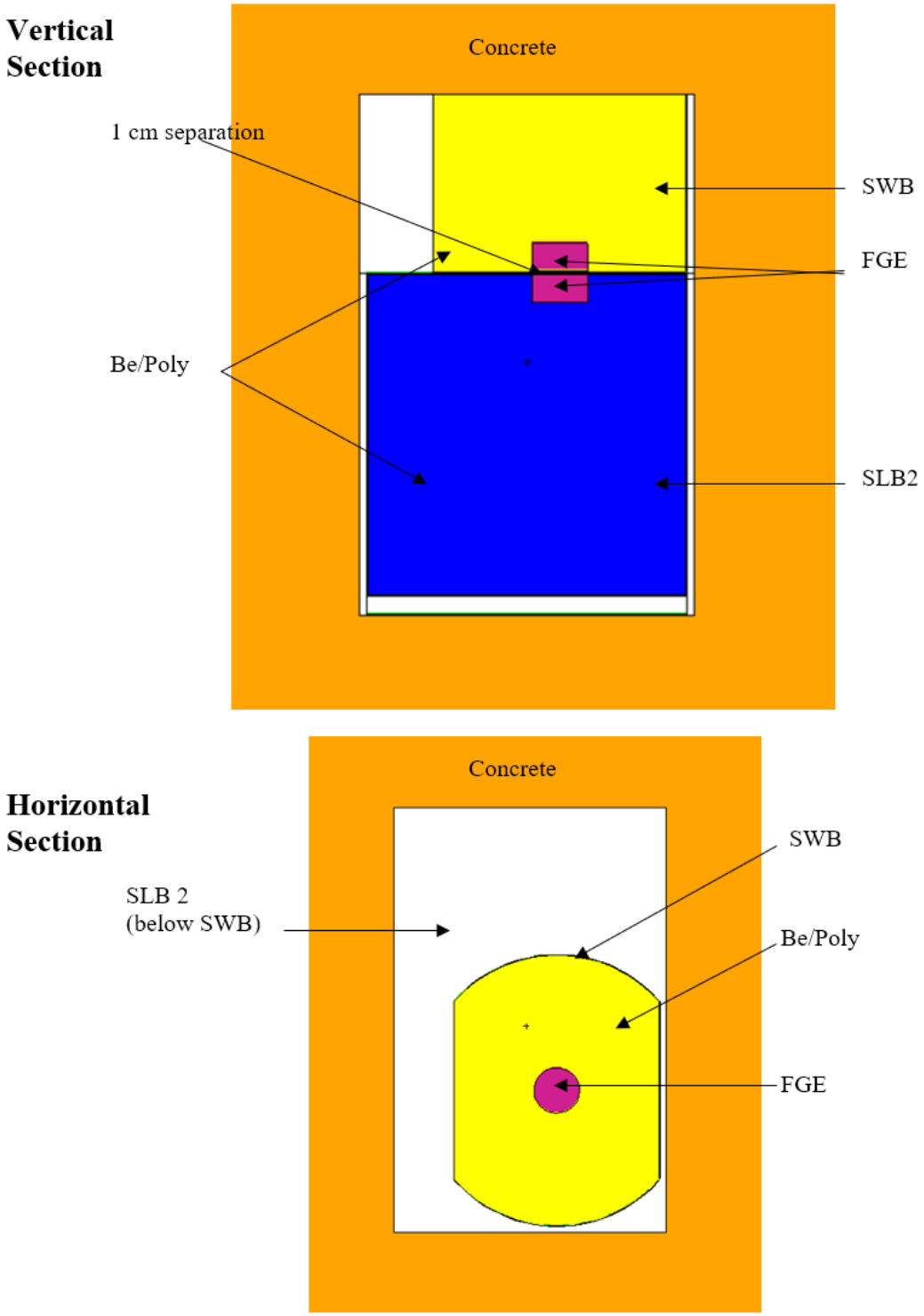


Figure A-9. SLB2-SWB Two-container Model

Table A-9. MCNP5 Results for SLB2-SWB Two- Container Model With Concrete External Reflector

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
325 FGE with 0 g ^{240}Pu				
800	0.94563	0.00082	0.94727	001sc08
900	0.94939	0.00077	0.95093	001sc09
1000	0.94955	0.00081	0.95117	001sc10
1100	0.94721	0.00077	0.94875	001sc11
1200	0.94404	0.00075	0.94554	001sc12
340 FGE with 5 g ^{240}Pu				
800	0.94840	0.00080	0.95000	0p1sc08
900	0.95126	0.00082	0.95290	0p1sc09
1000	0.95265	0.00075	0.95415	0p1sc10
1100	0.94916	0.00084	0.95084	0p1sc11
1200	0.94578	0.00079	0.94736	0p1sc12
360 FGE with 15 g ^{240}Pu				
800	0.94584	0.00093	0.94770	1p1sc08
900	0.95194	0.00081	0.95356	1p1sc09
1000	0.95258	0.00082	0.95422	1p1sc10
1100	0.94994	0.00086	0.95166	1p1sc11
1200	0.94755	0.00076	0.94907	1p1sc12
380 FGE with 25 g ^{240}Pu				
800	0.94836	0.00094	0.95024	2p1sc08
900	0.95141	0.00077	0.95295	2p1sc09
1000	0.95466	0.00083	0.95632	2p1sc10
1100	0.95288	0.00082	0.95452	2p1sc11
1200	0.95006	0.00077	0.95160	2p1sc12

Table A-10. MCNP5 Results for SLB2-SWB 380 FGE with 25 g ^{240}Pu Two-Container Model with Different External Reflectors

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
Concrete Reflector				
800	0.94836	0.00094	0.95024	2p1sc08
900	0.95141	0.00077	0.95295	2p1sc09
1000	0.95466	0.00083	0.95632	2p1sc10
1100	0.95288	0.00082	0.95452	2p1sc11
1200	0.95006	0.00077	0.95160	2p1sc12
Salt Reflector				
800	0.94850	0.00086	0.95022	2p1ss08
900	0.95339	0.00062	0.95463	2p1ss09
1000	0.95372	0.00061	0.95494	2p1ss10
1100	0.95253	0.00080	0.95413	2p1ss11
1200	0.94746	0.00078	0.94902	2p1ss12
MgO Reflector				
800	0.94845	0.00080	0.95005	2p1sm08
900	0.95102	0.00080	0.95262	2p1sm09
1000	0.95489	0.00080	0.95649	2p1sm10
1100	0.95196	0.00073	0.95342	2p1sm11
1200	0.94826	0.00069	0.94964	2p1sm12

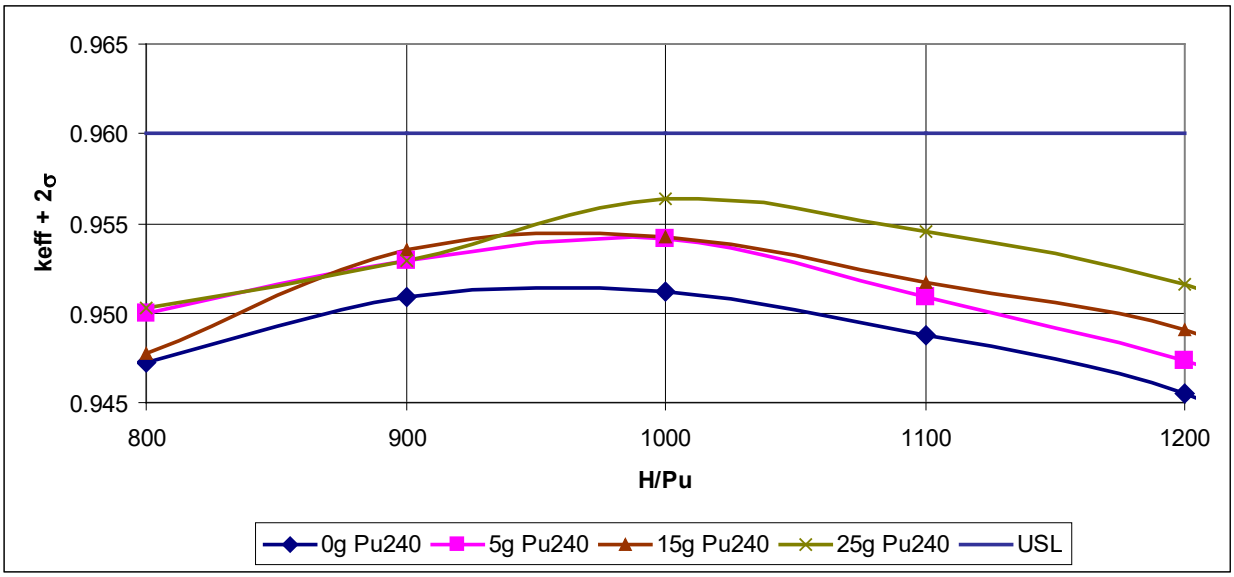


Figure A-10. System Reactivity for Concrete Reflected SLB2-SWB Two-Container Model

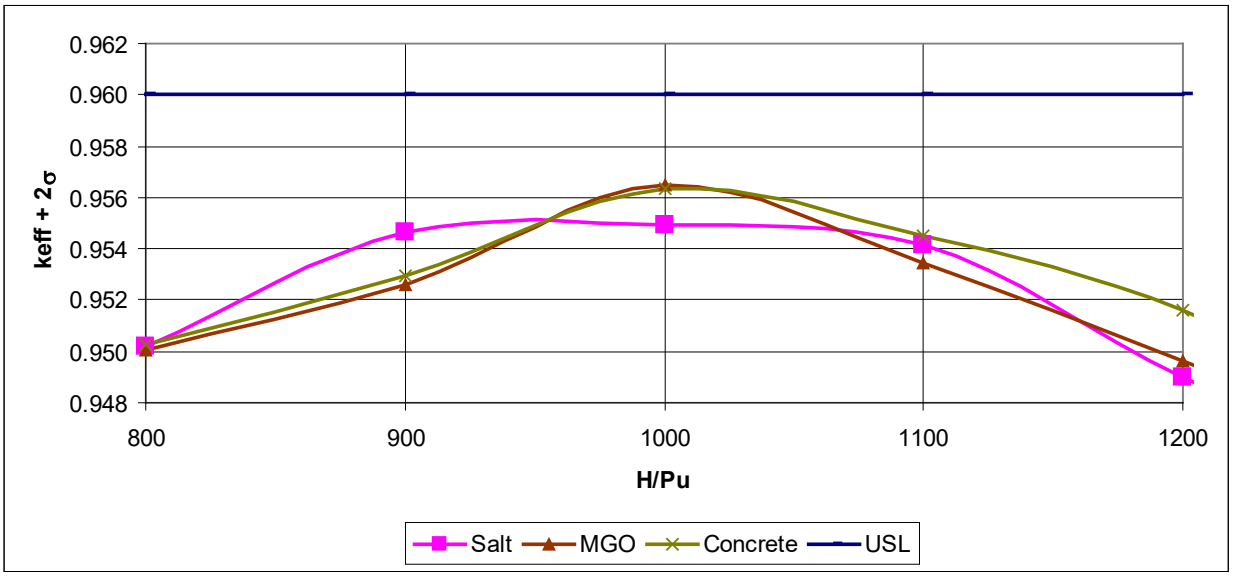


Figure A-11. System Reactivity for 380 g ^{239}Pu with 25 g ^{240}Pu SLB2-SWB Two-Container Model with Different Reflectors

A.4 MCNP5 Direct-loaded Waste Contingency Models

Contingent conditions were also evaluated for the underground storage array of various direct-loaded waste packages containing non-compacted fissile-bearing waste. Since the two-container models are sufficiently conservative to bound any contingency of more realistic or expected conditions related to the interaction between small numbers of containers, only array configurations with centrally located fissile material will be considered.

The contingency states evaluated in this section consisted of overstacking, overbatching, loss of geometry, and sprinkler system activation events. The contingency analyses for the various waste configurations consisted of:

- An overstacking event where the seven-packs were stacked four tiers high;
- An FGE overbatching event where the fissile mass in one container in the middle tier of the stack is increased to 150% of its mass limit;
- An overbatching event where one of the fissile-bearing drums in the middle tier contained 10 kilograms of beryllium;
- An underground roof falling event where the bottom tier of containers is compacted by 15 inches;
- A sprinkler activation event in the WHB resulting in interstitial moderation between the waste containers;
- Flooding of waste containers at various water densities from 0 to 1 g/cm^3, and
- An impact of a 41-ton forklift with drums in the underground repository resulting in crushed containers.

A.4.1 Array Overstack Model

Although WIPP panel heights were designed to accommodate three layers of waste containers, ground control safety constraints have resulted in areas of the disposal rooms being mined to a height greater than 13 feet. As a result, it is possible to stack greater than three tiers including the MgO. The computational results for a four-tier stack of 55-gallon drum seven-packs yielded a system eigenvalue less than 0.96 as summarized in Table A-11.

Table A-11. Results for an Array Overstacking Event with 55-Gallon Drum Seven-packs Four Tiers High

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
800	0.93608	0.00080	0.93768	dac4h16
900	0.94303	0.00073	0.94449	dac4h18
1000	0.94770	0.00070	0.94910	dac4h20
1100	0.94779	0.00067	0.94913	dac4h22
1200	0.94501	0.00072	0.94645	dac4h24
1300	0.94382	0.00069	0.94520	dac4h26

A.4.2 Array Overbatch Models

An overbatch event is unlikely since waste is required to meet the WAC as part of the approval to ship waste to WIPP. Also, the WIPP FGE limits meet or exceed the FGE limits for the transportation packages used to ship waste to WIPP. However, to ensure a conservative bound on waste storage, handling, and disposal of CH waste containers with less than 1% beryllium, a contingency event was simulated where it was evaluated that one container in a three-tier stack is overbatched by 50% of its nominal value. From a modeling perspective, one container in the bottom or middle tier is overbatched and the stack is infinitely reflected on the lateral surfaces as in the base array model. This is conservative as it results in one of twenty-one 55-gallon drums or one in three SWBs being overbatched. In the 55-gallon drum array, the seven-pack limit of 650 FGE was maintained. The other SWBs were modeled with 380 FGE and 25 grams of ^{240}Pu per container. Polyethylene reflection within the containers was not considered if the overbatched container contained less than 450 FGE and thus was below the subcritical limit for an optimally moderated Pu sphere with full water reflection from ANS/ANSI-8.1 Section 5.2. Full water reflection is judged to bound the reflection from 25% dense polyethylene in the containers. Instead, polyethylene is not modeled in these containers as it has been shown to isolate the units in the base array cases in Section A.2. However, the SWB overbatch scenario exceeds 450 FGE. The SWB overbatch was evaluated with and without polyethylene in the SWB. All overbatching contingency computations yielded a system eigenvalue under 0.96. Table A-12 through Table A-13 summarize the results of the MCNP5 calculations. The SWB is shown to be slightly more reactive with the polyethylene in the container showing that the reflection of the high overbatched mass drives the reactivity more than the interaction between the SWBs in the array.

Table A-12. Results for an Overbatching Event Where the Four Fissile Drums in the Middle Tier Contained 50, 100, 200, and 300 FGE

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
800	0.89083	0.00078	0.89239	dacdb16
900	0.90061	0.00079	0.90219	dacdb18
1000	0.90498	0.00079	0.90656	dacdb20
1100	0.90888	0.00078	0.91044	dacdb22
1200	0.90994	0.00077	0.91148	dacdb24
1300	0.90760	0.00069	0.90898	dacdb26
1400	0.90594	0.00065	0.90724	dacdb28
1500	0.90183	0.00064	0.90311	dacdb30

Table A-13. Results for an FGE Overbatching Event with SWBs

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
One SWB at 487.5 FGE with 0 g ^{240}Pu and 0% Polyethylene in SWB around Fissile Mass				
900	0.92061	0.00054	0.92169	00sno09
1000	0.92645	0.00055	0.92755	00sno10
1100	0.92828	0.00055	0.92938	00sno11
1200	0.93004	0.00052	0.93108	00sno12
1300	0.92637	0.00035	0.92707	00sno13
1400	0.92275	0.00050	0.92375	00sno14
One SWB at 487.5 FGE with 0 g ^{240}Pu and 25% Dense Polyethylene filling SWB around Fissile Mass				
900	0.93622	0.00058	0.93738	00swo09
1000	0.93739	0.00055	0.93849	00swo10
1100	0.93705	0.00053	0.93811	00swo11
1200	0.93484	0.00052	0.93588	00swo12
1300	0.93090	0.00040	0.93170	00swo13
1400	0.92465	0.00050	0.92565	00swo14
One SWB at 570 FGE with 37.5 g ^{240}Pu and 0% Polyethylene in SWB around Fissile Mass				
900	0.93278	0.00056	0.93390	2psno09
1000	0.93619	0.00057	0.93733	2psno10
1100	0.93972	0.00054	0.94080	2psno11
1200	0.93987	0.00050	0.94087	2psno12
1300	0.93858	0.00038	0.93934	2psno13
1400	0.93555	0.00048	0.93651	2psno14
One SWB at 570 FGE with 37.5 g ^{240}Pu and 25% Dense Polyethylene filling SWB around Fissile Mass				
900	0.93911	0.00056	0.94023	2pswo09
1000	0.94154	0.00054	0.94262	2pswo10
1100	0.94248	0.00054	0.94356	2pswo11
1200	0.93939	0.00049	0.94037	2pswo12
1300	0.93614	0.00041	0.93696	2pswo13
1400	0.93170	0.00052	0.93274	2pswo14

A.4.3 Array with Excess Beryllium

In addition to the FGE overbatching contingency, an overbatching event was considered where the beryllium content in one 55-gallon drum in the modeled three-tier stack of containers exceeds its mass limit. Specifically, a drum with a 5-kilogram beryllium limit was double batched to 10 kilograms. The results of this overbatching event, which is tabulated in Table A-14, illustrates that double batching the beryllium has only a minor effect.

Table A-14. Results for an Overbatching Event with One Fissile Drum in the Middle Tier Containing 10 kg of Beryllium

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
800	0.87837	0.00080	0.87997	dacbb16
900	0.89010	0.00074	0.89158	dacbb18
1000	0.89619	0.00073	0.89765	dacbb20
1100	0.89854	0.00075	0.90004	dacbb22
1200	0.89916	0.00070	0.90056	dacbb24
1300	0.89903	0.00071	0.90045	dacbb26
1400	0.89495	0.00070	0.89635	dacbb28
1500	0.89224	0.00069	0.89362	dacbb30
1600	0.88664	0.00066	0.88796	dacbb32
1700	0.88147	0.00061	0.88269	dacbb34
1800	0.87459	0.00059	0.87577	dacbb36

A.4.4 Underground Roof Fall Model

The loss of geometry contingency event where it is postulated that the roof fall during the operational phase of the disposal panel, is simulated as a vertical compaction of 15 inches to the bottom tier of drums. Specifically, the compaction was modeled by reducing the height of all drums in Section A.2.1 by 15 inches and then centering the fissile source in the drum. The results are summarized in Table A-15. As indicated by the data, the compaction has a small effect on the reactivity of the array (maximum base case reactivity is 0.90096) and the results remain below the USL of 0.96.

Table A-15. Results for a Roof Fall/Compaction Event

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
55-gallon Drums of Direct-loaded Waste Containing ≤ 1 wt% Special Reflectors				
800	0.82205	0.00079	0.82363	daccp10
900	0.85798	0.00090	0.85978	daccp12
1000	0.88209	0.00076	0.88361	daccp14
1100	0.89644	0.00074	0.89792	daccp16
1200	0.90751	0.00074	0.90899	daccp18
1300	0.91583	0.00079	0.91741	daccp20
1400	0.91693	0.00065	0.91823	daccp22
1500	0.91894	0.00070	0.92034	daccp24
1600	0.91859	0.00069	0.91997	daccp26
1700	0.91467	0.00061	0.91589	daccp28
1800	0.91166	0.00064	0.91294	daccp30

A.4.5 Sprinkler Activation Model

The contingency considered in this section addresses the potential activation of the sprinkler system in the WHB resulting in interstitial moderation between the waste containers. The model employed to simulate this event evaluates a bounding three-tier stack of seven-packs of 55-gallon drums where the ceiling and floor are modeled as 2 feet (60.96 centimeters) thick concrete, while the sides are mirrored for infinite reflection as shown in Figure C-15, of Appendix C. The other parameters are consistent with the base case model at optimum moderation (i.e., case dac0026 from Section A.2.1). Water from sprinkler activation is allowed to fill the spaces between the drums. The water density is varied from 0.05 to 1 g/cm^3, and the results are shown in Table A-16. All water densities reduce the reactivity of the direct-loaded waste array. Furthermore, the values are significantly below the USL.

Table A-16. Sprinkler Activation Contingency with Varied Water Density

Water density (g/cm^3)	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
55-gallon Drums of Direct-loaded Waste Containing ≤ 1 wt% Special Reflectors				
0	0.85104	0.00071	0.85246	das0026
0.05	0.81571	0.00066	0.81703	das0526
0.10	0.79249	0.00072	0.79393	das1026
0.15	0.77478	0.00067	0.77612	das1526
0.20	0.76234	0.00074	0.76382	das2026
0.25	0.75280	0.00071	0.75422	das2526
0.30	0.74562	0.00073	0.74708	das3026
0.40	0.73229	0.00071	0.73371	das4026
0.50	0.72438	0.00078	0.72594	das5026
0.75	0.70944	0.00078	0.71100	das7526
1.00	0.70494	0.00072	0.70638	da10026

A.4.6 Excess Water/Flooding in a CH Waste Containers

This contingent condition simulates an abnormal state where the various CH waste drums/containers contain an excess of liquid in the dunnage as a result of a generator site error or water seepage into the container. A water intrusion contingency analysis is performed where it is evaluated that various amounts of water mix with the internal polyethylene reflector around the fissile mass. The analysis is parametric in nature in that the amount of water in the beryllium-polyethylene-water mixture filling the container around the fissile mass varies to represent the range from dry to fully flooded containers. Specifically, the following partially/fully flooded conditions are analyzed:

- Beryllium mixed with 25% by volume polyethylene and 18.75% by volume water,
- Beryllium mixed with 25% by volume polyethylene and 37.5% by volume water,
- Beryllium mixed with 25% by volume polyethylene and 56.25% by volume water,
- Beryllium mixed with 25% by volume polyethylene and 75% by volume water,
- Beryllium mixed with 15% by volume polyethylene and 85% by volume water, and
- Beryllium mixed with 5% by volume polyethylene and 95% by volume water.

Partial and Full Flooding of a 55-Gallon Drum Array in the Underground Repository

The first CH waste configuration evaluated is a disposal array of seven-packs of 55-gallon drums in the underground repository. The model is consistent with that presented in Section A.2.1 with respect to fissile mass content and geometric configuration. The results of the flooding contingency calculation for both partially flooded and fully flooded drums are summarized in Figure A-12 and Figure A-13 and tabulated in Table A-17 and Table A-18. As indicated by the data, the system reactivity increases with the water content in the partial flooding state case and ultimately peaks at above 15% polyethylene and 85% water in the fully flooded state. In all cases, the system eigenvalue remains well below the USL; therefore, a criticality event result from a water intrusion contingency in an array of 55-gallon drums containing CH waste is not credible.

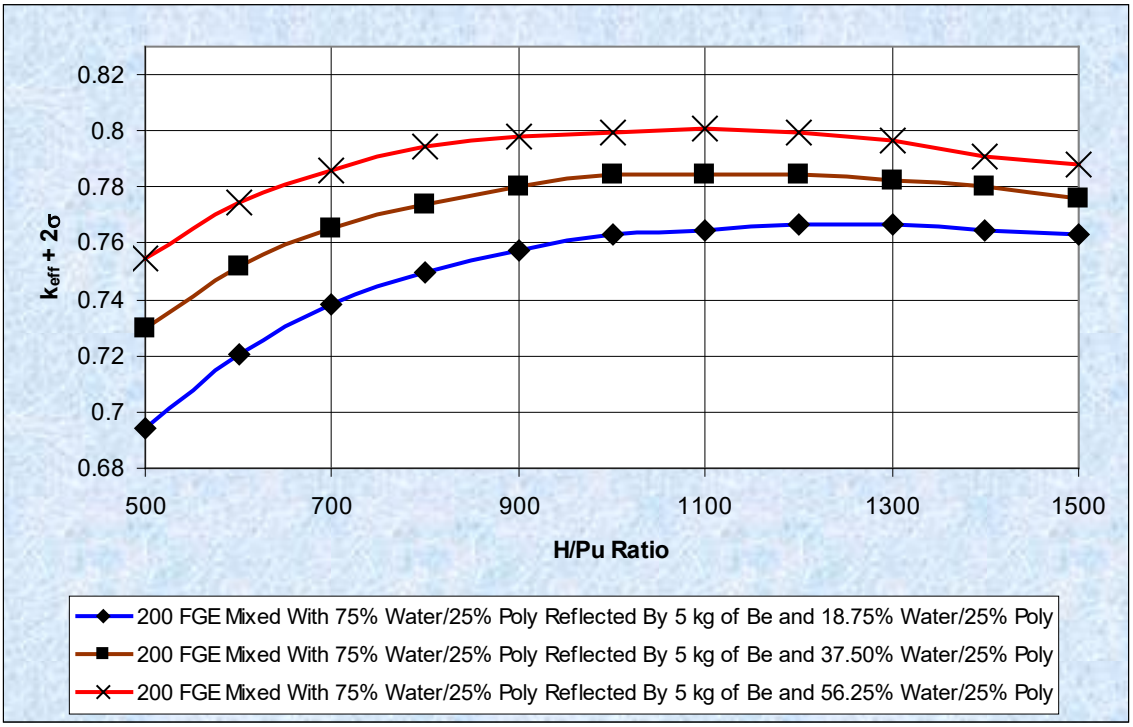


Figure A-12. Partial Flooding Results for an Underground Array of Seven-Packs of 55-gallon Drums

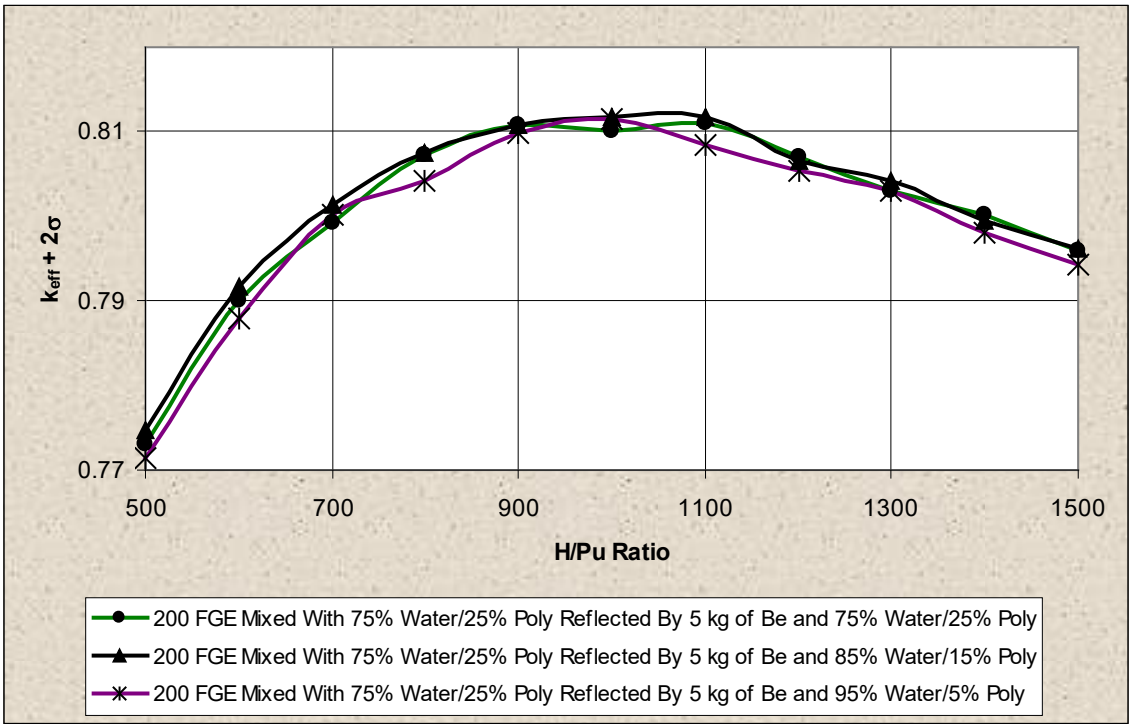


Figure A-13. Full Flooding Results for an Underground Array of Seven-Packs of 55-gallon Drums

Table A-17. Partial Flooding Results for an Underground Array of Seven-packs of 55-Gallon Drums

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
5 kg Beryllium Mixed With 25% By Volume Polyethylene and 18.75% By Volume Water				
500	0.69248	0.00087	0.69422	dacw010
600	0.71931	0.00077	0.72085	dacw012
700	0.73632	0.00087	0.73806	dacw014
800	0.74800	0.00083	0.74966	dacw016
900	0.75565	0.00078	0.75721	dacw018
1000	0.76120	0.00087	0.76294	dacw020
1100	0.76264	0.00085	0.76434	dacw022
1200	0.76493	0.00075	0.76643	dacw024
1300	0.76553	0.00077	0.76707	dacw026
1400	0.76333	0.00078	0.76489	dacw028
1500	0.76149	0.00072	0.76293	dacw030
5 kg Beryllium Mixed With 25% By Volume Polyethylene and 37.5% By Volume Water				
500	0.72799	0.00087	0.72973	dacw050
600	0.74966	0.00093	0.75152	dacw052
700	0.76357	0.00085	0.76527	dacw054
800	0.77197	0.00084	0.77365	dacw056
900	0.77887	0.00077	0.78041	dacw058
1000	0.78299	0.00076	0.78451	dacw060
1100	0.78324	0.00079	0.78482	dacw062
1200	0.78267	0.00076	0.78419	dacw064

Table A-17. Partial Flooding Results for an Underground Array of Seven-packs of 55-Gallon Drums

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
1300	0.78113	0.00074	0.78261	dacw066
1400	0.77855	0.00073	0.78001	dacw068
1500	0.77463	0.00078	0.77619	dacw070
5 kg Beryllium Mixed With 25% By Volume Polyethylene and 56.25% By Volume Water				
500	0.75289	0.00079	0.75447	dacw090
600	0.77298	0.00082	0.77462	dacw092
700	0.78435	0.00083	0.78601	dacw094
800	0.79260	0.00076	0.79412	dacw096
900	0.79668	0.00072	0.79812	dacw098
1000	0.79807	0.00079	0.79965	dacw100
1100	0.79907	0.00077	0.80061	dacw102
1200	0.79783	0.00078	0.79939	dacw104
1300	0.79474	0.00078	0.79630	dacw106
1400	0.78940	0.00076	0.79092	dacw108
1500	0.78696	0.00063	0.78822	dacw110

Table A-18. Full Flooding Results for an Underground Array of Seven-packs of 55-Gallon Drums

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
5 kg Beryllium Mixed With 25% By Volume Polyethylene and 75% By Volume Water				
500	0.77310	0.00076	0.77462	dacw130
600	0.79004	0.00086	0.79176	dacw132
700	0.79981	0.00081	0.80143	dacw134
800	0.80585	0.00082	0.80749	dacw146
900	0.80933	0.00078	0.81089	dacw138
1000	0.81022	0.00075	0.81172	dacw140
1100	0.81015	0.00079	0.81173	dacw142
1200	0.80514	0.00071	0.80656	dacw144
1300	0.80278	0.00072	0.80422	dacw146
1400	0.79802	0.00075	0.79952	dacw148
1500	0.79476	0.00072	0.79620	dacw150
5 kg Beryllium Mixed With 15% By Volume Polyethylene and 85% By Volume Water				
500	0.77143	0.00079	0.77301	dacw170
600	0.78827	0.00085	0.78997	dacw172
700	0.79777	0.00079	0.79935	dacw174
800	0.80575	0.00079	0.80733	dacw176
900	0.80934	0.00076	0.81086	dacw178
1000	0.80849	0.00077	0.81003	dacw180
1100	0.80953	0.00075	0.81103	dacw182
1200	0.80564	0.00074	0.80712	dacw184
1300	0.80165	0.00071	0.80307	dacw186
1400	0.79885	0.00069	0.80023	dacw188
1500	0.79460	0.00064	0.79588	dacw190

Table A-18. Full Flooding Results for an Underground Array of Seven-packs of 55-Gallon Drums

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
5 kg Beryllium Mixed With 5% By Volume Polyethylene and 95% By Volume Water				
500	0.76975	0.00089	0.77153	dacw210
600	0.78635	0.00083	0.78801	dacw212
700	0.79866	0.00080	0.80026	dacw214
800	0.80273	0.00076	0.80425	dacw216
900	0.80823	0.00082	0.80987	dacw218
1000	0.80976	0.00083	0.81142	dacw220
1100	0.80685	0.00074	0.80833	dacw222
1200	0.80399	0.00072	0.80543	dacw224
1300	0.80148	0.00074	0.80296	dacw226
1400	0.79664	0.00071	0.79806	dacw228
1500	0.79301	0.00070	0.79441	dacw230

Partial and Full Flooding of an Array of SWBs in the Underground Repository

A water intrusion event in an array of SWBs in the underground storage repository is simulated. The model used in the computational analysis is consistent with that used in Section A.2.2 with respects to fissile material content, geometry, and array configuration. Figure A-14 and Figure A-15 illustrate the computational results for the partially fully flooded states respectively, whereas Table A-19 and Table A-20 tabulate the associated numerical eigenvalues. Although system reactivity increases with water content and peaks for the fully flooded cases, the results indicate that all cases were below the established USL. Therefore, a criticality event due to water ingress in an array of SWBs containing CH waste is not credible.

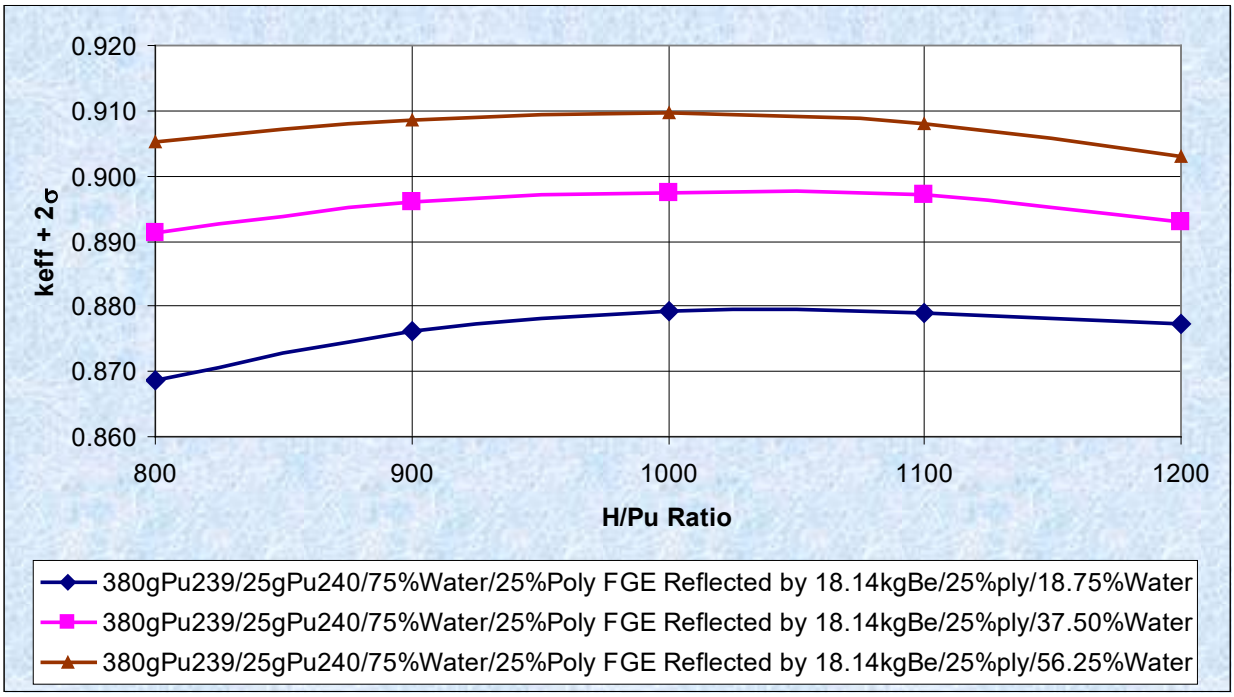


Figure A-14. Partial Flooding Results for an Underground Array of SWBs

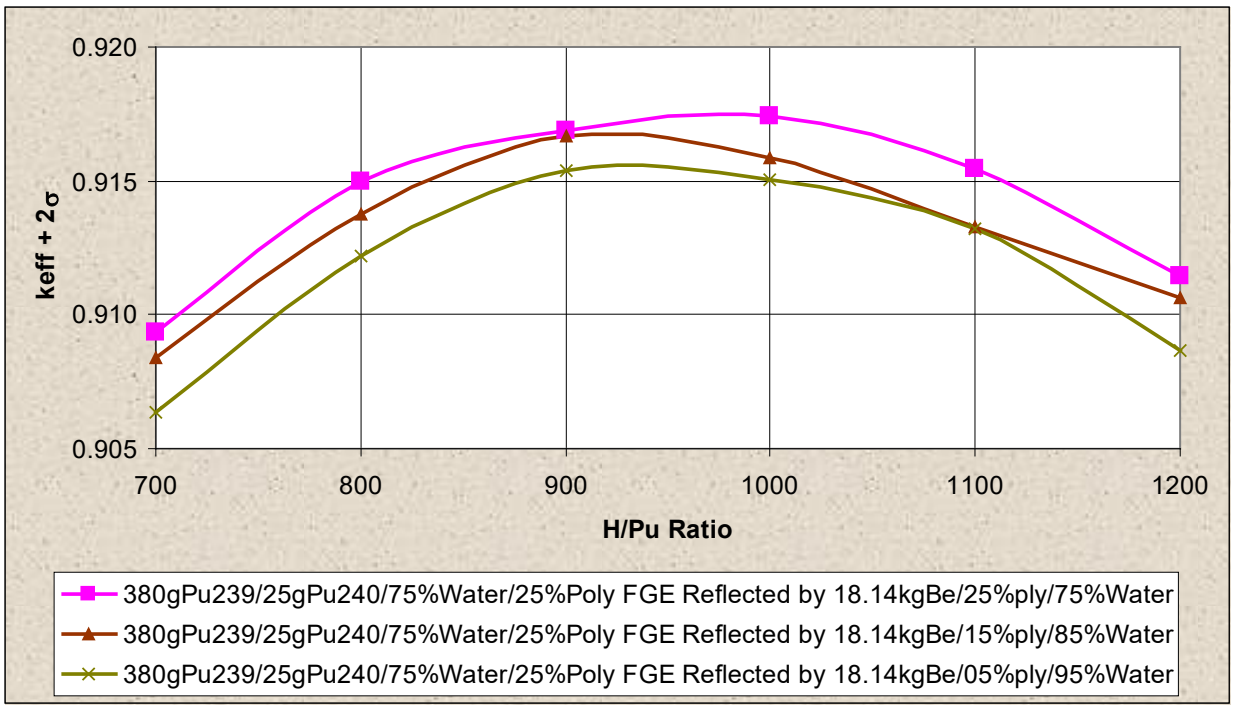


Figure A-15. Full Flooding Results for an Underground Array of SWBs

Table A-19. Partial Flooding Results for an Underground Array of SWBs

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
18.14 kg beryllium Mixed With 25% By Volume Polyethylene and 18.75% By Volume Water				
800	0.86760	0.00056	0.86872	2ps1808
900	0.87508	0.00051	0.87610	2ps1809
1000	0.87809	0.00055	0.87919	2ps1810
1100	0.87792	0.00055	0.87902	2ps1811
1200	0.87628	0.00053	0.87734	2ps1812
18.14 kg beryllium Mixed With 25% By Volume Polyethylene and 37.5% By Volume Water				
800	0.89002	0.00059	0.89120	2ps3708
900	0.89488	0.00054	0.89596	2ps3709
1000	0.89619	0.00054	0.89727	2ps3710
1100	0.89596	0.00055	0.89706	2ps3711
1200	0.89201	0.00051	0.89303	2ps3712
18.14 kg beryllium Mixed With 25% By Volume Polyethylene and 56.25% By Volume Water				
800	0.90401	0.00057	0.90515	2ps5608
900	0.90740	0.00054	0.90848	2ps5609
1000	0.90874	0.00051	0.90976	2ps5610
1100	0.90687	0.00053	0.90793	2ps5611
1200	0.90201	0.00049	0.90299	2ps5612

Table A-20. Full Flooding Results for an Underground Array of SWBs

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
18.14 kg beryllium Mixed With 25% By Volume Polyethylene and 75% By Volume Water				
700	0.90824	0.00056	0.90936	2ps7507
800	0.91390	0.00055	0.91500	2ps7508
900	0.91588	0.00051	0.91690	2ps7509
1000	0.91636	0.00053	0.91742	2ps7510
1100	0.91443	0.00052	0.91547	2ps7511
1200	0.91048	0.00050	0.91148	2ps7512
18.14 kg beryllium Mixed With 15% By Volume Polyethylene and 85% By Volume Water				
700	0.90727	0.00057	0.90841	2ps8507
800	0.91265	0.00054	0.91373	2ps8508
900	0.91555	0.00055	0.91665	2ps8509
1000	0.91490	0.00049	0.91588	2ps8510
1100	0.91225	0.00051	0.91327	2ps8511
1200	0.90960	0.00050	0.91060	2ps8512

Table A-20. Full Flooding Results for an Underground Array of SWBs

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
18.14 kg beryllium Mixed With 5% By Volume Polyethylene and 95% By Volume Water				
700	0.90528	0.00055	0.90638	2ps9507
800	0.91107	0.00055	0.91217	2ps9508
900	0.91434	0.00052	0.91538	2ps9509
1000	0.91399	0.00054	0.91507	2ps9510
1100	0.91212	0.00053	0.91318	2ps9511
1200	0.90772	0.00047	0.90866	2ps9512

A.4.7 Impact of a 41-Ton Forklift on a Seven-pack Array in the Underground Repository

This contingency simulates an accident condition where the 41-ton waste handling forklift impacts an array of seven-packs of 55-gallon drums containing CH waste in the underground repository. The 41-ton forklift is used to move the lead-shielded facility cask containing remote handled (RH) waste and the shielded, heavy portions of the horizontal emplacement retrieval equipment as described in the *Waste Isolation Pilot Plant Documented Safety Analysis* (DOE/WIPP-07-3372). The 41-ton forklift can also be used to move other large, heavy underground equipment from the waste hoist. The forklift is not normally near the CH waste face because the RH waste is typically emplaced into boreholes in the salt walls before the CH waste is emplaced nearby. The RH horizontal emplacement waste handling equipment is typically placed between the CH waste face and the approaching 41-ton forklift.

To simulate the effects of a high-energy impact of the 41-ton forklift on the waste drums, some of the air volume within the 55-gallon drums is expelled, leaving the drums permanently deformed. In particular, the volume of the 55-gallon drums is reduced to 75% of their initial volume in the model. This is a conservative bound on the deformation of the drum considering the maximum credible impact momentum of the forklift, the yield strength of a certified 55-gallon drum, and the way the drums are configured in a seven-pack array. Since some of the air is expelled, the internal reflector mass around the moderated fissile will compress and the density will increase. Thus, the polyethylene, which makes up the bulk of the dunnage around the fissile mass, is compressed from a maximum of 25 to 33% of its theoretical density. Furthermore, the model evaluates the geometry of the 55-gallon drums as deformed into an elliptical shape with the ratio of the major to minor axes being 2. The elongated fissile mass and internal reflector waste in the 55-gallon drums are moved closer together and become more reactive in this configuration. The model uses a rectangular array (since the waste packages and drums are elliptical cylinders) to minimize the distance between fissile masses in the array. Finally, to maximize the reactivity state of the system and at the same time not restrict the number of seven-packs involved in the accident, mirror boundary conditions are used on three of the four lateral boundaries simulating an infinite array. The fourth boundary uses a reflector made up of 200 centimeters of lead to bound the neutron reflection from the RH canister and the forklift. In the vertical plane, the upper tier is reflected by an MgO layer (approximately 62 centimeters thick) placed on top of the 55-gallon drums and the whole stack is then reflected by 300 centimeters of salt above and below. The contents of the waste package used in the forklift impact contingency analysis are consistent with that presented in Section A.2.1.

Two configurations of fissile material within the drums were considered in the contingency analysis. The first configuration evaluates three 200-FGE drums as impacted by the forklift and the whole seven-pack stack is crushed and displaced into the surrounding seven-packs. The resulting arrangement is a three-by-

three array with three 200-FGE drums in the first row, one 50-FGE drum in the middle of the second row with one non-fissile bearing drum on either side, and one non-fissile bearing drum in the middle of the last row with one 200-FGE drum on either side. The two 200-FGE drums in the last row actually originate from the surrounding seven-packs. The boundaries that are not reflected by lead are infinitely reflected to model an infinite array of crushed seven-packs. The second configuration is similar to the first except the fissile contents in the drums in the first and last rows are exchanged. Figure A-16 and Figure A-17 illustrate the pertinent model features for the two configurations used in the analysis. Finally, to maximize the interaction effects, a computation was also performed where the polyethylene in the internal reflector was removed and only the beryllium remained in the reflector zone of the "crushed" drums. Figure A-18, Table A-21 and Table A-22 summarize the results of the contingency calculation. As indicated by the data, the maximum system eigenvalue is less than 0.89501 and occurs when the polyethylene was removed from the crushed drums, thereby allowing the closely located fissile masses to interact. Therefore, it is concluded that a criticality event due to the high impact of a large object such as a 41-ton forklift with an array of seven-packs of 55-gallon drums is not credible.

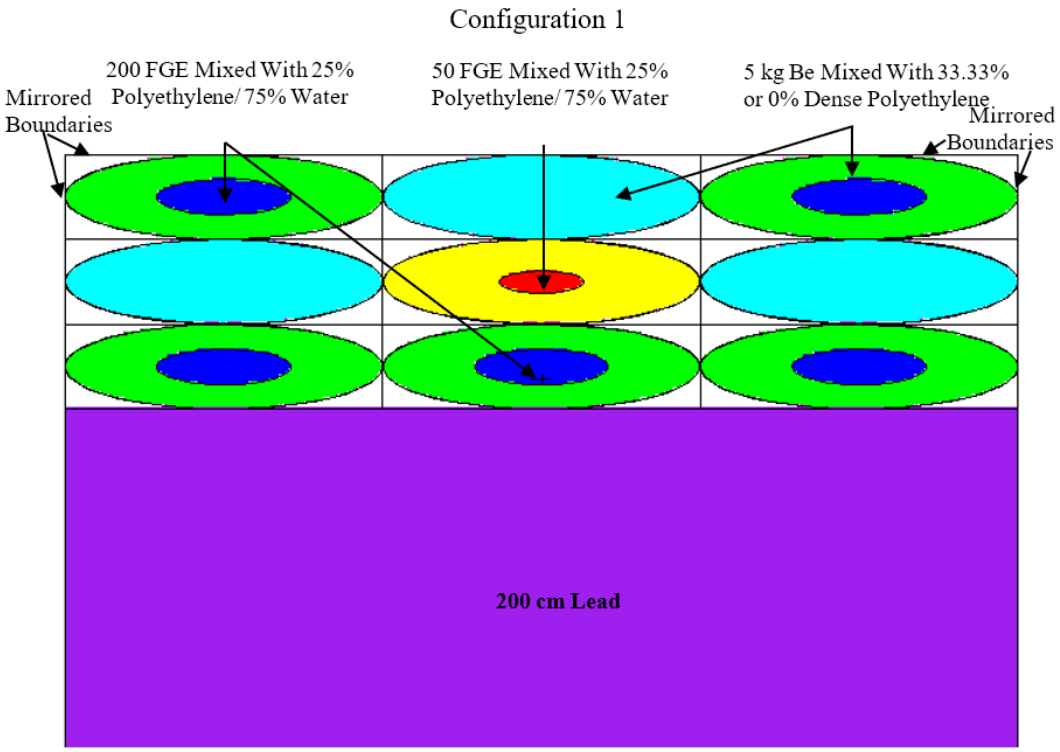


Figure A-16. Top View of Configuration 1 Model for the High Energy Impact Contingency Between a 41-ton Forklift and an Array of 55-Gallon Drums Seven-packs

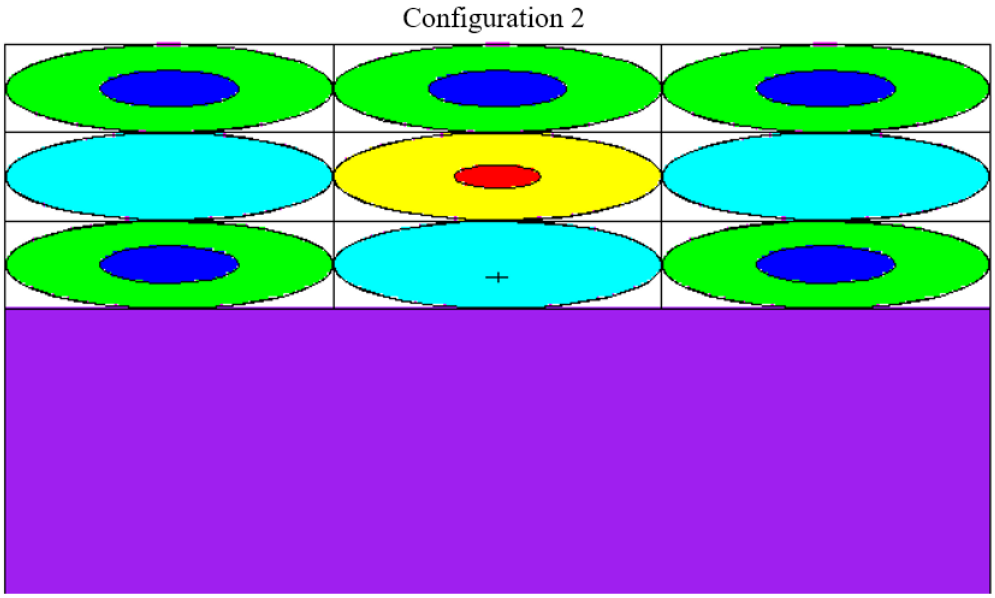


Figure A-17. Top View of Configuration 2 Model for the High Energy Impact Contingency Between a 41-ton Forklift and an Array of 55-Gallon Drums Seven-packs

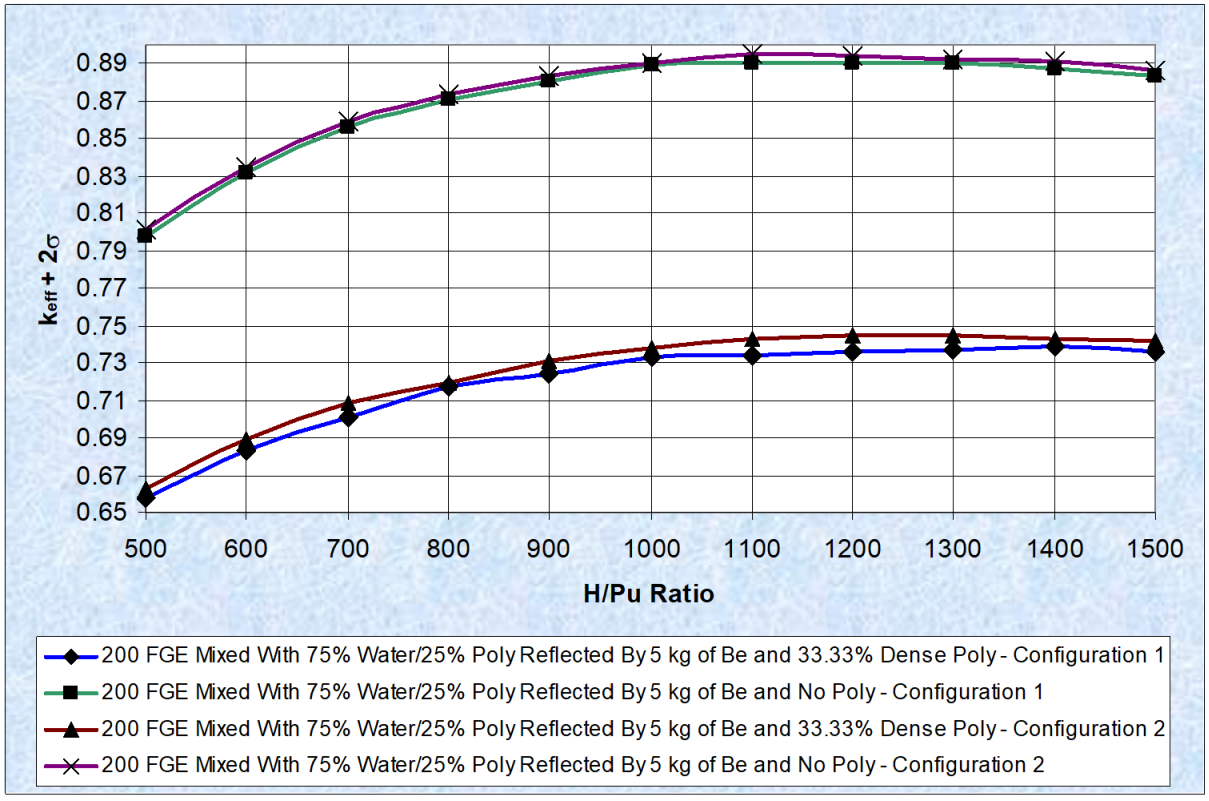


Figure A-18. System Reactivity Resulting from a High Energy Impact of a 41-ton Forklift with an Array of 55-Gallon Drums Seven-packs

Table A-21. MCNP5 Results for a High Energy Impact Contingency of 41-ton Forklift with an Array of 55-Gallon Drums Seven-packs – Configuration 1

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
5 kg Beryllium Mixed With 33% Dense Polyethylene				
500	0.65619	0.00084	0.65787	dacf010
600	0.68160	0.00082	0.68324	dacf012
700	0.69888	0.00085	0.70058	dacf014
800	0.71556	0.00083	0.71722	dacf016
900	0.72278	0.00080	0.72438	dacf018
1000	0.73164	0.00081	0.73326	dacf020
1100	0.73216	0.00076	0.73368	dacf022
1200	0.73429	0.00079	0.73587	dacf024
1300	0.73495	0.00075	0.73645	dacf026
1400	0.73731	0.00075	0.73881	dacf028
1500	0.73481	0.00068	0.73617	dacf030
5 kg Beryllium and No Polyethylene				
500	0.79638	0.00069	0.79776	dacf050
600	0.83041	0.00077	0.83195	dacf052
700	0.85392	0.00085	0.85562	dacf054
800	0.86887	0.00074	0.87035	dacf056
900	0.87896	0.00082	0.88060	dacf058
1000	0.88746	0.00072	0.88890	dacf060
1100	0.88868	0.00074	0.89016	dacf062
1200	0.88905	0.00070	0.89045	dacf064
1300	0.88864	0.00069	0.89002	dacf066
1400	0.88607	0.00063	0.88733	dacf068
1500	0.88222	0.00061	0.88344	dacf070

Table A-22. MCNP5 Results for a High Energy Impact Contingency of 41-ton Forklift with an Array of 55-Gallon Drums Seven-packs – Configuration 2

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
5 kg Beryllium Mixed With 33% Dense Polyethylene				
500	0.66135	0.00084	0.66303	dacf090
600	0.68691	0.00084	0.68859	dacf092
700	0.70678	0.00081	0.70840	dacf094
800	0.71824	0.00078	0.71980	dacf096
900	0.72954	0.00076	0.73106	dacf098
1000	0.73684	0.00070	0.73824	dacf100
1100	0.74063	0.00088	0.74239	dacf102
1200	0.74326	0.00078	0.74482	dacf104
1300	0.74343	0.00078	0.74499	dacf106
1400	0.74180	0.00069	0.74318	dacf108
1500	0.74062	0.00072	0.74206	dacf110

Table A-22. MCNP5 Results for a High Energy Impact Contingency of 41-ton Forklift with an Array of 55-Gallon Drums Seven-packs – Configuration 2

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
5 kg Beryllium and No Polyethylene				
500	0.80013	0.00086	0.80185	dacf130
600	0.83314	0.00081	0.83476	dacf132
700	0.85708	0.00084	0.85876	dacf134
800	0.87188	0.00068	0.87324	dacf136
900	0.88215	0.00075	0.88365	dacf138
1000	0.88862	0.00072	0.89006	dacf140
1100	0.89347	0.00077	0.89501	dacf142
1200	0.89318	0.00068	0.89454	dacf144
1300	0.89068	0.00067	0.89202	dacf146
1400	0.88945	0.00068	0.89081	dacf148
1500	0.88481	0.00070	0.88621	dacf150

A.5 Conclusions

This appendix demonstrates that the following direct-loaded containers with less than or equal to 1 wt% special reflector materials will remain below the USL in the two-container configuration, as well as in the underground array with the following limits:

- 55-gallon, 85-gallon, 100-gallon drums
  - Maximum 200 FGE per drum
  - Maximum 1 wt% particulate beryllium per drum
  - Maximum 650 FGE per pack of drums
- SWB containers
  - Maximum 325 FGE with 0 grams ^{240}Pu, 340 FGE with 5 grams ^{240}Pu, 360 FGE with 15 grams ^{240}Pu, OR 380 FGE with 25 grams ^{240}Pu per SWB
  - Maximum 1 wt% particulate beryllium per SWB
- SLB2 containers
  - Maximum 325 FGE with 0 grams ^{240}Pu, 340 FGE with 5 grams ^{240}Pu, 360 FGE with 15 grams ^{240}Pu, OR 380 FGE with 25 grams ^{240}Pu per SLB2
  - Maximum 1 wt% particulate beryllium per SLB2.

A.6 References

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WTS, 2007b. *Standard Large Box 2 Assembly (SLB2) Bottom Loading*, 165-F-017-W1, Revision A, (http://www.wipp.energy.gov/library/slb/165-F-017.pdf), Washington TRU Solutions LLC, Carlsbad, NM.

A.7 Sample MCNP5 Input File Listings for Appendix A

A.7.1 MCNP Input File Listing for 55-gallon Drum Array Case (Filename dac0026)

```
C CCCC
```

```
C                                                                                $
9     5    -0.02308   -2 -10  8                          U=3    IMP:N=1          $
10    LIKE 3 BUT U=3                                             IMP:N=1          $
11    LIKE 4 BUT U=3                                             IMP:N=1          $
C                                                                                $
C     CELL CARDS FOR THE HEXAGONAL 7-PACK STACK.                                $
C                                                                                $
12    0               -21 20 -22 25 -23 24 -27 26 LAT=2 U=4    IMP:N=1          $
                       FILL=-3:3 -3:3 0:2                                        $
                       4 16R                                                     $
                           2 3   4 4 4 4                                         $
                          2 1 3  4 4 4 4                                         $
                           2 3   4 16R                                           $
                       4 16R                                                     $
                           2 3   4 4 4 4                                         $
                          2 1 3  4 4 4 4                                         $
                           2 3   4 16R                                           $
                       4 16R                                                     $
                           2 3   4 4 4 4                                         $
                          2 1 3  4 4 4 4                                         $
                           2 3   4 16R                                           $
13    0               -61 60 -62 65 -63 64 -67 66 FILL=4       IMP:N=1          $
C                                                                                $
C     CELL CARDS FOR THE MGO AND SALT LAYERS.                                   $
C                                                                                $
14    8    -2.165     (53:-66) -61 60 -62 65 -63 64 50 -52     IMP:N=1          $
15    7    -1.45      -61 60 -62 65 -63 64 67 -53              IMP:N=1          $
C                                                                                $
C     CELL CARDS FOR THE REST OF THE UNIVERSE.                                  $
C                                                                                $
16    0               -50:52:61:-60:62:-65:63:-64              IMP:N=0          $
                                                                                 $
C                                                                                $
C     SURFACE CARDS FOR ALL DRUM SUFFACES                                       $
C                                                                                $
2  CZ  28.575                                                                    $
4  CZ  28.696                                                                    $
6  PZ  0.0                                                                       $
8  PZ  0.121                                                                     $
10 PZ  84.576                                                                    $
12 PZ  84.697                                                                    $
C                                                                                $
C     CELL CARDS FOR THE 50 AND 200 FGE DRUMS.                                  $
C                                                                                $
14 RCC 0 0  35.1479 0 0  14.4012   7.2006                                        $
34 RCC 0 0  30.9182 0 0  22.8605  11.4303                                        $
C                                                                                $
C     SURFACE CARDS FOR THE HEXAGONAL 7-PACK.                                   $
C                                                                                $
20 PX -28.75                                                                     $
21 PX  28.75                                                                     $
22 P   1    1.7321    0    57.5                                                  $
23 P  -1    1.7321    0    57.5                                                  $
24 P  -1    1.7321    0   -57.5                                                  $
25 P   1    1.7321    0   -57.5                                                  $
26 PZ  0.0                                                                       $
27 PZ  84.697                                                                    $
C                                                                                $
C     SURFACE CARDS FOR THE MGO AND SALT LAYERS.                                $
C                                                                                $
50 PZ -300.00                                                                    $
52 PZ  616.321                                                                   $
53 PZ  316.321                                                                   $
C                                                                                $
C     SURFACE CARDS FOR THE 7-PACK STACK INFINITE ARRAY.                        $
C                                                                                $
*60 PY -78.5                                                                     $
*61 PY  78.5                                                                     $
*62 P   1.7321   1    0   157                                                   $
*63 P   1.7321  -1    0   157                                                   $
```

```
*64 P   1.7321  -1    0  -157                                          $
*65 P   1.7321   1    0  -157                                          $
66 PZ   0.0                                                           $
67 PZ   254.091                                                       $
                                                                      $
C                                                                     $
C  DATA CARDS.                                                       $
C                                                                     $
MODE N                                                                $
C                                                                     $
C  SOURCE CARDS.                                                      $
C                                                                     $
KCODE 5000 1.0 50 250                                                 $
KSRC -58 0 43    -30 -50 43                                           $
     -58 0 128   -30 -50 128                                          $
     -58 0 213   -30 -50 213                                          $
C                                                                     $
C  MATERIAL CARDS                                                     $
C                                                                     $
C                                                                     $
C  PU-H2O-POLY FOR THE FISSILE MASS CONTAINING 50 GRAMS OF PU.         $
C                                                                     $
M1    94239.60C     -0.021322                                         $
       1001.60C     -0.116868                                         $
       8016.60C     -0.664390                                         $
       6000.60C     -0.197420                                         $
MT1   LWTR.01T   POLY.01T                                             $
C                                                                     $
C  PU-H2O-POLY FOR THE FISSILE MASS CONTAINING 200 GRAMS OF PU.        $
C                                                                     $
M2    94239.60C     -0.021322                                         $
       1001.60C     -0.116868                                         $
       8016.60C     -0.664390                                         $
       6000.60C     -0.197420                                         $
MT2   LWTR.01T   POLY.01T                                             $
C                                                                     $
C  BE-POLY REFLECTOR AROUND THE FISSILE MASS CONTAINING 50 GRAMS PU.   $
C                                                                     $
M3    4009.60C      -1.000000                                         $
MT3   BE.01T                                                          $
C                                                                     $
C  BE-POLY REFLECTOR AROUND THE FISSILE MASS CONTAINING 200 GRAMS PU.  $
C                                                                     $
M4    4009.60C      -1.000000                                         $
MT4   BE.01T                                                          $
C                                                                     $
C  BE-POLY REFLECTOR IN THE NON-FISSILE MASS DRUMS.                    $
C                                                                     $
M5    4009.60C      -1.000000                                         $
MT5   BE.01T                                                          $
C                                                                     $
C  55-GALLON DRUM STEEL WALLS.                                        $
C                                                                     $
M6     6000.60C     -0.001500                                         $
      25055.60C     -0.006000                                         $
      15031.60C     -0.000350                                         $
      16000.60C     -0.000400                                         $
      26054.60C     -0.058513                                         $
      26056.60C     -0.909630                                         $
      26057.60C     -0.020827                                         $
      26058.60C     -0.0027769                                        $
C                                                                     $
C  MGO LAYER.                                                         $
C                                                                     $
M7    12000.60C           0.5                                       $
      8016.60C            0.5                                       $
C                                                                     $
C  SALT REFLECTOR.                                                    $
C                                                                     $
M8    11023.60C           0.5                                       $
```

```
      17000.60C           0.5                                                  $
C                                                                              $
C     PRINT TABLE 40 FOR MASS FRACTIONS                                        $
C                                                                              $
PRINT 40                                                                       $
C                                                                              $
C     PRINT TO MCTAL FILE                                                      $
C                                                                              $
PRDMP 2j 1                                                                     $
```

A.7.2 MCNP Input File Listing for 2-Drum Case (Filename m55g100)

```
STACKED 55 GALLON DRUM MODEL. BOTH DRUMS WITH 200G PU, H/PU = 1000             $
C     FGE WITH MIXED WITH A MODERATOR WHICH IS 25% BY VOLUME POLYETHYLENE      $
C     AND 75% BY VOLUME WATER. THE FISSILE MASS IS REFLECTED BY               $
C     A MIXTURE OF 5 KGS. OF BE AND POLYETHYLENE AT 25% PACKING FRACTION.     $
C     THE DRUMS ARE STACKED DIRECTLY ONE ON TOP OF ANOTHER WITH THE FISSILE    $
C     MASS IN THE LOWER DRUM BEING LOCATED AT THE TOP OF THE DRUM AND THE      $
C     FISSILE MASS IN THE UPPER DRUM BEING LOCATED IN THE BOTTOM OF THE DRUM. $
C     IN THIS CONFIGURATION THE FISSILE MASSES ARE IN CLOSE PROXIMITY.         $
C     BOTH FISSILE MASSES ARE CYLINDRICAL IN SHAPE WITH A H/D RATIO OF 0.5.    $
C     CONTAINER WALL DENSITY (STEEL) IS 50% TO ACCOUNT FOR DEGRADATION.        $
C     THE TWO-DRUM STACK IS SURROUNDED ON ALL SIDES WITH  300 CM OF MgO.       $
C     THE BOUNDARIES ARE MIRRORED TO SIMULATE INFINITE REFLECTION. 1/11/05     $
C                                                                             $
C CCCC
```

```
C                                                                       $
C     SURFACE CARDS FOR A 300 CM REFLECTOR AROUND THE TWO DRUMS         $
C                                                                       $
*100      CZ  328.69641                                                 $
*101      PZ  469.39564                                                 $
*102      PZ -300.00000                                                 $

C                                                                       $
C     MODE CARD.                                                       $
C                                                                       $
MODE N                                                                  $
C                                                                       $
C     TRANSFORMATION CARDS FOR THE TWO-DRUM MODEL.                     $
C                                                                       $
TR1   0.00000     0.00000    84.69782                                   $
C                                                                       $
C     MATERIAL CARDS                                                    $
C                                                                       $
C     PU-CH2-H2O (55 GALLON DRUM)                                       $
C                                                                       $
M1    94239.60C -0.027542     1001.60C -0.116125                  &     $
       8016.60C -0.660167     6000.60C -0.196165                        $
C                                                                       $
C     BE-CH2 REFLECTOR (55 GALLON DRUM)                                 $
C                                                                       $
M2     4009.60C -0.094875  6000.60C -0.774957  1001.60C -0.130168       $
C                                                                       $
C     CARBON STEEL DRUM.                                               $
C                                                                       $
M6     6000.60C -0.001500  25055.60C -0.006000  15031.60C -0.000350    &     $
      16000.60C -0.000400  26054.60C -0.058513  26056.60C -0.909630    &     $
      26057.60C -0.020827  26058.60C -0.0027769                               $
C                                                                       $
C     MgO                                                               $
C                                                                       $
M7      8016.60C -0.39700  12000.60C -0.603000                          $
C                                                                       $
C     S(ALPHA,BETA)                                                     $
C                                                                       $
MT1   LWTR.01T   GRPH.01T                                               $
MT2   POLY.01T   GRPH.01T    BE.01T                                     $
C                                                                       $
C     SOURCE CARDS                                                      $
C                                                                       $
KCODE 1000     1.0      50   800                                       $
KSRC  0.00000  0.00000  80.00000                                       $
PRINT                                                                   $
C                                                                       $
C     PRINT TO MCTAL FILE                                               $
C                                                                       $
PRDMP 2j 1                                                              $
```

A.7.3 MCNP Input File Listing for Two-Container SWB Case (Filename cswb100)

```
STACKED SWBs MODEL. BOTH SWBs WITH 325G PU, H/PU=1000              1/13/05     $
C     FGE MIXED WITH A H2O-POLYETHYLENE MODERATOR WHICH IS 25% BY               $
C     VOLUME POLYETHYLENE AND 75% BY VOLUME WATER. THE FISSILE MASS IN EACH     $
C     OF THE SWBs IS REFLECTED BY A MIXTURE OF 18.14 KGS. OF BERYLLIUM AND      $
C     POLYETHYLENE WITH AN OVERALL PACKING FRACTION OF 25%.                     $
C     ONE SWB IS STACKED DIRECTLY ON TOP OF THE OTHER SWB WITH                  $
C     THE FISSILE MASS IN THE LOWER SWB BEING LOCATED AT THE TOP OF             $
C     THE SWB CONTAINER AND THE FISSILE MASS IN THE UPPER SWB                   $
C     LOCATED IN THE BOTTOM. IN THIS CONFIGURATION THE FISSILE                  $
C     MASSES ARE IN CLOSE PROXIMITY. BOTH FISSILE MASSES ARE CYLINDRICAL IN     $
C     SHAPE WITH A H/D RATIO OF 0.5.                                            $
C     CONTAINER WALL DENSITY (STEEL) IS 50% TO ACCOUNT FOR DEGRADATION.         $
C     THE TWO-SWB STACK IS SURROUNDED ON ALL SIDES WITH 300 CM OF CONCRETE.     $
```

```
C                                                                                $
C CCCC
```

```
C     MATERIAL CARDS                                                          $
C                                                                             $
C     PU-CH2-H2O (SWB)                                                        $
C                                                                             $
M1    94239.60C -0.027542    1001.60C -0.116125      &                        $
       8016.60C -0.660167    6000.60C -0.196165                               $
C                                                                             $
C     BE-CH2 REFLECTOR (SWB)                                                  $
C                                                                             $
M2     4009.60C -0.039762  6000.60C -0.822144  1001.60C -0.138094             $
C                                                                             $
C     CARBON STEEL.                                                          $
C                                                                             $
M6     6000.60C -0.001500  25055.60C -0.006000  15031.60C -0.000350    &      $
      16000.60C -0.000400  26054.60C -0.058513  26056.60C -0.909630    &      $
      26057.60C -0.020827  26058.60C -0.0027769                              $
C                                                                             $
C     CONCRETE                                                                $
C                                                                             $
C     Composition from Handbook of Health Physics and Radiological Health     $
C     3rd Edition for Ordinary Concrete.                                     $
C                                                                             $
M7    1001.60c   -0.0056     8016.60c   -0.4981     11023.60c  -0.0171        $
      12000.60c  -0.0026     13027.60c  -0.0457     14000.60c  -0.3151        $
      16032.60c  -0.0013     19000.60c  -0.0192     20000.60c  -0.0829        $
      26054.60c  -0.0007316  26056.60c  -0.011373   26057.60c  -0.0002604     $
      26058.60c  -3.472e-005                                                  $
C                                                                             $
C     S(ALPHA,BETA)                                                           $
C                                                                             $
MT1   LWTR.01T   GRPH.01T                                                     $
MT2   POLY.01T   GRPH.01T    BE.01T                                           $
MT7   LWTR.01T                                                                $
C                                                                             $
C     SOURCE CARDS                                                            $
C                                                                             $
KCODE 1000     1.0      50   800                                            $
KSRC  0.00000  0.00000  80.00000                                             $
PRINT                                                                         $
C                                                                             $
C     PRINT TO MCTAL FILE                                                     $
C                                                                             $
PRDMP 2j 1                                                                    $
```

A.7.4 MCNP Input File Listing for Two-Container SLB2-SWB Case (Filename 2p1sm10)

```
SLB2/SWB 2-CONTAINER, 380G PU239, 25G PU240, H/PU=1000, 1cm internal separation
C     SWB STACKED ON SLB2 WITH SWB IN THE CORNER OF SLB2. FISSILE MASSES IN     $
C     CLOSE PROXIMITY.  SPECIFICALLY, THE FISSILE MASSES ARE MODELED AS         $
C     CYLINDERS WITH AN H/D=1/2. THE FISSILE MASS IN THE SLB2 IS MIXED          $
C     WITH A MODERATOR WHICH IS 25% BY VOLUME POLYETHYLENE AND 75% BY VOLUME    $
C     WATER. THE FISSILE MASS IS REFLECTED BY A MIXTURE OF 47.7 KGS OF BE       $
C     AND 25% DENSE POLYETHYLENE.  THE FISSILE MASS IN THE SWB IS               $
C     MIXED WITH A H2O-POLY MODERATOR WHICH IS 25% BY VOLUME                    $
C     POLYETHYLENE AND 75% BY VOLUME WATER. THE FISSILE MASS IN THE SWB IS      $
C     REFLECTED BY A MIXTURE OF 18.14 KGS. OF BE AND POLYETHYLENE WHICH HAS A   $
C     DENSITY OF 25% OF THEORETICAL. THE FISSILE MASS IN THE LOWER SLB2 IS      $
C     LOCATED AT THE TOP OF THE SLB2 AND THE FISSILE MASS IN THE UPPER SWB      $
C     IS LOCATED IN THE BOTTOM OF THE SWB SO THAT THE MASSES ARE IN CLOSE       $
C     PROXIMITY OF ONE ANOTHER.  THE SLB2 AND SWB WALL DENSITY (STEEL) IS 50%   $
C     TO ACCOUNT FOR DEGRADATION.  ALL LATERAL SIDES AND VERTICAL PLANES ARE    $
C     REFLECTED BY 300 CM OF MGO.                                  8/25/10      $
C                                                                             $
C CCCC
```

```
1     1    -1.0075   -1                                  IMP:N=1              $
2     2    -0.2364   -2  1                               IMP:N=1              $
3     5    -3.9300   -3  2                               IMP:N=1              $
4     5    -3.9300   -5  4  TRCL=(0  7.79 0)             IMP:N=1              $
5     LIKE 4 BUT             TRCL=(0  90.75 0)           IMP:N=1              $
6     LIKE 4 BUT             TRCL=(0 173.72 0)           IMP:N=1              $
7     LIKE 4 BUT             TRCL=(0 256.70 0)           IMP:N=1              $
8     0              -4      TRCL=(0  7.79 0)            IMP:N=1              $
9     LIKE 8 BUT             TRCL=(0  90.75 0)           IMP:N=1              $
10    LIKE 8 BUT             TRCL=(0 173.72 0)           IMP:N=1              $
11    LIKE 8 BUT             TRCL=(0 256.70 0)           IMP:N=1              $
20    0              -10 3  #4 #5 #6 #7 #8 #9 #10 #11    IMP:N=1              $
C                                                                             $
C     CELL CARDS FOR THE UPPER SWB.                                           $
C                                                                             $
21    LIKE 1 BUT             TRCL=(0  0   18.15)         IMP:N=1              $
22    4    -0.2391   #21    (-104 -112 102 -108 109)    IMP:N=1              $
23    5    -3.9300          (-106 101 -110 111 -113)                         $
                            (-102:104:108:-109:112)     IMP:N=1              $
24    0              -20    (106:-101:110:-111:113)     IMP:N=1              $
C                                                                             $
C     CELL CARDS FOR THE CONCRETE REFLECTOR.                                  $
C                                                                             $
70    6    -1.45     -100 20 10                          IMP:N=1              $
C                                                                             $
C     CELL CARDS FOR OUTSIDE THE REFLECTOR.                                   $
C                                                                             $
100   0               100                                 IMP:N=0              $
                                                                              $
C                                                                             $
C     SURFACE CARDS FOR THE LOWER SLB2 AND UPPER SWB.                         $
C                                                                             $
1     RCC  104.46 91.44 179.07   0 0 -16.3454 16.3454                         $
2     BOX  4.29 4.29 10.64 165.89 0 0  0 265.43 0  0 0 168.43                 $
3     BOX  3.81 3.81 10.16 166.85 0 0  0 266.38 0  0 0 169.39                 $
4     BOX  3.81 0.32  0.32 166.85 0 0  0   9.52 0  0 0   9.52                 $
5     BOX  3.81 0     0    166.85 0 0  0  10.16 0  0 0  10.16                 $
10    BOX  0    0     0    174.47 0 0  0 274.00 0  0 0 179.55                 $
20 1  BOX  0    0     0    174.47 0 0  0 274.00 0  0 0  93.98                 $
C                                                                             $
C     SURFACE CARDS FOR THE SWB.                                              $
C                                                                             $
101 2 PZ   0                                                                  $
102 2 PZ   0.3175                                                             $
104 2 PZ   93.6625                                                            $
106 2 PZ   93.98                                                              $
108 2 PX   65.8813                                                            $
109 2 PX  -65.8813                                                            $
110 2 PX   66.1988                                                            $
111 2 PX  -66.1988                                                            $
112 2 CZ   87.3125                                                            $
113 2 CZ   87.63                                                              $
C                                                                             $
C     SURFACE CARDS FOR THE OUTSIDE REFLECTOR.                                $
C                                                                             $
100   BOX  -300 -300 -300  774.47 0 0  0 874.00 0  0 0 873.53                 $
                                                                              $
C                                                                             $
C     DATA CARDS                                                              $
C                                                                             $
MODE N                                                                        $
C                                                                             $
C     TRANSFORMATION CARD                                                     $
C                                                                             $
TR1   0 0 179.55                                                              $
TR2   104.46 91.44 179.55                                                     $
C                                                                             $
C     SOURCE CARDS                                                            $
C                                                                             $
KCODE 5000     1.0     50    250                                            $
```

```
KSRC  104.46 91.44 171.9588                                                    $
      104.46 91.44 188.7200                                                    $
C                                                                              $
C     MATERIAL CARDS                                                           $
C                                                                              $
C     PU-H2O-POLY FISSILE MASS (SLB2).                                         $
C                                                                              $
M1    94239.60C -0.027493   1001.60C -0.115915                          &       $
       8016.60C -0.658973   6000.60C -0.195810  94240.60C -0.001809            $
MT1   LWTR.01T   POLY.01T                                                      $
C                                                                              $
C     BE-POLY REFLECTOR AROUND THE FISSILE MASS (SLB2).                        $
C                                                                              $
M2     4009.60C     -0.027241                                                  $
       6000.60C     -0.832865                                                  $
       1001.60C     -0.139895                                                  $
MT2   BE.01T      POLY.01T                                                     $
C                                                                              $
C     BE-POLY REFLECTOR AROUND THE FISSILE MASS (SWB).                         $
C                                                                              $
M4     4009.60C -0.039802    6000.60C -0.822110   1001.60C -0.138088           $
MT4   BE.01T      POLY.01T                                                     $
C                                                                              $
C     STEEL FOR SLB2S.                                                         $
C                                                                              $
M5     6000.60C     -0.001500                                                  $
      25055.60C     -0.006000                                                  $
      15031.60C     -0.000350                                                  $
      16000.60C     -0.000400                                                  $
      26054.60C     -0.058513                                                  $
      26056.60C     -0.909630                                                  $
      26057.60C     -0.020827                                                  $
      26058.60C     -0.0027769                                                 $
C                                                                              $
C     MGO REFLECTOR.                                                           $
C                                                                              $
M6    12000.60C           0.5                                                  $
       8016.60C           0.5                                                  $
C                                                                              $
C     SALT REFLECTOR.                                                          $
C                                                                              $
M7    11023.60C           0.5                                                  $
      17000.60C           0.5                                                  $
C                                                                              $
C     CONCRETE                                                                 $
C     Composition from Handbook of Health Physics and Radiological Health      $
C     3rd Edition for Ordinary Concrete.                                       $
C                                                                              $
M8     1001.60c  -0.0056      8016.60c  -0.4981     11023.60c  -0.0171         $
      12000.60c  -0.0026     13027.60c  -0.0457     14000.60c  -0.3151         $
      16032.60c  -0.0013     19000.60c  -0.0192     20000.60c  -0.0829         $
      26054.60c  -0.0007316  26056.60c  -0.011373   26057.60c  -0.000260        $
      26058.60c  -3.472e-005                                                   $
MT8   LWTR.01T                                                                 $
C                                                                              $
C     OUPUT                                                                    $
C                                                                              $
PRINT                                                                          $
```

A.7.5 MCNP Input File Listing for Impacted 55-gallon Drum Array (Filename dacf142)

```
CCCC
```

```
C     DRUMS CONTAIN A H2O-POLY MODERATOR WHICH IS MIXED WITH THE PU. THE H2O-   $
C     POLY MODERATOR IS 25% BY VOLUME POLY AND 75% BY VOLUME WATER. THE FISSILE $
C     MASSES ARE CENTRALLY LOCATED IN THE FOUR (4) FISSILE BEARING DRUM AND     $
C     ARE ELLIPTICAL IN SHAPE WITH A MAJOR AXIS TO MINOR AXIS RATIO OF 2.0.    $
C     IN ORDER TO SIMULATE A CRUSHED CONDITION, IT IS ASSUMED THAT THE VOLUME   $
C     AVAILABLE FOR THE INTERNAL REFLECTOR HAS BEEN REDUCED TO 75% OF THE       $
C     DESIGN VOLUME OF THE 55-GALLON DRUM. AS A RESULT, THE FISSILE MASSES ARE $
C     REFLECTED BY 5 KGS. OF BERYLLIUM MIXED WITH 0% DENSE POLYETHYLENE.        $
C     THE THREE (3) NON-FISSILE BEARING ARE FILLED WITH THE SAME REFLECTOR      $
C     MATERIAL AS THE FISSILE BEARING DRUMS. THE DRUM STEEL WALL DENSITY IS 50% $
C     TO ACCOUNT FOR DEGRADATION. THE 7-PACKS ARE STACKED 3-HIGH WITH A MGO     $
C     LAYER ON TOP. THE UPPER AND LOWER VERTICAL PLANES ARE REFLECTED BY        $
C     300 CM OF SALT. THE LATERAL BOUNDARIES ARE MIRRORED ON THREE SIDES TO     $
C     SIMULATE INFINITE REFLECTION IN THREE OF THE LATERAL PLANE. ON THE FRONT   $
C     PLANE, THE CRUSHED DRUMS ARE REFLECTED BY 200 CM OF LEAD.                 $
C                                                                               $
C CCCC
```

```
2  REC   0 0  0.1214 0 0 84.5764 34.9971 0 0 17.4985                    $
3  REC   0 0  0.0000 0 0 84.6978 35.1185 0 0 17.6199                    $
C                                                                       $
C     CELL SURFACE FOR THE 200 FGE DRUM.                               $
C                                                                       $
4  REC   0 0 31.5370 0 0 21.6237 15.2903 0 0  7.6451                    $
5  REC   0 0  0.1214 0 0 84.5764 34.9971 0 0 17.4985                    $
6  REC   0 0  0.0000 0 0 84.6978 35.1185 0 0 17.6199                    $
C                                                                       $
C     SURFACE CARDS FOR THE BE-POLY DRUM.                              $
C                                                                       $
7  REC   0 0  0.1214 0 0 84.5764 34.9971 0 0 17.4985                    $
8  REC   0 0  0.0000 0 0 84.6978 35.1185 0 0 17.6199                    $
C                                                                       $
C     SURFACE CARDS FOR THE RECTANGULAR LATTICE.                       $
C                                                                       $
9  PX    35.1185                                                        $
10 PX   -35.1185                                                        $
11 PY    17.6199                                                        $
12 PY   -17.6199                                                        $
13 PZ    84.6978                                                        $
14 PZ     0.0000                                                        $
*15 PX  105.3554                                                        $
*16 PX -105.3554                                                        $
*17 PY   52.8596                                                        $
18 PY   -52.8596                                                        $
19 PZ    254.0933                                                       $
20 PZ    0.000                                                          $
C                                                                       $
C     SURFACE CARDS FOR THE MGO AND SALT LAYERS.                       $
C                                                                       $
25 PZ   316.3234                                                        $
26 PZ   254.0933                                                        $
27 PZ   616.3234                                                        $
28 PZ  -300.0000                                                        $
C                                                                       $
C     SURFACE CARDS FOR THE LEAD SHIELD LAYER.                         $
C                                                                       $
30 PY  -252.8596                                                        $
                                                                        $
C                                                                       $
C  DATA CARDS.                                                         $
C                                                                       $
MODE N                                                                  $
C                                                                       $
C  SOURCE CARDS.                                                       $
C                                                                       $
KCODE 5000 1.0 50 250                                                   $
KSRC  0  0   40.000                                                     $
      0  0  125.000                                                     $
      0  0  205.000                                                     $
C                                                                       $
C  MATERIAL CARDS                                                       $
C                                                                       $
C                                                                       $
C  PU-H2O-POLY FOR THE FISSILE MASS CONTAINING 50 GRAMS OF PU.          $
C                                                                       $
M1    94239.60C     -0.025101                                           $
       1001.60C     -0.116417                                           $
       8016.60C     -0.661824                                           $
       6000.60C     -0.196657                                           $
MT1   LWTR.01T   POLY.01T                                               $
C                                                                       $
C  PU-H2O-POLY FOR THE FISSILE MASS CONTAINING 200 GRAMS OF PU.         $
C                                                                       $
M2    94239.60C     -0.025101                                           $
       1001.60C     -0.116417                                           $
       8016.60C     -0.661824                                           $
       6000.60C     -0.196657                                           $
MT2   LWTR.01T   POLY.01T                                               $
```

```
C                                                                       $
C  BE REFLECTOR AROUND THE FISSILE MASS CONTAINING 50 GRAMS PU.         $
C                                                                       $
M3     4009.60C     -1.000000                                           $
MT3   BE.01T                                                           $
C                                                                       $
C  BE REFLECTOR AROUND THE FISSILE MASS CONTAINING 200 GRAMS PU.        $
C                                                                       $
M4     4009.60C     -1.000000                                          $
MT4   BE.01T                                                           $
C                                                                       $
C  BE REFLECTOR IN THE NON-FISSILE MASS DRUMS.                          $
C                                                                       $
M5     4009.60C     -1.000000                                          $
MT5   BE.01T                                                           $
C                                                                       $
C  55-GALLON DRUM STEEL WALLS.                                          $
C                                                                       $
M6     6000.60C     -0.001500                                          $
      25055.60C     -0.006000                                          $
      15031.60C     -0.000350                                          $
      16000.60C     -0.000400                                          $
      26054.60C     -0.058513                                          $
      26056.60C     -0.909630                                          $
      26057.60C     -0.020827                                          $
      26058.60C     -0.0027769                                         $
C                                                                       $
C  MGO LAYER.                                                           $
C                                                                       $
M7    12000.60C           0.5                                          $
      8016.60C            0.5                                          $
C                                                                       $
C  SALT REFLECTOR.                                                      $
C                                                                       $
M8    11023.60C           0.5                                          $
      17000.60C           0.5                                          $
C                                                                       $
C  LEAD REFLECTOR.                                                      $
C                                                                       $
M9    82206.60c      0.24100000                                        $
      82207.60c      0.22100000                                        $
      82208.60c      0.52400000                                        $
C                                                                       $
C     PRINT TABLE 40 FOR MASS FRACTIONS                                 $
C                                                                       $
PRINT 40                                                               $
C                                                                       $
C     PRINT TO MCTAL FILE                                               $
C                                                                       $
PRDMP 2j 1                                                             $
```

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Appendix B Direct-Loaded Waste Containing Greater Than 1 Weight Percent Special Reflectors

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Note: Appendix B is unaffected by Revision 8 and no changes were made from the previous revision. Original signatures are on file with WIPP-016 Revision 7.

Note: An extent of condition was performed to Revision 7 of this NCSE to confirm all established limits, assumptions, and judgements. As part of the review, it was identified in Section B.3.3, which documents the analysis for the Container Overstack scenario, that an assumption was made that the ceiling height in waste disposal rooms in the WIPP underground does not support stacking of waste four tiers high with an MgO supersack, which is incongruent with other WIPP NCSE appendices. WIPP-099 (*Extent of Condition Review for WIPP-016, Rev. 7*) documents the analysis of the container overstack scenario with the MgO supersack to justify removing this assumption. This change will be incorporated into this NCSE in a future revision.

Analyst in Training NCS Engineer	N. Dickes	Date
Analyst Senior NCS Engineer	S. L. Larson	Date
Peer Reviewer Senior NCS Engineer	W. D. Newmyer	Date

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Introduction

This appendix focuses on direct-loaded waste containers containing greater than 1 wt% of special reflector material. Special reflector materials are those that have been shown to increase reactivity above that of a 25% polyethylene/75% water-reflected system and must be limited when mass loading limits are based on this polyethylene/water reflection combination. Containers with limits on special reflector materials are discussed in Appendix A. Beryllium is modeled as the special reflector material, as it has been shown to result in the highest reactivity when reflecting a plutonium system in *Reactivity Effects of Moderator and Reflector Materials on a Finite Plutonium System* (Neeley et al. 2004). 100 grams of ^{239}Pu and 100 kilograms of beryllium per drum is modeled based on minimizing impact to generator site operations. In the SWB, 100 grams of ^{239}Pu is also modeled but the beryllium content is not limited. Sample MCNP5 input file listings for the models contained in this appendix are included in Section B.6.

B.1 Waste Configurations for Direct-Loaded Waste with Greater Than 1 Weight Percent Special Reflector Materials

B.1.1 55-gallon Drums

The direct-loaded 55-gallon drums are modeled with 100 grams of ^{239}Pu mixed with a polyethylene-water moderator. The 100 kilograms of beryllium is introduced in varying amounts into the moderator and the remainder is modeled as a reflector. Without beryllium, the moderator is 25% by volume polyethylene and 75% by volume water.

The 100 kilograms of beryllium is considered to be in particulate form in compounds such as beryllium oxide (BeO) or as metal waste from machining processes. Beryllium evaluated both as a moderator and as a reflector is consistent with Section 6.4.3.2.2 of the *TRUPACT-II Safety Analysis Report* (DOE-CBFO 2005a) where beryllium is shown slightly more reactive modeled in the reflector than in the moderator. In the moderator, beryllium is modeled at full density for conservatism. However, when modeled as a reflector around ^{239}Pu, beryllium is modeled at 70% density. The use of 100% dense beryllium, although bounding, is not possible in these waste drums per *Review of Special Reflectors in the TRU Waste Inventory* (Taggert and Moon 2004). Because the beryllium consists of molds, shapes, chunks, coarse particles and fines randomly filling the waste container instead of being specifically constructed to surround the fissile material and fill the container with no void, beryllium at 70% of theoretical density or 1.295 g/cm^3 is used given that the maximum theoretical density for randomly packed uniform spheres is 70% (“Recursive packing of dense particle mixtures” [Elliot et al. 2002] and “Is random packing of spheres well defined?” [Torquato et al. 2007]). Both polyethylene and void are evaluated in the remainder of the drum. The polyethylene is modeled at a maximum packing fraction of 25% as determined to bound the packing fraction of direct-loaded (non-machine compacted) waste in the TRUPACT-II SAR.

The 55-gallon drum dimensions given in Table 2-1 are used in the MCNP5 models. The drum walls are carbon steel (*Standard Specification for Steel, Carbon (0.15 Maximum, Percent), Hot-Rolled Sheet and Strip Commercial* [ASTM A 569]), which is modeled with the composition given in Table 5-5. The theoretical density of carbon steel is 7.86 g/cm^3, but is modeled at 50% of this value, or 3.93 g/cm^3, to allow for fabrication tolerances, localized wall thinning, or other degradation. Section 2.1.2 of the *Contact-Handled Transuranic Waste Authorized Methods for Payload Control (CH-TRAMPAC)* (DOE-CBFO 2005b) requires that the integrity of the container be visually inspected prior to transport to ensure there is no significant rusting whereas the 50% value is conservative.

B.1.2 Standard Waste Box (SWB)

As discussed in Section A.1.2, direct-loaded waste may also be loaded into SWBs. These containers are modeled with the dimensions given in Table 2-3; the steel is modeled with the composition given in Table 5-5 at half the theoretical density as per Section A.1.2.

B.2 Array Models

B.2.1 55-gallon Drum Array Model

The seven-pack 55-gallon drum array model discussed in Appendix A was used to evaluate the 100-gram ^{239}Pu system with 100 kilograms of beryllium per drum. The fissile mass is modeled as a cylinder located in the center of each drum, and the H/D ratio of the cylinder is 1. The beryllium was modeled in varying amounts as a moderator with the amount not used as moderator modeled as a reflector. Figure B-1 and Figure B-2 show a typical configuration. The weight ratios for the fissile material input into MCNP5 are summarized in Table B-1.

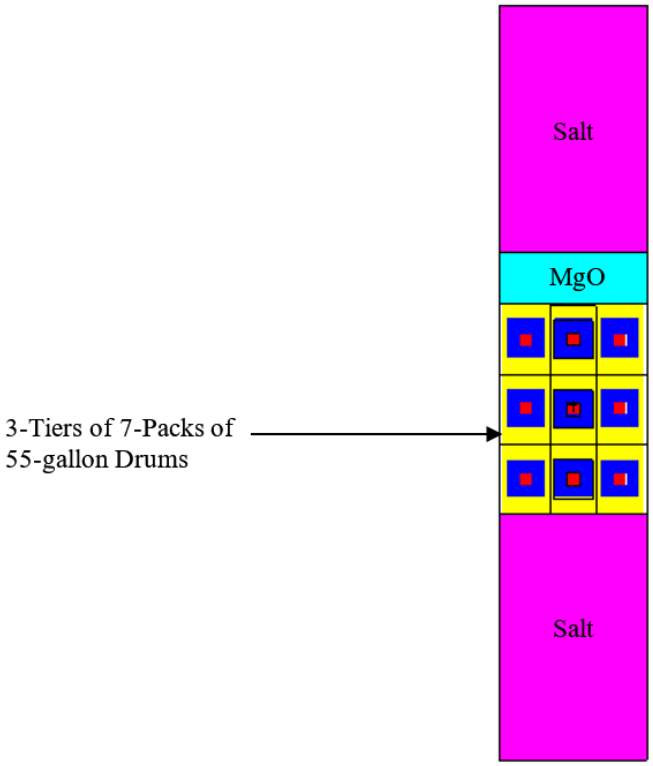

Figure B-1. Typical 55-gallon Drum Seven-pack Array Model, X-Z Plane

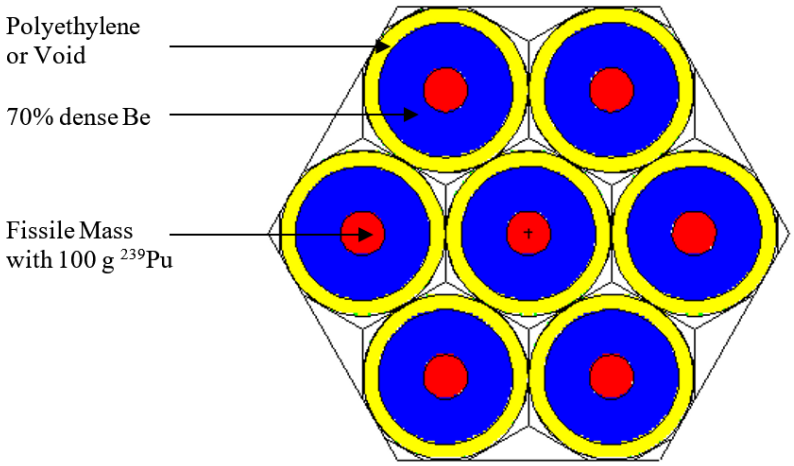

Figure B-2. Typical 55-gallon Drum Seven-pack Array Model, X-Y Plane

Table B-1. Parameters for 100 FGE Cylinder in 55-gallon Drum Seven-pack Array Model

H/Pu Ratio	Density (g/cm^3)	Pu (wt fraction)	H (wt fraction)	O (wt fraction)	C (wt fraction)	beryllium (wt fraction)	Cylinder Radius (cm)
0% Beryllium, 25% Polyethylene, 75% Water in Moderator							
700	1.0170	0.038887	0.114771	0.652466	0.193876	0.00000	7.3830
800	1.0123	0.034193	0.115331	0.655653	0.194823	0.00000	7.7184
900	1.0087	0.030509	0.115771	0.658153	0.195566	0.00000	8.0269
1000	1.0057	0.027542	0.116125	0.660167	0.196165	0.00000	8.3134
1100	1.0033	0.025101	0.116417	0.661824	0.196657	0.00000	8.5814
1200	1.0013	0.023058	0.116661	0.663212	0.197070	0.00000	8.8336
10% Beryllium, 22.5% Polyethylene, 67.5% Water in Moderator							
800	1.0959	0.028430	0.095893	0.545149	0.161988	0.168500	7.9938
20% Beryllium, 20% Polyethylene, 60% Water in Moderator							
800	1.1796	0.023483	0.079207	0.450286	0.133800	0.313200	8.3134
40% Beryllium, 15% Polyethylene, 45% Water in Moderator							
800	1.3470	0.015428	0.052040	0.295843	0.087908	0.548800	9.1490
60% Beryllium, 10% Polyethylene, 30% Water in Moderator							
800	1.5146	0.009151	0.030866	0.175473	0.052141	0.732400	10.4718
80% Beryllium, 5% Polyethylene, 15% Water in Moderator							
800	1.6822	0.004120	0.013900	0.079020	0.023480	0.879500	13.1921
100% Beryllium, 0% Polyethylene, 0% Water in Moderator							
15000	1.8530	0.001765	0.00000	0.00000	0.00000	0.998235	16.9453
20000	1.8522	0.001325	0.00000	0.00000	0.00000	0.998675	18.6505
25000	1.8518	0.001060	0.00000	0.00000	0.00000	0.998940	20.0904

First, a seven-pack with 700 grams of ^{239}Pu (100 grams of ^{239}Pu/drum) was modeled with varying amounts of beryllium, water, and polyethylene in the moderator and the remainder of the 100 kilograms of beryllium modeled as a reflector. Figure B-3 shows that the 100 kilograms of beryllium is more reactive as a reflector. Next, the polyethylene was replaced with void. Figure B-3 shows this as a more reactive configuration, and unlike the external polyethylene, the void causes the reactivity to increase with increasing beryllium moderator. The results for these cases are tabulated in Table B-2. To evaluate 100% beryllium moderation (i.e., no polyethylene or water in the moderator), the beryllium/plutonium ratio in the fissile material was optimized as before by varying the amount of beryllium in the moderator with the remainder of the 100 kilograms modeled as a reflector. The beryllium in the moderator is modeled at 100% density while the beryllium in the reflector is at 70% dense. Thus, no assumptions are made on how the beryllium-plutonium compound was formed. Figure B-4 and Table B-3 show that a beryllium-plutonium ratio of approximately 20,000 is most reactive. With 100 kilograms at this beryllium-plutonium ratio, there are approximately 75 kilograms of beryllium in the moderator and 25 kilograms of beryllium in the reflector. Additional cases with 80 and 90 kilograms of beryllium instead of 100 kilograms are included in Table B-3, which shows that less beryllium is less reactive. All cases are below the USL with the highest $k_{eff} + 2\sigma$ value being less than 0.90. Thus, 55-gallon drums containing 100 FGE per drum and 100 kilograms of beryllium will remain subcritical in the seven-pack array configuration.

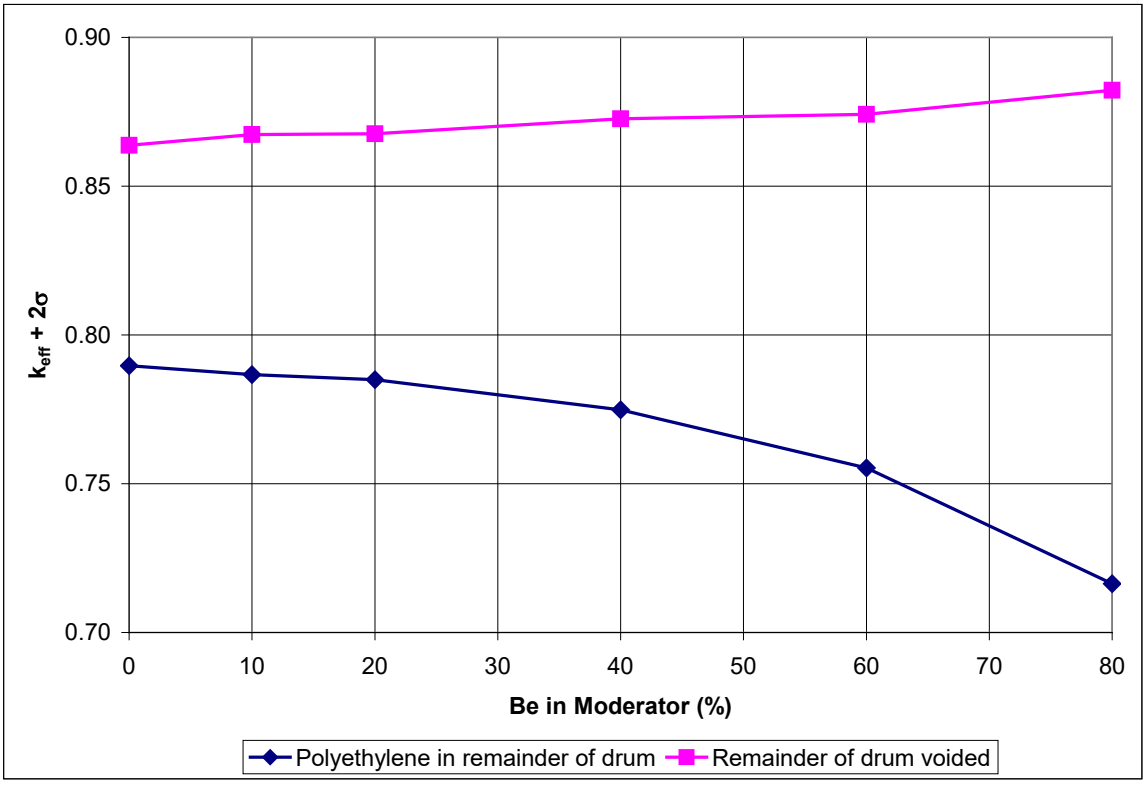

Figure B-3. Seven-pack Array Reactivity with 100 g ^{239}Pu/drum as a Function of Beryllium Moderation (H/Pu=800)

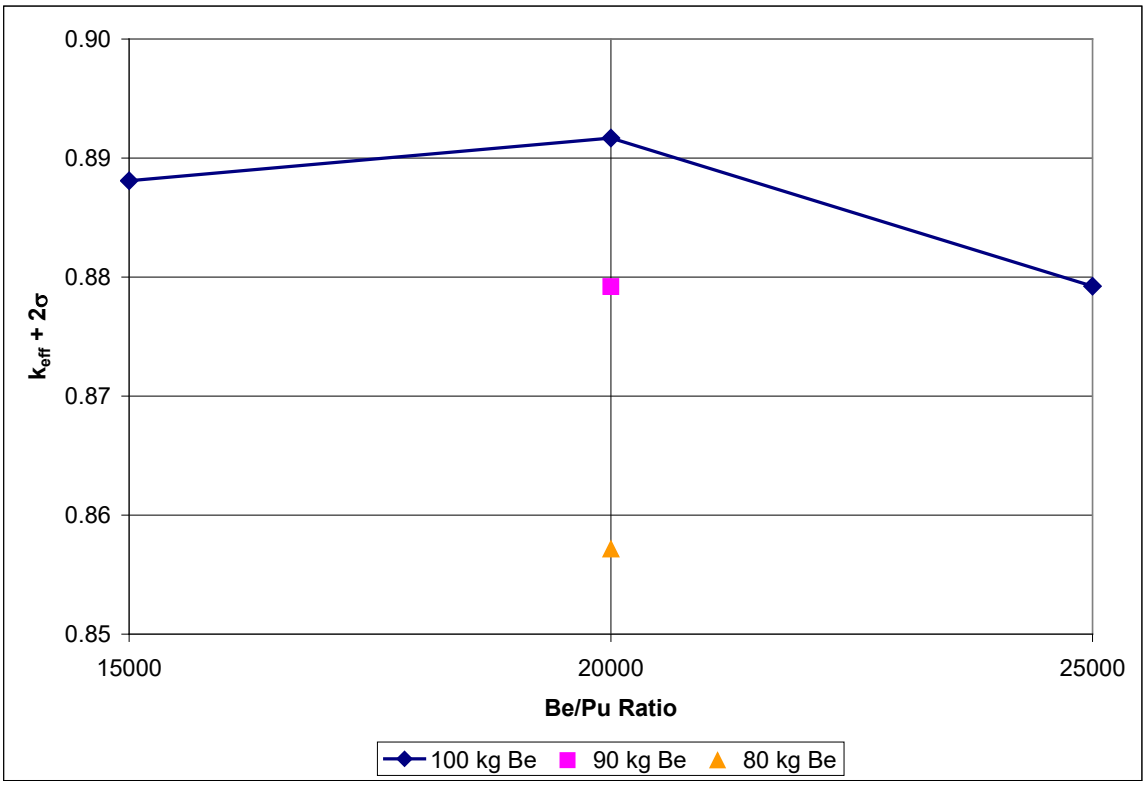

Figure B-4. Seven-pack Array Reactivity with 100 g ^{239}Pu/drum as a Function of Beryllium/Plutonium Ratio

Table B-2. Beryllium Moderator Results for 55-gallon Drum Seven-pack Array Model with 100 FGE/drum (H/Pu Ratio = 800)

% Be in Moderator	Remaining Drum Fill	keff	σ	keff + 2σ	Filename
0	Polyethylene	0.78800	0.00083	0.78966	b700a0
10	Polyethylene	0.78513	0.00078	0.78669	b700a1
20	Polyethylene	0.78347	0.00076	0.78499	b700a2
40	Polyethylene	0.77326	0.00080	0.77486	b700a4
60	Polyethylene	0.75370	0.00081	0.75532	b700a6
80	Polyethylene	0.71489	0.00074	0.71637	b700a8
0	Void	0.86218	0.00077	0.86372	a708v0
10	Void	0.86588	0.00074	0.86736	a708v1
20	Void	0.86608	0.00078	0.86764	a708v2
40	Void	0.87127	0.00068	0.87263	a708v4
60	Void	0.87258	0.00077	0.87412	a708v6
80	Void	0.88078	0.00073	0.88224	a708v8

Table B-3. 100% Beryllium Moderator Results for 55-gallon Drum Seven-pack Array Model with 100 FGE/drum

Be/Pu Ratio	Be (kg)	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
15000	100	0.88673	0.00068	0.88809	a15kb
20000	100	0.89027	0.00071	0.89169	a20kb
25000	100	0.87803	0.00060	0.87923	a25kb
20000	90	0.87782	0.00069	0.87920	a20kb9
20000	80	0.85578	0.00069	0.85716	a20kb8

B.2.2 SWB Array Model

Following the model described in Section A.2.2, an SWB array was considered. Each SWB contained 100 grams of ^{239}Pu with the remaining volume filled with 70% dense beryllium (the subsequent beryllium mass was approximately 2500 kg). The beryllium, water, and polyethylene amounts were varied in the moderator with the remainder of the beryllium modeled as a reflector. Comparison of the results in Table B-4, Table B-5, and Table B-6 shows that the beryllium is most reactive as a reflector. The H/Pu ratio was varied in this most reactive case and the results given in Table B-4. All cases are below the USL with the highest $k_{eff} + 2\sigma$ value being 0.80815 for an H/Pu ratio of 1,000. To further investigate the effect of beryllium, two additional cases were evaluated. First, Table B-5 confirms beryllium is most reactive when modeled as a reflector instead of a moderator. Second, Table B-6 shows that moderation by beryllium only is the least reactive configuration, with the peak $k_{eff} + 2\sigma$ value less than 0.7 for a Be/Pu ratio of 15,000. The size of the SWB container reduces the interaction between the containers, and the reactivity of the SWB array is less than that of the 55-gallon drum array discussed in the Section B.2.1. Thus, SWBs with 100 FGE and unlimited beryllium per container will remain subcritical.

Table B-4. Results for SWB Array Model with 100 FGE/SWB and Unlimited Beryllium as a Reflector

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
800	0.80081	0.00088	0.80257	aswb08f
900	0.80415	0.00093	0.80601	aswb09f
1000	0.80629	0.00093	0.80815	aswb10f
1100	0.80422	0.00084	0.80590	aswb11f
1200	0.80277	0.00085	0.80447	aswb12f
1300	0.79936	0.00082	0.80100	aswb13f

Table B-5. Results for SWB Array Model with 100 FGE/SWB (H/Pu Ratio = 1000) and Unlimited Beryllium as a Moderator and Reflector

% Be in Moderator	Remaining SWB Fill	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
0	Beryllium	0.80629	0.00093	0.80815	aswb10f
10	Beryllium	0.80281	0.00090	0.80461	aswbf1
40	Beryllium	0.79285	0.00086	0.79457	aswbf4
80	Beryllium	0.74068	0.00084	0.74236	aswbf8

Table B-6. Results for SWB Array Model with 100 FGE/SWB and Beryllium Moderation

Be/Pu Ratio	Remaining SWB Fill	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
10000	Beryllium	0.67077	0.00083	0.67243	aswbf10
15000	Beryllium	0.68581	0.00085	0.68751	aswbf15
20000	Beryllium	0.68562	0.00086	0.68734	aswbf20
25000	Beryllium	0.67774	0.00081	0.67936	aswbf25
35000	Beryllium	0.65372	0.00073	0.65518	aswbf35

B.3 Two-container Models

B.3.1 55-gallon Direct-Loaded Two-Drum Model

The two-container 55-gallon drum model discussed in Appendix A was used to evaluate the 100-gram ^{239}Pu system with 100 kilograms of beryllium. The fissile mass in the top drum is located in the bottom of the drum and the fissile mass in the bottom drum is located in the top; the H/D ratio of the combined cylinders is 1. Magnesium oxide is modeled as the external reflector (300 centimeters thick) in the initial calculations with concrete and salt reflection also considered later in the analysis. The beryllium was modeled in varying amounts in the moderator with the mass not used in the moderator modeled in the reflector region. Figure B-5 shows a typical 55-gallon drum, two-container configuration; the parameters for the fissile material input into MCNP5 are given in Table B-7.

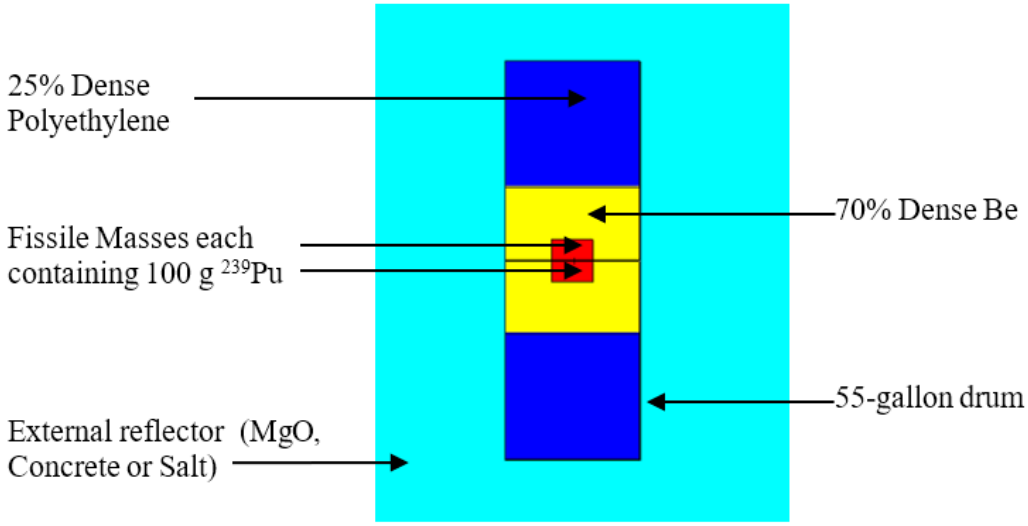

Figure B-5. Typical 55-gallon Drum Two-container Model

Table B-7. Parameters for 100 FGE Cylinder in 55-gallon Drum Two-Container Model

H/Pu Ratio	Density (g/cm^3)	Pu (wt. fraction)	H (wt. fraction)	O (wt. fraction)	C (wt. fraction)	Be (wt. fraction)	Cylinder Radius (cm)
0% Beryllium, 25% Polyethylene, 75% Water in Moderator							
600	1.0232	0.045076	0.114032	0.648264	0.192628	0.00000	8.83703
700	1.0170	0.038887	0.114771	0.652466	0.193876	0.00000	9.30195
800	1.0123	0.034193	0.115331	0.655653	0.194823	0.00000	9.72453
900	1.0087	0.030509	0.115771	0.658153	0.195566	0.00000	10.11327
1000	1.0057	0.027542	0.116125	0.660167	0.196165	0.00000	10.47421
10% Beryllium, 22.5% Polyethylene, 67.5% Water in Moderator							
600	1.1057	0.037551	0.094993	0.540032	0.160467	0.167000	9.15220
700	1.1001	0.032360	0.095505	0.542944	0.161333	0.167900	9.63380
800	1.0959	0.028430	0.095893	0.545149	0.161988	0.168500	10.07154
900	1.0927	0.025351	0.096197	0.546877	0.162501	0.169100	10.47421
1000	1.0901	0.022874	0.096442	0.548267	0.162914	0.169500	10.84810
1100	1.0879	0.020838	0.096643	0.549409	0.163254	0.169900	11.19785
20% Beryllium, 20% Polyethylene, 60% Water in Moderator							
600	1.1883	0.031067	0.078591	0.446789	0.132761	0.310800	9.51793
700	1.1833	0.026748	0.078942	0.448780	0.133352	0.312200	10.01889
800	1.1796	0.023483	0.079207	0.450286	0.133800	0.313200	10.47421
900	1.1767	0.020928	0.079414	0.451464	0.134150	0.314000	10.89306
1000	1.1744	0.018875	0.079580	0.452411	0.134431	0.314700	11.28195
1100	1.1725	0.017188	0.079717	0.453188	0.134662	0.315200	11.64574
40% Beryllium, 15% Polyethylene, 45% Water in Moderator							
600	1.3535	0.020466	0.051773	0.294330	0.087458	0.546000	10.47421
700	1.3498	0.017594	0.051925	0.295193	0.087715	0.547600	11.02575
800	1.3470	0.015428	0.052040	0.295843	0.087908	0.548800	11.52702
900	1.3449	0.013738	0.052129	0.296351	0.088059	0.549700	11.98812
1000	1.3432	0.012381	0.052201	0.296759	0.088180	0.550500	12.41624
1100	1.3417	0.011268	0.052260	0.297093	0.088280	0.551100	12.81671
60% Beryllium, 10% Polyethylene, 30% Water in Moderator							
600	1.5188	0.012164	0.030772	0.174939	0.051982	0.730100	11.98812
700	1.5164	0.010445	0.030826	0.175244	0.052073	0.731400	12.61966
800	1.5146	0.009151	0.030866	0.175473	0.052141	0.732400	13.19361
900	1.5131	0.008143	0.030898	0.175652	0.052194	0.733100	13.72155
1000	1.512	0.007334	0.030923	0.175795	0.052236	0.733700	14.21173
1100	1.5111	0.006672	0.030943	0.175912	0.052271	0.734200	14.67023
80% Beryllium, 5% Polyethylene, 15% Water in Moderator							
600	1.6843	0.005487	0.013881	0.078912	0.023448	0.878300	15.10174
700	1.6831	0.004707	0.013892	0.078974	0.023467	0.879000	15.89765
800	1.6822	0.004121	0.013900	0.079020	0.023480	0.879500	16.62097
900	1.6815	0.003665	0.013906	0.079056	0.023491	0.879900	17.28629
1000	1.6810	0.003299	0.013911	0.079085	0.023500	0.880200	17.90398
1100	1.6805	0.003000	0.013915	0.079109	0.023507	0.880500	18.48177

First, beryllium was evaluated as a moderator and as a reflector. Polyethylene was modeled in the remainder of the drum since this increases reflection in the two-container model compared to modeling void. Figure B-6 shows that the 100 kilograms of beryllium is more reactive as a reflector than as a moderator and reflector in the two-container configuration. This is consistent with the results in Section 6.4.3.2.2 of the TRUPACT-II SAR (DOE-CBFO 2005a), which also modeled 100 FGE in a single unit. The array model is more reactive with beryllium moderation because it results in a larger fissile volume at a lower fissile concentration with less beryllium reflector compared to the beryllium-reflected case. In the array model, the larger fissile volume results in more interaction between the containers and increases reactivity; therefore, the thinner beryllium reflector layer also allows for more interaction. In contrast, in the two-container model, the lower fissile concentration reduces the reactivity as the fissile material is more like a fully reflected single unit.

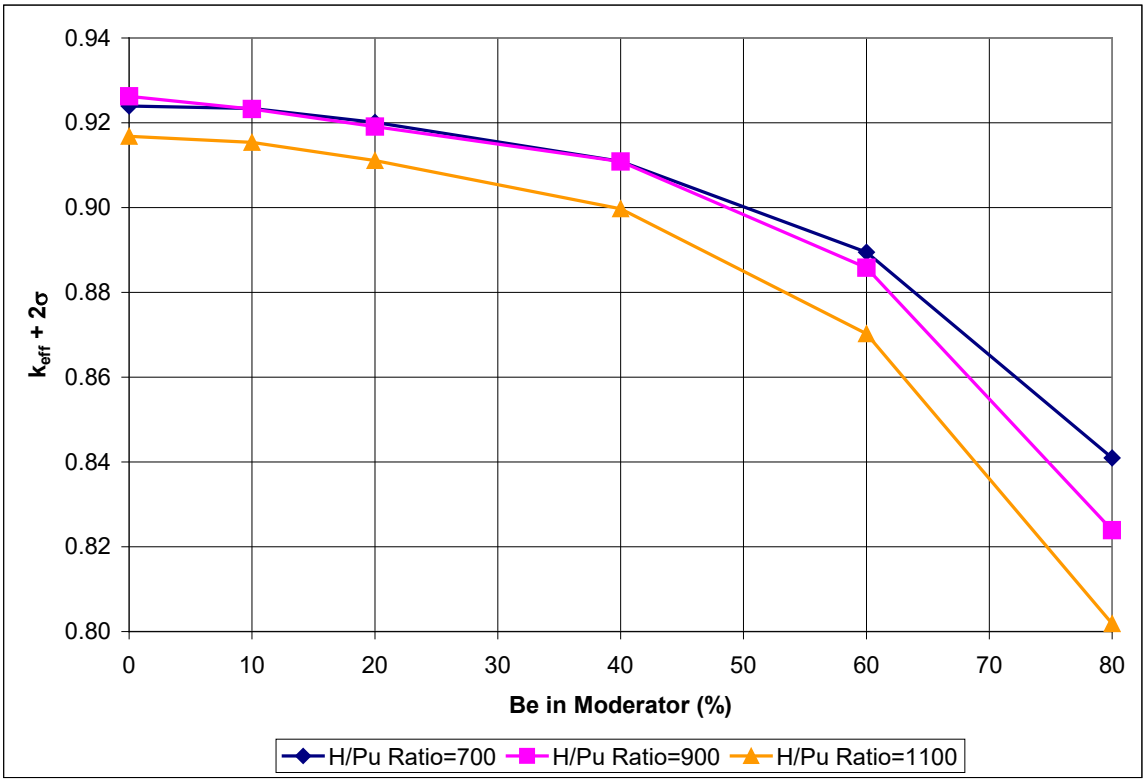

Figure B-6. Two-Container Reactivity as a Function of Beryllium Location

Next, the H/Pu ratio in the fissile material was varied to determine the optimum value. Figure B-6 shows that an H/Pu ratio of approximately 800 is most reactive (with a 25% polyethylene, 75% water and 0% beryllium moderator). Additional cases with 10 and 20% beryllium in the moderator are included for illustration and verification that 0% beryllium is most reactive. Table B-8 summarizes the beryllium moderation results from Figure B-6 and Figure B-7.

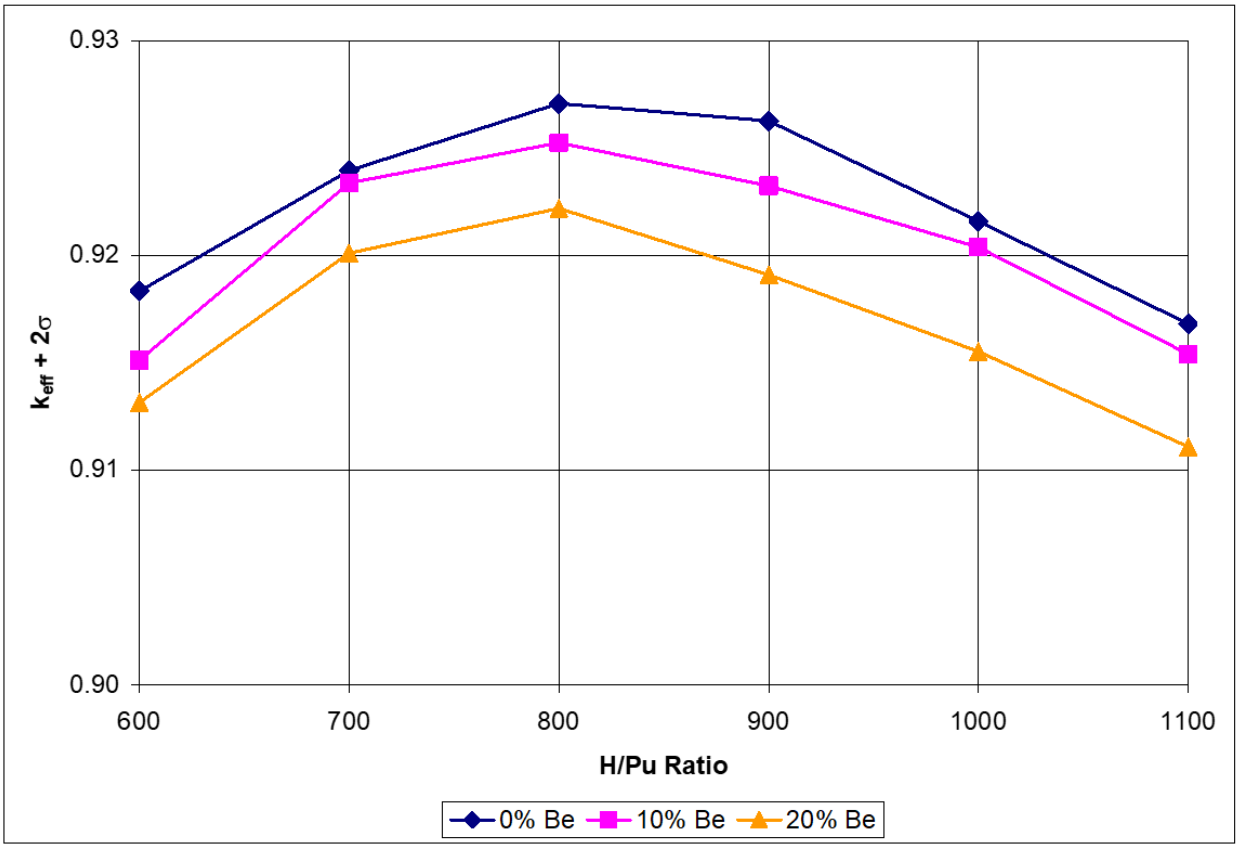

Figure B-7. Two-Container Reactivity as a Function of H/Pu Ratio

Table B-8. Beryllium Moderator Results for 55-gallon Drum Two-Container Model with 100 FGE/Drum

H/Pu Ratio	% Be in Moderator	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
600	0	0.91625	0.00104	0.91833	b0006m
700	0	0.92205	0.00095	0.92395	b0007m
800	0	0.92503	0.00102	0.92707	b0008m
900	0	0.92410	0.00108	0.92626	b0009m
1000	0	0.91968	0.00095	0.92158	b0010m
1100	0	0.91477	0.00102	0.91681	b0011m
600	10	0.91285	0.00113	0.91511	b1006m
700	10	0.92107	0.00115	0.92337	b1007m
800	10	0.92311	0.00107	0.92525	b1008m
900	10	0.92103	0.00110	0.92323	b1009m
1000	10	0.91828	0.00105	0.92038	b1010m
1100	10	0.91342	0.00099	0.91540	b1011m
600	20	0.91086	0.00114	0.91314	b2006m
700	20	0.91790	0.00110	0.92010	b2007m
800	20	0.92000	0.00109	0.92218	b2008m
900	20	0.91687	0.00111	0.91909	b2009m
1000	20	0.91336	0.00108	0.91552	b2010m
1100	20	0.90898	0.00105	0.91108	b2011m
700	40	0.90866	0.00113	0.91092	b4007m
900	40	0.90874	0.00106	0.91086	b4009m
1100	40	0.89768	0.00101	0.89970	b4011m
700	60	0.88725	0.00112	0.88949	b6007m
900	60	0.88374	0.00103	0.88580	b6009m
1100	60	0.86815	0.00104	0.87023	b6011m
700	80	0.83882	0.00106	0.84094	b8007m
900	80	0.82173	0.00109	0.82391	b8009m
1100	80	0.79989	0.00098	0.80185	b8011m

Lastly, the exterior reflector material around the drums was varied to include concrete and salt. The optimum fissile material moderator of 25% polyethylene and 75% water without beryllium, as found in Table B-8, is modeled. The results for the model as a function of H/Pu ratio in the moderator are given in Figure B-8 and Table B-9. Although concrete reflection appears slightly higher for some H/Pu ratios, the difference is statistically insignificant and all cases are well below the USL with the highest $k_{eff} + 2\sigma$ value being less than 0.93. Therefore, 55-gallon drums containing 100 FGE will remain subcritical in the two-container configuration.

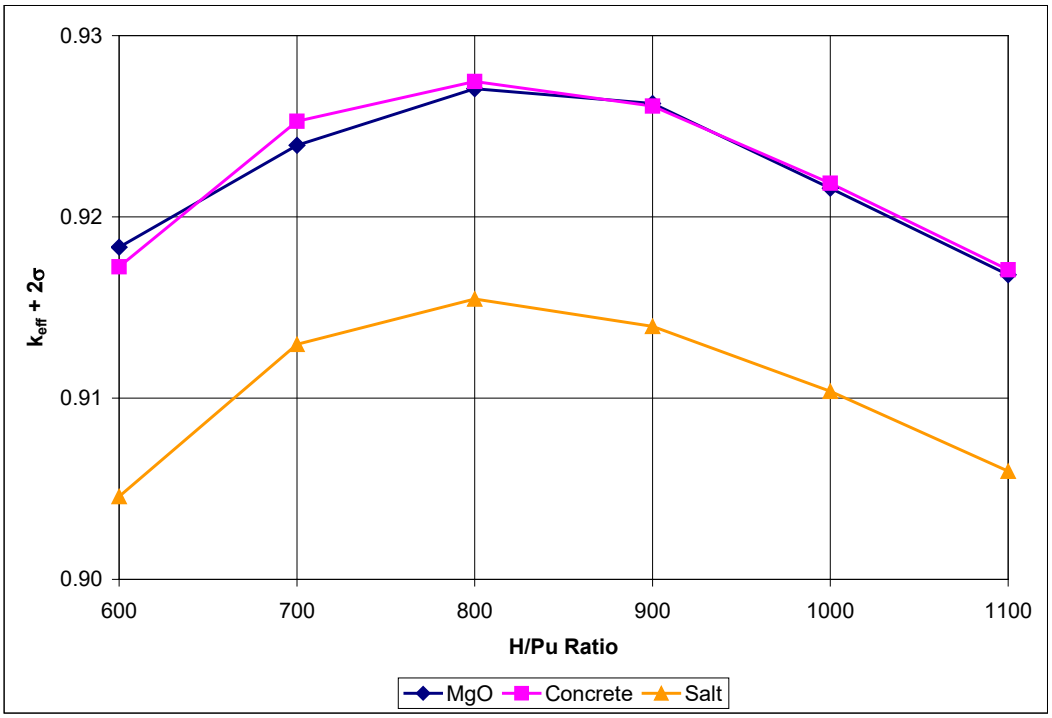

Figure B-8. Two-Container Reactivity as a Function of External Reflector

Table B-9. Exterior Reflector Results For 55-Gallon Drum Two-Container Model With 100 FGE/Drum

H/Pu Ratio	Reflector	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
600	MgO	0.91625	0.00104	0.91833	b0006m
700	MgO	0.92205	0.00095	0.92395	b0007m
800	MgO	0.92503	0.00102	0.92707	b0008m
900	MgO	0.92410	0.00108	0.92626	b0009m
1000	MgO	0.91968	0.00095	0.92158	b0010m
1100	MgO	0.91477	0.00102	0.91681	b0011m
600	Concrete	0.91513	0.00106	0.91725	b0006c
700	Concrete	0.92324	0.00102	0.92528	b0007c
800	Concrete	0.92551	0.00098	0.92747	b0008c
900	Concrete	0.92415	0.00098	0.92611	b0009c
1000	Concrete	0.91994	0.00096	0.92186	b0010c
1100	Concrete	0.91524	0.00092	0.91708	b0011c
600	Salt	0.90249	0.00104	0.90457	b0006s
700	Salt	0.91075	0.00111	0.91297	b0007s
800	Salt	0.91353	0.00097	0.91547	b0008s
900	Salt	0.91200	0.00098	0.91396	b0009s
1000	Salt	0.90858	0.00090	0.91038	b0010s
1100	Salt	0.90395	0.00101	0.90597	b0011s

B.3.2 SWB Direct-loaded Two-Container Model

Following the model described in Section A.3.2, two SWBs are modeled using the same parameters as in Section B.1.2. The previous sections show that MgO and concrete reflection results in similar reactivity with salt reflection having a slightly lower reactivity. Thus, only MgO reflection was modeled with the SWB. Table B-10 shows the maximum $k_{eff} + 2\sigma$ value was less than 0.921 at H/Pu = 800 even with the SWBs filled with beryllium and externally fully reflected. Thus the 2-SWB model remains subcritical with a loading of 100 FGE per SWB.

Table B-10. Results for SWB Two-Container Model with 100 FGE/SWB and Unlimited Beryllium

H/Pu Ratio	Reflector	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
600	MgO	0.91037	0.00094	0.91225	2swb06f
700	MgO	0.91671	0.00093	0.91857	2swb07f
800	MgO	0.91918	0.00090	0.92098	2swb08f
900	MgO	0.91837	0.00084	0.92005	2swb09f
1000	MgO	0.91500	0.00070	0.91640	2swb10f
1100	MgO	0.90922	0.00081	0.91084	2swb11f

B.3.3 Container Overstack Model

The overstack scenario evaluates an infinitely reflected, four-tier seven-pack array of 55-gallon drums. There are 100 grams of ^{239}Pu and 100 kilograms of beryllium in each container. The 55-gallon drums are modeled with the beryllium in the moderator as shown to be most reactive in Section B.2.1. The MgO supersacks are modeled on top of the fourth tier and the salt is modeled on the top and bottom of the stack as in the three-tier model. Table B-11 shows that the maximum reactivity for the 55-gallon drum array occurs at a beryllium/plutonium ratio of 20,000 and exceeds the USL of 0.96 but is less than 0.97 (the USL without administrative margin). In addition to operator error with regard to stacking, a significant mining error would have to occur to allow enough clearance to stack the drums four tiers throughout the panel with the MgO supersack on top. The optimum case is modeled by replacing the MgO supersack with salt as a more credible condition, as there would not be room for the MgO on top of the fourth tier of drums throughout the array. The reactivity is reduced below the USL to less than 0.89 indicating that this contingent event will remain subcritical.

Table B-11. Results for an Array of 55-Gallon Drums Stacked Four Tiers High

Be/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
Four Tiers of 55-gallon Drums with MgO Supersack				
15000	0.95533	0.00084	0.95701	a415kb
20000	0.96490	0.00069	0.96628	a420kb
25000	0.95579	0.00068	0.95715	a425kb
Four Tiers of 55-gallon Drums without MgO Supersack				
20000	0.88835	0.00069	0.88973	a420kbm

B.3.4 Fissile Overbatch Model

Two overbatch scenarios are considered in this section. The first one evaluates a single 55-gallon drum in the center of a seven-pack array in the middle tier overbatched by 50% to 150 grams of ^{239}Pu. The other containers contain 100 grams of ^{239}Pu. In the 55-gallon drums, the fissile mixture in to the 100 gram drums is mixed with the beryllium at the optimum beryllium/plutonium ratio of 20,000 from Section B.2.1. Typically, a 50% overbatch has been evaluated. However, the combination of 150 grams of ^{239}Pu and 100 kilograms of beryllium, at the optimum beryllium/plutonium ratio of 20,000, is not physically possible. Therefore, two alternative cases were evaluated. First, 150 grams of ^{239}Pu and 100 kilograms of beryllium were modeled in the overbatched drum at the maximum possible beryllium/plutonium ratio of 17,683.6 and lower. Second, the maximum amount of ^{239}Pu for a beryllium/plutonium ratio of 20,000 and 100 kilograms of beryllium, which is 132.6273 g, was evaluated. The results in Table B-12 show that all cases are below the USL with the highest $k_{eff} + 2\sigma$ value remaining below 0.91.

The second overbatch case evaluates the SWB array with all three containers conservatively overbatched 50% to 150 grams of ^{239}Pu and the remaining volume filled with 70% dense beryllium. The SWB is explicitly modeled as it is not limited to 100 kilograms of beryllium so the additional reflection needed to be evaluated with the overmass. As discussed in Section B.2.2, the size of the SWB isolates the individual containers and the results in Table B-13 show that all cases are below the USL with the highest $k_{eff} + 2\sigma$ value remaining below 0.91.

Table B-12. Overbatch Case Results for 55-gallon Drum Array Model

Be/Pu Ratio	^{239}Pu in Overbatch (g)	^{239}Pu in Overbatch (wt. frac)	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
100 kg Be in Moderator						
10000	150	0.002646	0.90077	0.00075	0.90227	ao10kb
15000	150	0.001765	0.90248	0.00070	0.90388	ao15kb
17683.6	150	0.001498	0.90142	0.00068	0.90278	ao17kb
20000	132.6	0.001325	0.89684	0.00067	0.89818	ao20kb

Table B-13. Overbatch Case Results for SWB Array Model

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
SWB filled with approximately 2500 kg Be in Reflector				
600	0.89198	0.00100	0.89398	oswb06f
700	0.90158	0.00095	0.90348	oswb07f
800	0.90779	0.00087	0.90953	oswb08f
900	0.90588	0.00089	0.90766	oswb09f
1000	0.90594	0.00091	0.90776	oswb10f
1100	0.90194	0.00095	0.90384	oswb11f
1200	0.89658	0.00084	0.89826	oswb12f
1300	0.89028	0.00082	0.89192	oswb13f

B.3.5 Excess Beryllium Model

The excess beryllium scenario evaluates a single drum in the center of the middle tier of a seven-pack array with beryllium filling the drum around the fissile mass. The results in Table B-14 for 55-gallon drums show that all cases are below the USL with the highest $k_{eff} + 2\sigma$ value less than 0.89.

Table B-14. Excess Beryllium Results for 55-gallon Drum Array Model

Be/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
100 kg Be in Moderator				
15000	0.88197	0.00077	0.88351	ae15kb
20000	0.88708	0.00067	0.88842	ae20kb
25000	0.87759	0.00064	0.87887	ae25kb

B.3.6 Underground Roof Fall Model

The compaction scenario considers the lower tier of a seven-pack array reduced by 15 inches in height as a result of roof fall in the underground repository. The results in Table B-15 show that all cases are well below the USL as the highest $k_{eff} + 2\sigma$ value is less than 0.90. In fact, this upset condition has little impact on k_{eff} compared to the maximum normal condition result is 0.89169 per Table B-3. The SWB is already filled with 70% dense beryllium such that the fissile material is already well reflected and each unit is isolated from one another. In addition, the SWB arrays have a lower reactivity than the 55-gallon drum array under normal conditions and thus are not modeled separately for this contingency.

Table B-15. Compaction Case Results for 55-gallon Drum Seven-pack Array Model with 100 FGE/drum

Be/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
15000	0.89480	0.00070	0.89620	ac15kb
20000	0.89660	0.00066	0.89792	ac20kb
25000	0.88332	0.00066	0.88464	ac25kb

B.4 Conclusions

This appendix demonstrates that direct loaded 55-gallon drums or SWBs with greater than 1 wt% special reflector materials will remain below the USL in the two-container configuration as well in the underground array with the following limits:

- Maximum 100 FGE/drum or SWB, and
- Maximum 100 kilograms of beryllium/drum (no Be limit for SWB).

B.5 References

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Elliot J.A., A. Kelly, and A.H. Windle, 2002. "Recursive packing of dense particle mixtures," J. Mat. Sci. Lett. **21**:1249-1251; 2002.

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B.6 Sample MCNP5 Input File Listings for Appendix B

B.6.1 55-gallon Drum Two-Container Model (Filename b0007m)

```
STACKED 55 GAL DRUMS, APPEND B. BOTH DRUMS W/ 100G PU,  0% BE MOD, H/PU = 700  $
C     FGE WITH MIXED WITH A BE-POLY-WATER MODERATOR:  0% BE WITH POLY-WATER    $
C     (25% BY VOLUME POLY AND 75% BY VOLUME WATER). THE FISSILE MASS           $
C     IS REFLECTED BY THE REMAINING BE (100 KG MINUS BE IN FGE CYLINDER) AT    $
C     70% PACKING FRACTION AND POLYETHYLENE AT 25% PACKING FRACTION.          $
C     THE DRUMS ARE STACKED DIRECTLY ONE ON TOP OF ANOTHER WITH THE FISSILE    $
C     MASS IN THE LOWER DRUM BEING LOCATED AT THE TOP OF THE DRUM AND THE      $
C     FISSILE MASS IN THE UPPER DRUM BEING LOCATED IN THE BOTTOM OF THE DRUM. $
C     IN THIS CONFIGURATION THE FISSILE MASSES ARE IN CLOSE PROXIMITY.        $
C     BOTH FISSILE MASSES ARE CYLINDRICAL IN SHAPE WITH A H/D RATIO OF 0.5.   $
C     CONTAINER WALL DENSITY (STEEL) IS 50% TO ACCOUNT FOR DEGRADATION.       $
C     THE TWO-DRUM STACK IS SURROUNDED ON ALL SIDES WITH  300 CM OF MgO.      $
C     THE BOUNDARIES ARE MIRRORED TO SIMULATE INFINITE REFLECTION. 10/12/07   $
C                                                                              $
C CCCC
```

```
2         PZ   84.57641                                                    $
3         PZ   75.27466                                                    $
4         CZ   28.57500                                                    $
5         PZ   84.57641                                                    $
6         PZ    0.12141                                                    $
7         CZ   28.69641                                                    $
8         PZ   84.69782                                                    $
9         PZ    0.00000                                                    $
10        PZ   53.48783                                                    $
C                                                                          $
C     SURFACE CARDS FOR THE UPPER 55 GALLON DRUM IN THE TWO-DRUM MODEL.    $
C                                                                          $
22        PZ  115.90781                                                    $
23  1     CZ   28.57500                                                    $
24  1     PZ   84.57641                                                    $
25  1     PZ    0.12141                                                    $
26  1     CZ   28.69641                                                    $
27  1     PZ   84.69782                                                    $
28  1     PZ    0.00000                                                    $
C                                                                          $
C     SURFACE CARDS FOR A 300 CM REFLECTOR AROUND THE TWO DRUMS            $
C                                                                          $
*100       CZ  328.69641                                                   $
*101       PZ  469.39564                                                   $
*102       PZ -300.00000                                                   $

C                                                                          $
C     MODE CARD.                                                           $
C                                                                          $
MODE N                                                                     $
C                                                                          $
C     TRANSFORMATION CARDS FOR THE TWO-DRUM MODEL.                         $
C                                                                          $
TR1   0.00000     0.00000    84.69782                                      $
C                                                                          $
C     MATERIAL CARDS                                                       $
C                                                                          $
C     PU-BE-CH2-H2O (55 GALLON DRUM)                                       $
C                                                                          $
M1    94239.60C -0.038887     1001.60C -0.114771                    &      $
       8016.60C -0.652466     6000.60C -0.193876                           $
C                                                                          $
C     CH2 REFLECTOR (55 GALLON DRUM)                                       $
C                                                                          $
M2     6000.60C -0.856188  1001.60C -0.143812                              $
C                                                                          $
C     BE REFLECTOR (55 GALLON DRUM)                                        $
C                                                                          $
M3     4009.60C 1                                                          $
C                                                                          $
C     CARBON STEEL DRUM.                                                   $
C                                                                          $
M6     6000.60C -0.001500  25055.60C -0.006000  15031.60C -0.000350    &   $
      16000.60C -0.000400  26054.60C -0.058513  26056.60C -0.909630    &   $
      26057.60C -0.020827  26058.60C -0.0027769                            $
C                                                                          $
C     MgO                                                                  $
C                                                                          $
M7      8016.60C -0.39700  12000.60C -0.603000                             $
C                                                                          $
C     S(ALPHA,BETA)                                                        $
C                                                                          $
MT1   LWTR.01T   GRPH.01T                                                  $
MT2   POLY.01T   GRPH.01T                                                  $
MT3   BE.01T                                                               $
C                                                                          $
C     SOURCE CARDS                                                         $
C                                                                          $
KCODE 1000     1.0      50   800                                         $
KSRC  0.00000  0.00000  80.00000                                          $
```

```
PRINT                                                                          $
```

B.6.2 55-gallon Drum Array Model (Filename b700a1)

```
55-gallon Drum Array Case, 700 G TOTAL, 10%BE/22.5%POLY/67.5%H20 MODERATOR
C     INFINITE ARRAY 7-PACK MODEL OF 55-GALLON DRUMS WITH 7 55-GALLON          $
C     DRUMS CONTAINING 100 GRAMS PU AT H/PU = 800. ALL FISSILE BEARING         $
C     DRUMS CONTAIN A H2O-POLY MODERATOR WHICH IS MIXED WITH THE PU. THE H2O-  $
C     POLY MODERATOR % IS BY VOLUME. THE FISSILE MASSES ARE CENTRALLY LOCATED  $
C     IN THE FISSILE BEARING DRUMS AND ARE CYLINDRICAL WITH A H/D RATIO OF 1.0.$
C     THE FISSILE MASSES ARE REFLECTED BY THE REMAINING BE (100 KG MINUS       $
C     BE IN FGE CYLINDER) IN A CYLINDER AT 70% DENSITY WITH H/D=1.0 AND THE    $
C     REMAINING VOLUME WITH POLYETHYLENE AT A DENSITY OF 25% OF THEORETICAL.   $
C     THE DRUM STEEL WALL DENSITY IS 50% TO ACCOUNT FOR DEGRADATION. THE 7-PACKS$
C     ARE STACKED 3-HIGH WITH A MGO LAYER ON TOP. THE UPPER AND LOWER VERTICAL $
C     PLANES ARE REFLECTED BY 300 CM OF SALT. THE LATERAL BOUNDARIES ARE       $
C     MIRRORED TO SIMULATE INFINITE REFLECTION IN THE LATERAL PLANE. 10/21/07  $
C                                                                              $
C CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC$
C                                                                              $
C     CELL CARDS FOR THE 100 FGE DRUMS.                                        $
C                                                                              $
1     1    -1.0959   -14                              U=1    IMP:N=1          $
2     3    -1.295     14  -11                         U=1    IMP:N=1          $
3     4    -0.2308    11  -2 -10  8                   U=1    IMP:N=1          $
4     6    -3.93      (2:10:-8) -4 6 -12              U=1    IMP:N=1          $
5     0               (4:-6:12)                       U=1    IMP:N=1          $
C                                                                              $
C     CELL CARDS FOR THE HEXAGONAL 7-PACK STACK.                               $
C                                                                              $
12    0               -21 20 -22 25 -23 24 -27 26 LAT=2 U=4    IMP:N=1          $
                       FILL=-3:3 -3:3 0:2                                     $
                       4 16R                                                  $
                           1 1   4 4 4 4                                      $
                          1 1 1  4 4 4 4                                      $
                           1 1   4 16R                                        $
                       4 16R                                                  $
                           1 1   4 4 4 4                                      $
                          1 1 1  4 4 4 4                                      $
                           1 1   4 16R                                        $
                       4 16R                                                  $
                           1 1   4 4 4 4                                      $
                          1 1 1  4 4 4 4                                      $
                           1 1   4 16R                                        $
13    0               -61 60 -62 65 -63 64 -67 66 FILL=4       IMP:N=1          $
C                                                                              $
C     CELL CARDS FOR THE MGO AND SALT LAYERS.                                  $
C                                                                              $
14    8    -2.165     (53:-66) -61 60 -62 65 -63 64 50 -52     IMP:N=1          $
15    7    -1.45      -61 60 -62 65 -63 64 67 -53              IMP:N=1          $
C                                                                              $
C     CELL CARDS FOR THE REST OF THE UNIVERSE.                                 $
C                                                                              $
16    0               -50:52:61:-60:62:-65:63:-64              IMP:N=0          $

C                                                                              $
C     SURFACE CARDS FOR ALL DRUM SUFFACES                                      $
C                                                                              $
2  CZ  28.575                                                                  $
4  CZ  28.696                                                                  $
6  PZ  0.0                                                                     $
8  PZ  0.121                                                                   $
10 PZ  84.576                                                                  $
12 PZ  84.697                                                                  $
C                                                                              $
C     CELL CARDS FOR THE 100 FGE DRUMS.                                        $
C                                                                              $
11 RCC 0 0  19.0008 0 0  46.6963  23.3481   $BE around 100 FGE                  $
```

```
14 RCC 0 0  34.3551 0 0  15.9876   7.9938   $100 FGE                          $
C                                                                             $
C     SURFACE CARDS FOR THE HEXAGONAL 7-PACK.                                 $
C                                                                             $
20 PX -28.75                                                                  $
21 PX  28.75                                                                  $
22 P   1    1.7321    0    57.5                                               $
23 P  -1    1.7321    0    57.5                                               $
24 P  -1    1.7321    0   -57.5                                               $
25 P   1    1.7321    0   -57.5                                               $
26 PZ  0.0                                                                    $
27 PZ  84.697                                                                 $
C                                                                             $
C     SURFACE CARDS FOR THE MGO AND SALT LAYERS.                              $
C                                                                             $
50 PZ -300.00                                                                 $
52 PZ  616.321                                                                $
53 PZ  316.321                                                                $
C                                                                             $
C     SURFACE CARDS FOR THE 7-PACK STACK INFINITE ARRAY.                      $
C                                                                             $
*60 PY -78.5                                                                  $
*61 PY  78.5                                                                  $
*62 P   1.7321   1    0   157                                                 $
*63 P   1.7321  -1    0   157                                                 $
*64 P   1.7321  -1    0  -157                                                 $
*65 P   1.7321   1    0  -157                                                 $
66 PZ   0.0                                                                   $
67 PZ   254.091                                                               $

C                                                                             $
C  DATA CARDS.                                                               $
C                                                                             $
MODE N                                                                        $
C                                                                             $
C  SOURCE CARDS.                                                             $
C                                                                             $
KCODE 5000 1.0 50 250                                                         $
KSRC -58 0 43    -30 -50 43                                                   $
     -58 0 128   -30 -50 128                                                  $
     -58 0 213   -30 -50 213                                                  $
C                                                                             $
C  MATERIAL CARDS                                                            $
C                                                                             $
C                                                                             $
C  PU-H2O-POLY FOR THE FISSILE MASS CONTAINING 100 GRAMS OF PU.               $
C                                                                             $
M1    94239.60C -0.028430     1001.60C -0.095893                      &       $
       8016.60C -0.545149     6000.60C -0.161988  4009.60C -0.168500          $
MT1   LWTR.01T   GRPH.01T    BE.01T                                           $
C                                                                             $
C  BE REFLECTOR AROUND THE FISSILE MASS CONTAINING 100 GRAMS PU.              $
C                                                                             $
M3    4009.60C      -1.000000                                                 $
MT3   BE.01T                                                                  $
C                                                                             $
C     CH2 REFLECTOR (55 GALLON DRUM)                                          $
C                                                                             $
M4    6000.60C -0.856188  1001.60C -0.143812                                  $
MT4   POLY.01T   GRPH.01T                                                     $
C                                                                             $
C  55-GALLON DRUM STEEL WALLS.                                                $
C                                                                             $
M6     6000.60C     -0.001500                                                 $
      25055.60C     -0.006000                                                 $
      15031.60C     -0.000350                                                 $
      16000.60C     -0.000400                                                 $
      26054.60C     -0.058513                                                 $
      26056.60C     -0.909630                                                 $
      26057.60C     -0.020827                                                 $
```

```
      26058.60C     -0.0027769                                                  $
C                                                                               $
C  MGO LAYER.                                                                  $
C                                                                               $
M7    12000.60C           0.5                                                   $
      8016.60C            0.5                                                   $
C                                                                               $
C  SALT REFLECTOR.                                                             $
C                                                                               $
M8    11023.60C           0.5                                                   $
      17000.60C           0.5                                                   $
C                                                                               $
C     PRINT TABLE 40 FOR MASS FRACTIONS                                         $
C                                                                               $
PRINT 40                                                                        $
55-gallon Drum Array Overbatch Model (Filename ao15kb)
55-gallon Drum Array Case, 750 G TOTAL, 100%BE, BE/PU=15000, EXCESS BE, 150 FGE
C     INFINITE ARRAY 7-PACK MODEL OF 55-GALLON DRUMS WITH 7 55-GALLON           $
C     DRUMS CONTAINING 100 GRAMS PU AT BE/PU=20000. ALL FISSILE BEARING DRUMS   $
C     CONTAIN A BE MODERATOR WHICH IS MIXED WITH THE PU. THE FISSILE            $
C     MASSES ARE CENTRALLY LOCATED IN THE FISSILE BEARING DRUMS AND             $
C     ARE CYLINDRICAL IN SHAPE WITH A H/D RATIO OF 1.0. THE FISSILE MASSES     $
C     ARE REFLECTED BY A BERYLLIUM CYLINDER (100 KG - BE IN THE FISSILE MASS)   $
C     AT 70% DENSITY WITH H/D=1.0 AND REMAINING VOLUME WITH VOID.              $
C     THE CENTER DRUM IS 150 GRAMS PU FISSILE MASS AT BE/PU AS PER TITLE        $
C     THE DRUM STEEL WALL DENSITY IS 50% TO ACCOUNT FOR DEGRADATION. THE 7-PACKS$
C     ARE STACKED 3-HIGH WITH A MGO LAYER ON TOP. THE UPPER AND LOWER VERTICAL $
C     PLANES ARE REFLECTED BY 300 CM OF SALT. THE LATERAL BOUNDARIES ARE       $
C     MIRRORED TO SIMULATE INFINITE REFLECTION IN THE LATERAL PLANE. 11/01/07  $
C                                                                               $
C CCCC
```

```
C                                                                          $
C     CELL CARDS FOR THE REST OF THE UNIVERSE.                            $
C                                                                          $
16    0               -50:52:61:-60:62:-65:63:-64             IMP:N=0      $

C                                                                          $
C     SURFACE CARDS FOR THE 150 FGE DRUM                                   $
C                                                                          $
31  RCC 0 0  21.4227 0 0  41.8524   20.9262  $BE REFLECTOR                  $
34  RCC 0 0  22.9514 0 0  38.7951   19.3975  $FGE                           $
C                                                                          $
C     SURFACE CARDS FOR ALL DRUM SUFFACES                                  $
C                                                                          $
2  CZ  28.575                                                              $
4  CZ  28.696                                                              $
6  PZ  0.0                                                                 $
8  PZ  0.121                                                               $
10 PZ  84.576                                                              $
12 PZ  84.697                                                              $
C                                                                          $
C     CELL CARDS FOR THE 100 FGE DRUMS.                                   $
C                                                                          $
11 RCC 0 0  21.1618 0 0  42.3743  21.1871   $BE around 100 FGE             $
14 RCC 0 0  23.6984 0 0  37.3009  18.6505   $100 FGE                       $
C                                                                          $
C     SURFACE CARDS FOR THE HEXAGONAL 7-PACK.                             $
C                                                                          $
20 PX -28.75                                                               $
21 PX  28.75                                                               $
22 P   1    1.7321    0    57.5                                            $
23 P  -1    1.7321    0    57.5                                            $
24 P  -1    1.7321    0   -57.5                                            $
25 P   1    1.7321    0   -57.5                                            $
26 PZ  0.0                                                                 $
27 PZ  84.697                                                              $
C                                                                          $
C     SURFACE CARDS FOR THE MGO AND SALT LAYERS.                          $
C                                                                          $
50 PZ -300.00                                                              $
52 PZ  616.321                                                             $
53 PZ  316.321                                                             $
C                                                                          $
C     SURFACE CARDS FOR THE 7-PACK STACK INFINITE ARRAY.                   $
C                                                                          $
*60 PY -78.5                                                               $
*61 PY  78.5                                                               $
*62 P   1.7321   1    0   157                                             $
*63 P   1.7321  -1    0   157                                             $
*64 P   1.7321  -1    0  -157                                             $
*65 P   1.7321   1    0  -157                                             $
66 PZ   0.0                                                                $
67 PZ   254.091                                                            $

C                                                                          $
C  DATA CARDS.                                                            $
C                                                                          $
MODE N                                                                     $
C                                                                          $
C  SOURCE CARDS.                                                           $
C                                                                          $
KCODE 5000 1.0 50 250                                                      $
KSRC -58 0 43    -30 -50 43                                                $
     -58 0 128   -30 -50 128                                               $
     -58 0 213   -30 -50 213                                               $
C                                                                          $
C  MATERIAL CARDS                                                          $
C                                                                          $
C  PU-BE FOR THE FISSILE MASS CONTAINING 100 GRAMS OF PU.                  $
C                                                                          $
M1    94239.60C -0.001325     4009.60C -0.998675                           $
```

```
MT1   BE.01T                                                              $
C                                                                         $
C  PU-BE FOR THE FISSILE MASS CONTAINING 150 GRAMS OF PU.                $
C                                                                         $
M2    94239.60C -0.001765     4009.60C -0.998235                          $
MT2   BE.01T                                                              $
C                                                                         $
C  BE REFLECTOR AROUND THE FISSILE MASS                                   $
C                                                                         $
M3    4009.60C      -1.000000                                             $
MT3   BE.01T                                                              $
C                                                                         $
C  55-GALLON DRUM STEEL WALLS.                                            $
C                                                                         $
M6     6000.60C     -0.001500                                            $
      25055.60C     -0.006000                                            $
      15031.60C     -0.000350                                            $
      16000.60C     -0.000400                                            $
      26054.60C     -0.058513                                            $
      26056.60C     -0.909630                                            $
      26057.60C     -0.020827                                            $
      26058.60C     -0.0027769                                           $
C                                                                         $
C  MGO LAYER.                                                             $
C                                                                         $
M7    12000.60C           0.5                                           $
      8016.60C            0.5                                           $
C                                                                         $
C  SALT REFLECTOR.                                                        $
C                                                                         $
M8    11023.60C           0.5                                           $
      17000.60C           0.5                                           $
C                                                                         $
C     PRINT TABLE 40 FOR MASS FRACTIONS                                   $
C                                                                         $
PRINT 40                                                                  $
```

Appendix C Machine-Compacted Waste

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Analyst in Training NCS Engineer	HONG JUN ZHU (Affiliate) Digitally signed by HONG JUN ZHU (Affiliate) Date: 2026.07.14 05:57:22 -06'00' H.J. Zhu	Date
Analyst NCS Engineer	 Digitally signed by Derrick Faunce DN: cn=Derrick Faunce, ou=21 Consulting Group, Inc., email=dfaunce@21cgi.com, c=US Date: 2026.07.14 08:07:16 -04'00' D. Faunce	Date
Analyst NCS Engineer	NEIL DICKES (Affiliate) Digitally signed by NEIL DICKES (Affiliate) Date: 2026.07.14 07:21:57 -06'00' N. Dickes	Date
Peer Reviewer Senior NCS Engineer	Sandi Larson Digitally signed by Sandi Larson DN: C=US, OU="21 Consulting Group, Inc.", CN=Sandi Larson, E=slarson@21cgi.com Date: 2026-07-14 08:29:21 S. L. Larson	Date

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Introduction

This appendix focuses on compacted waste in 55-gallon drums, 100-gallon drums, and SWBs. Compacting is typically performed mechanically on 55-gallon drums and the resulting machine-compacted drum is called a "puck." Approximately four pucks are loaded into a 100-gallon drum and sent to the WIPP for disposal. Direct loading of an SWB with pucks is also evaluated. The criticality safety limits are given for the outer container, not the compacted puck. For analysis purposes, the steel of the compacted puck is ignored and the fissile material is modeled in a compact geometry as if all fissile material in the drum was contained in one puck. In reality, the fissile material will likely be spread throughout the pucks and the steel wall of the compacted drum will absorb neutrons. Consequently, the modeled configuration is conservative from a criticality safety perspective. Special reflector materials are limited to less than 1 wt% and are modeled as beryllium consistent with the previous appendices. Both two-container and array configurations are considered. All models in this appendix were updated to MCNP6.2 in Revision 8. Sample MCNP6.2 input file listings are included in Section C.9.

C.1 Machine-Compacted Waste Configurations

C.1.1 Fully Compacted Waste in 100-gallon Drums

This configuration evaluates the drum contents fully compacted and the non-fissile material in the drum, modeled as polyethylene, reaches theoretical density. Thus, the fissile mass is moderated with 100% dense polyethylene. The drums are modeled with two fissile limits using the fissile mixture parameters detailed in Table 5-1. The first limit of 170 grams of ^{239}Pu does not credit any difference in the internal and external dimension when the drums are stacked. The second higher fissile mass is 200 grams of ^{239}Pu and only applies when the design of the container lid and bottom that provides inherent spacing between the internal contents of two stacked drums is credited. With both limits, the fissile mass is reflected by a 100% dense mixture of polyethylene and beryllium. The beryllium content in the reflector mixture is 5 kilograms, which is slightly is slightly greater than 1% by weight of the rated 1,000-pound weight capacity of the drum *Contact-Handled Transuranic Waste Authorized Methods for Payload Control (CH-TRAMPAC)* (DOE-CBFO 2022). The beryllium is spread uniformly through the reflector region mixed with polyethylene at its theoretical density. The 100-gallon drum is modeled with the dimensions given in Table 2-2, and the steel drum wall is modeled with the composition given in Table 5-5 at 50% density to allow for degradation.

C.1.2 Partially Compacted Waste in 100-gallon Drums

Because 100% compaction may be overly conservative with regard to the compaction that can physically be achieved, limits are also determined based on 70% compaction. This scenario is also evaluated in the *TRUPACT-II Safety Analysis Report* (DOE-CBFO 2025) and will require the waste generator to control the compaction process. The fissile mass in this model consists of 200 grams of ^{239}Pu moderated with a polyethylene-water mixture, which is 70% by volume polyethylene and 30% by volume water. This fissile mixture is detailed in Table 5-2 and is consistent with the approved TRUPACT-II contents model used in the criticality safety analysis for partially compacted waste. Reflection of the fissile mass with a 70% dense mixture of 5 kilograms of beryllium and polyethylene is modeled. As with the fully compacted case, the beryllium is spread uniformly through the polyethylene reflector. The 100-gallon drum is modeled with the dimensions given in Table 2-2, and the steel drum wall is modeled with the composition given in Table 5-5 at 50% density to allow for degradation.

C.1.3 Fully Compacted Waste Direct-Loaded in a Standard Waste Box

Only full compaction is considered for the contents of the SWB. Thus, moderation of the fissile mass is modeled with 100% dense polyethylene and the fissile mass is reflected with a 100% dense mixture of beryllium and polyethylene. The fissile mass consists 200 grams of ^{239}Pu in a SWB, and its mixture parameters are detailed in Table 5-1. The beryllium content in the reflector mixture is 18.14 kilograms, which represents 1% by weight of the rated weight capacity of the SWB. The 18.14 kilograms of beryllium is homogeneously distributed throughout the polyethylene filling the SWB. The SWB is modeled with the dimensions given in Table 2-3, which results in an interior volume of 1.92×10^6 cm^3, and the steel wall is modeled with the composition given in Table 5-5 at 60% density to allow for degradation.

C.1.4 Fully Compacted Waste in 55-gallon Drums

Although machine-compacted waste is typically packaged in 100-gallon drums, fully compacted waste with 200 FGE in 55-gallons drums is also analyzed to avoid restricting future operations. The model is identical to that described in Section C.1.1 except the container dimensions of a 55-gallon drum from Table 2-1 are used.

C.1.5 Partially Compacted Waste in 55-gallon Drums

Partially compacted waste based on 70% compaction and 200 FGE is also analyzed in 55-gallon drums. The model is identical to that described in Section C.1.2 except the container dimensions of a 55-gallon drum from Table 2-1 are used.

C.2 Array Models Containing Machine-compacted Waste

An infinite array model simulating the worst-case normal configuration for storage of drums or SWBs containing machine-compacted waste is constructed. Geometrically, the fissile mass mixture is modeled as a cylinder with an H/D ratio of 1. A cylindrical puck with this aspect ratio has the same surface-to-volume ratio as that of a sphere, and the reactivity effect, when reflected, is very close to that of a sphere with equivalent mass and moderation. The fissile cylinder is centrally located in the container. With random placement of the fissile unit in each container, the average center-to-center separation in either the horizontal or vertical direction will be statistically the same as that of the array with all fissile masses centered in the containers. Drum configurations are emplaced on a hexagonal lattice unit with pitch characteristics typical of a three-pack of 100-gallon drums or a seven-pack of 55-gallon drums. The drums or SWBs are stacked three tiers high and all lateral surfaces are mirrored to simulate an infinite array. In the array models, the lower horizontal plane is reflected with 300 centimeters of salt and the upper plane is reflected by 62.23 centimeters of magnesium oxide (MgO) backed by 300 centimeters of salt. This reflector configuration represents a conservative bound on the underground repository reflector conditions with an MgO supersack on top of the storage containers. The array configuration is consistent with the array models discussed in the previous appendices. Figure C-1 summarizes the pertinent features of the baseline array model used in the analysis for 100-gallon drums as an example.

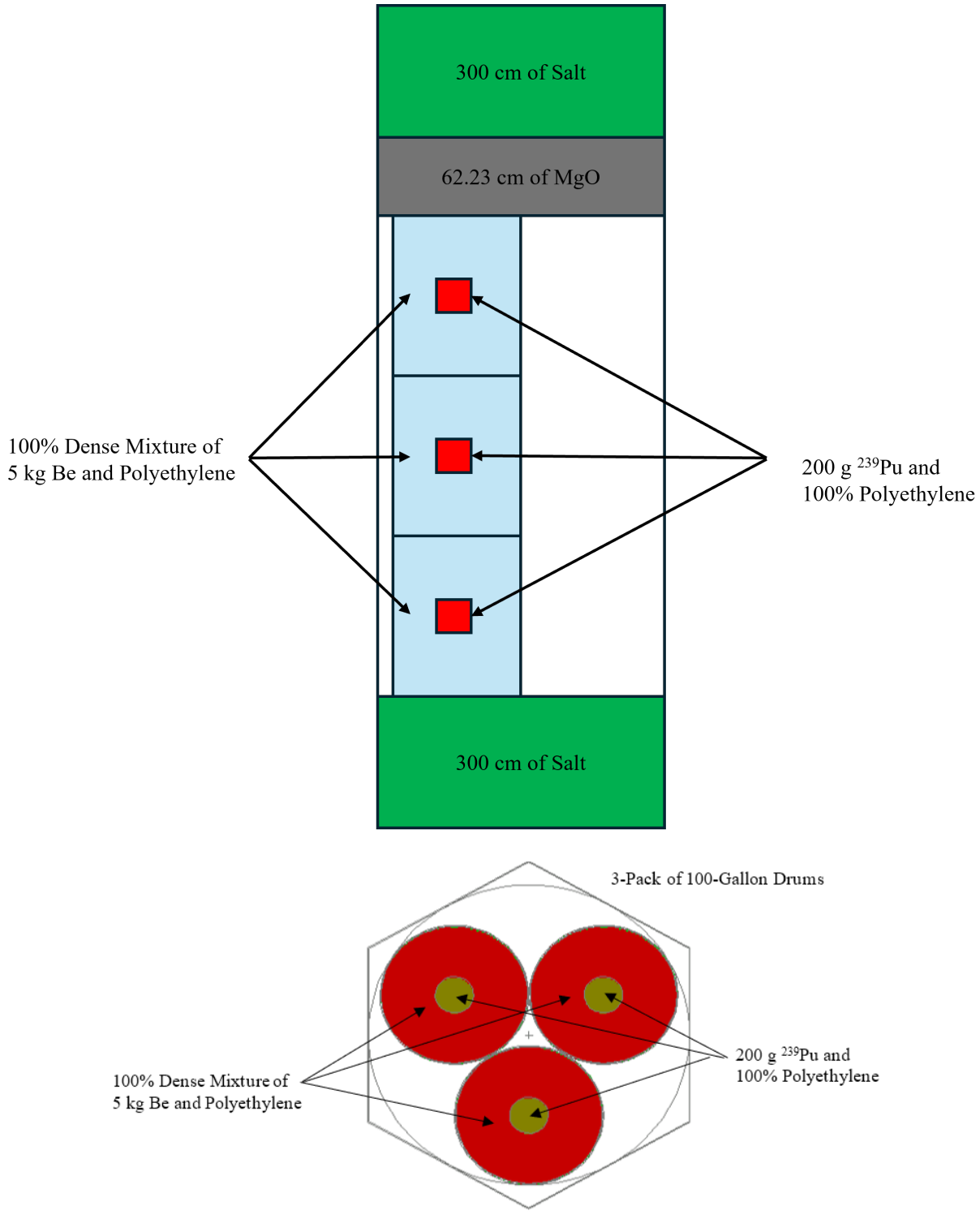

Figure C-1. Infinite Array Model for Storage of 100-gallon Drums of Machine-compacted Waste

C.2.1 Infinite Array of 100-gallon Drums of Machine-compacted Waste

An infinite array model that bounds the storage of both fully and partially compacted 100-gallon drums is constructed where the ^{239}Pu mass is 200 grams/drum and 100% compaction is evaluated. This model includes the maximum mass combined with the maximum compaction based on the limits given in Section C.7. Any vertical design spacing credited in the two-container models in Section C.3 is ignored, and the bottom of the container is placed directly onto the lid of the lower container. This simplifies the modeling while providing a conservative analysis. The three-pack stack of 100-gallon drums is reflected as discussed in Section C.2.

The H/Pu ratio is varied in all of the drums to find the most reactive state. The results of the 100-gallon drum infinite storage array calculations are summarized in Table C-1 and Figure C-2. The $k_{eff} + 2\sigma$ value is low at less than 0.87.

Table C-1. 100-gallon Drum Infinite Storage Array Computational Results

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
700	0.85289	0.00026	0.85341	aray114
800	0.85832	0.00026	0.85884	aray116
900	0.86114	0.00026	0.86166	aray118
1000	0.86049	0.00025	0.86099	aray120
1100	0.85921	0.00024	0.85969	aray122
1200	0.85584	0.00024	0.85632	aray124

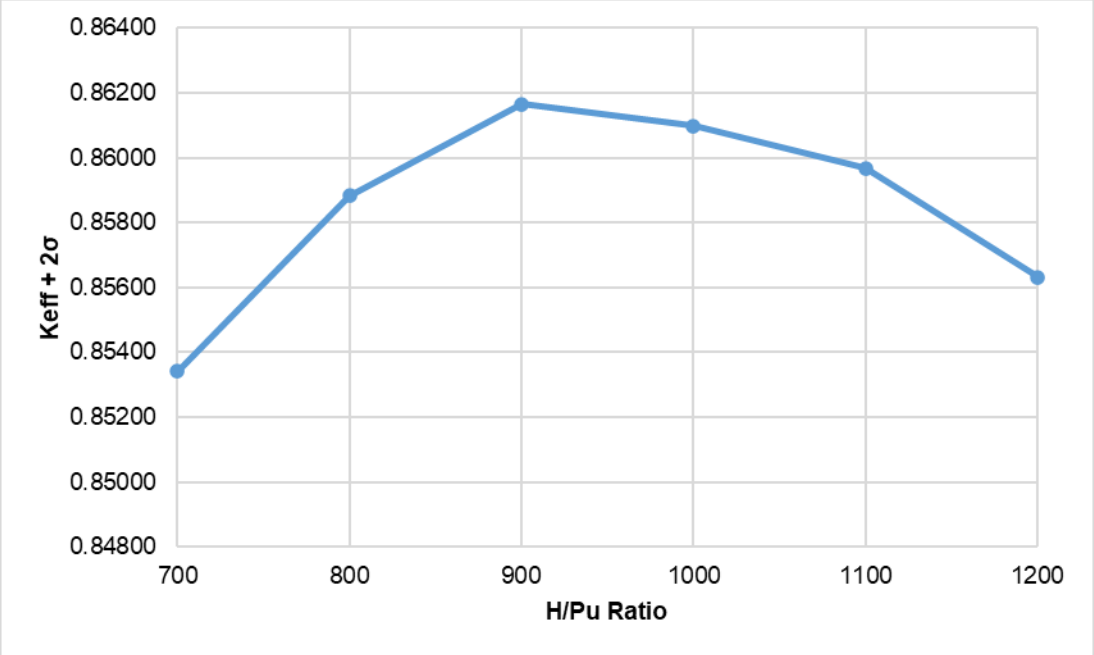

Figure C-2. Compacted Waste in 100-gallon Drum Infinite Storage Array

To verify that the 100% dense polyethylene reflector does not reduce k_{eff} by preventing interaction between waste containers, a calculation was performed where the reflector concentration around each fissile mass was reduced to allow for maximum coupling between the fissile units. Although the waste

pucks in the 100-gallon drums are compacted, the computation considers a range of reflector conditions ranging from 100% dense compaction to 50% compaction. Table C-2 gives the $k_{eff} + 2\sigma$ value at the optimum H/Pu ratio, and Figure C-3 shows the computational results. As indicated by the reduction in reactivity with decreasing polyethylene density, the reflection provided by the polyethylene is more significant than the drum-to-drum interaction.

Table C-2. 100-gallon Drum Infinite Storage Array Reactivity at Optimum H/Pu

Optimum H/Pu Ratio	Reflector Density (%)	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
900	100	0.86114	0.00026	0.86166	aray118
1000	75	0.84492	0.00025	0.84542	arad120
1100	50	0.81974	0.00024	0.82022	arad222

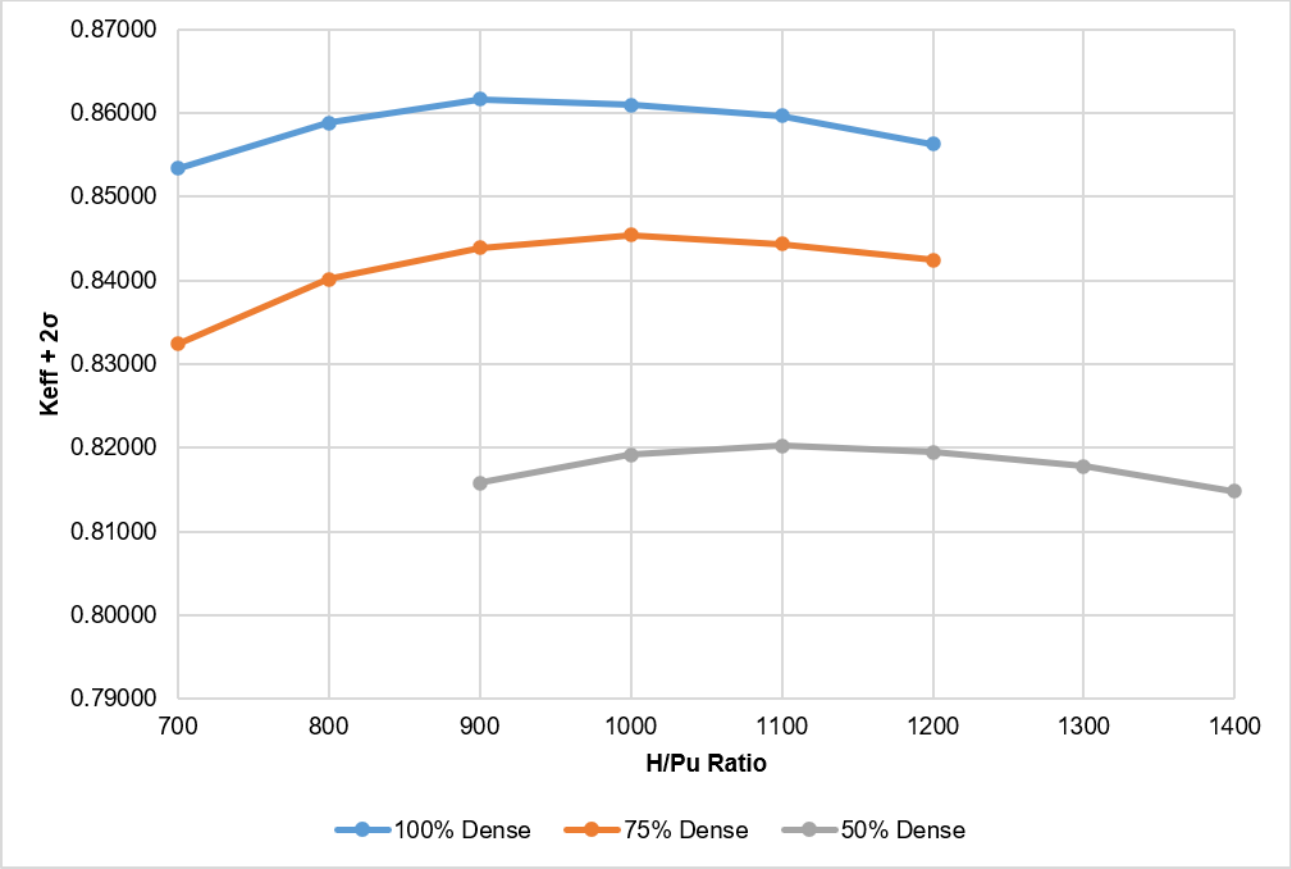

Figure C-3. 100-gallon Drum Storage Array Reactivity vs. Polyethylene Reflector Density

C.2.2 Infinite Array of 55-gallon Drums of Machine-compacted Waste

An infinite array of 55-gallon drums with machine-compacted waste is also modeled. Although machine-compacted waste is typically packaged in 100-gallon drums, these calculations are performed with the same parameters to avoid restricting future operations. Each drum contains up to 200 FGE, the fissile mass mixture is modeled as a cylinder with an H/D ratio of one centrally located in the drum, and the vertical spacing provided by the drum is ignored. The FGE in each seven-pack is further limited to 600

FGE. The center drum and two adjacent outer drums of the seven-pack are modeled at 200 FGE surrounded by 5 kilograms of beryllium in 100% polyethylene. The other four drums contain 5 kilograms of beryllium in 100% dense polyethylene with no fissile material. The reflection provided by the polyethylene/beryllium in the non-fissile drums increases the reactivity of the system compared to the configuration where these drums are empty.

The results of the 55-gallon drum infinite storage array calculations are summarized in Figure C-4 and Table C-3. The maximum $k_{eff} + 2\sigma$ value is 0.86230 at an optimum H/Pu ratio of 900 (filename ara5518). Consequently, the 600-FGE limit per seven-pack of machine-compacted waste results in a subcritical system. These 55-gallon drum calculations combined with the 100-gallon-drum evaluation in Section C.2.1 bound machine-compacted waste in 85-gallon drums that are stored in a four-pack arrangement. Thus, the limits of 200 FGE per drum and 600 FGE per pack apply to 55-, 85-, or 100-gallon drums.

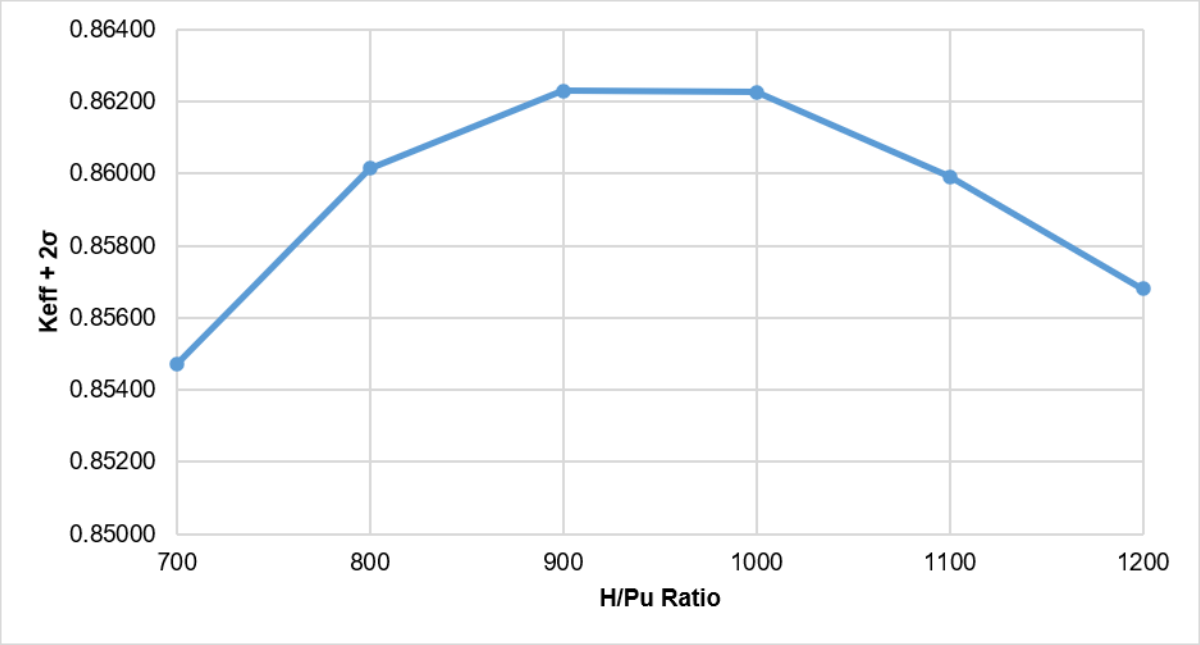

Figure C-4. 55-gallon Drum Infinite Storage Array Reactivity as a Function of H/Pu Ratio

Table C-3. 55-gallon Drum Infinite Storage Array Computational Results

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
700	0.85421	0.00026	0.85473	ara5514
800	0.85962	0.00026	0.86014	ara5516
900	0.86178	0.00026	0.86230	ara5518
1000	0.86177	0.00024	0.86225	ara5520
1100	0.85941	0.00025	0.85991	ara5522
1200	0.85632	0.00024	0.85680	ara5524

C.2.3 Infinite Array of SWBs of Machine-Compacted Waste

An infinite array simulating the worst-case configuration of SWB containers with machine-compacted waste was modeled with a ^{239}Pu mass of 200 grams per SWB. The compacted reflector dunnage was modeled as a mixture of 18.14 kilograms of beryllium and polyethylene at 100% density. The SWBs are modeled in the hexagonal lattice and stacked three tiers high with no vertical spacing between them. The stack is mirrored on all lateral sides to simulate an infinite array and reflected top and bottom by MgO and salt as discussed in Section C.2.

The results of the SWB infinite storage array calculation are summarized in Figure C-5 and Table C-4 with the maximum $k_{eff} + 2\sigma$ of 0.86162 at an optimum H/Pu ratio of 1000 (filename ar1000_200).

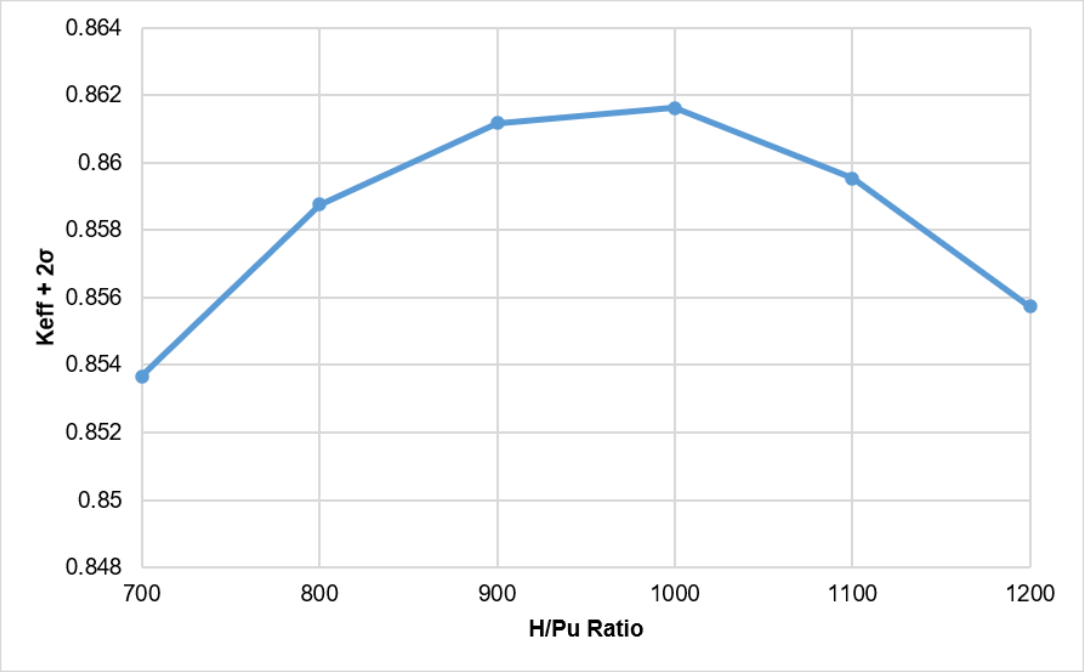

Figure C-5. SWB 200 FGE Infinite Storage Array Reactivity as a Function of H/Pu Ratio

Table C-4. SWB 200 FGE Infinite Storage Array Computational Results

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
700	0.85314	0.00026	0.85366	ar700_200
800	0.85823	0.00026	0.85875	ar800_200
900	0.86066	0.00025	0.86116	ar900_200
1000	0.86114	0.00024	0.86162	ar1000_200
1100	0.85905	0.00024	0.85953	ar1100_200
1200	0.85526	0.00024	0.85574	ar1200_200

C.3 MCNP Two-container Models for Machine-compacted Waste in Drums

The two-container models used in this evaluation consider the different container types and fissile loadings that could be stacked with a drum or SWB containing machine-compacted CH waste in a

bounding configuration. The primary intent of the two-container analyses is to establish an FGE mass limit on machine-compacted waste that is conservative enough to ensure that a criticality at the WIPP due to the handling and disposal/storage of machine-compacted waste is not credible.

The two containers modeled are surrounded with a 300-centimeter reflector of concrete, MgO, or salt using the material compositions discussed in Section 5.2.4. These reflectors would be present in above-ground handling and storage and repository disposal.

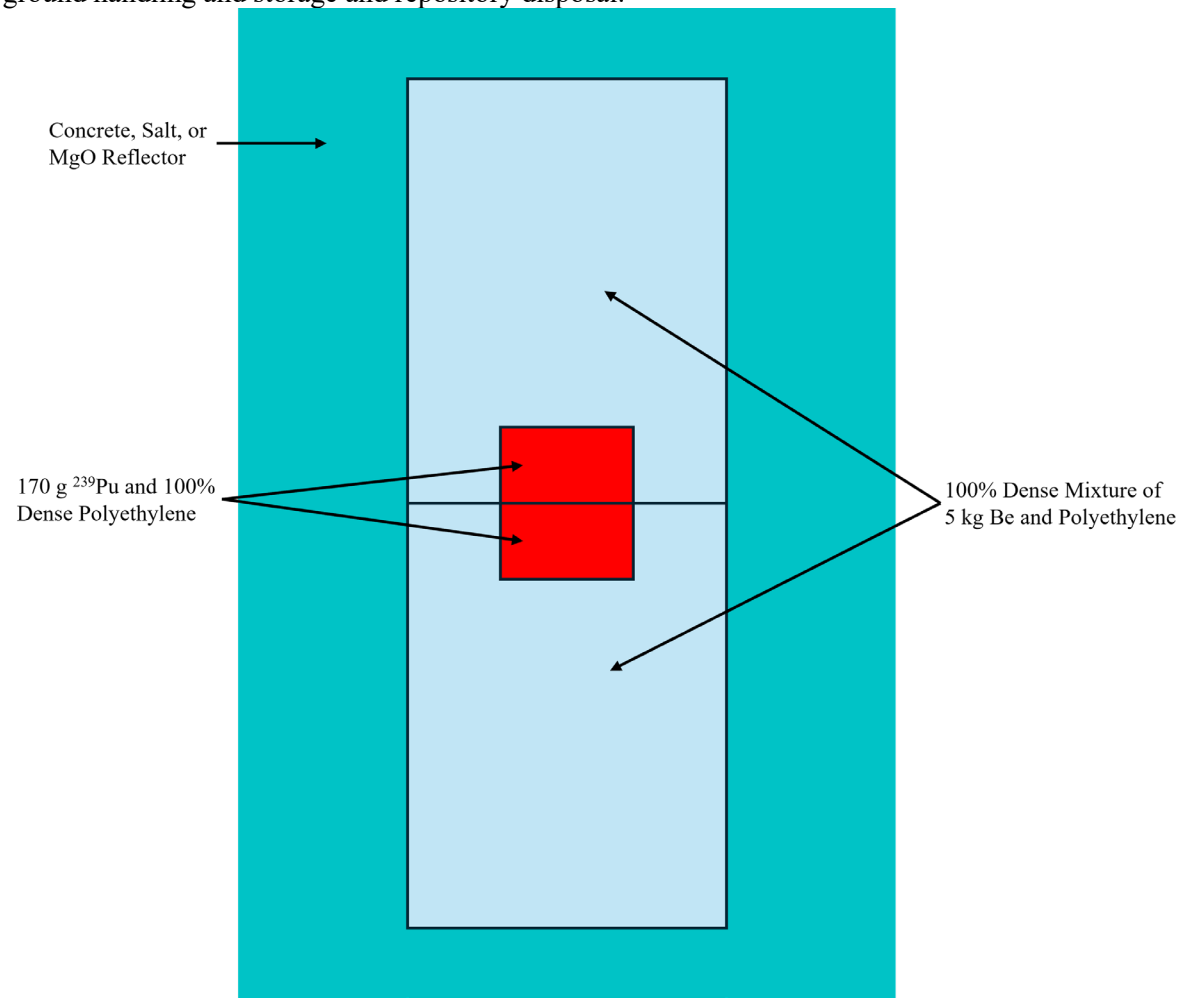

Figure C-6 summarizes the geometric characteristics of a 100-gallon two-drum model of fully compacted waste as an example.

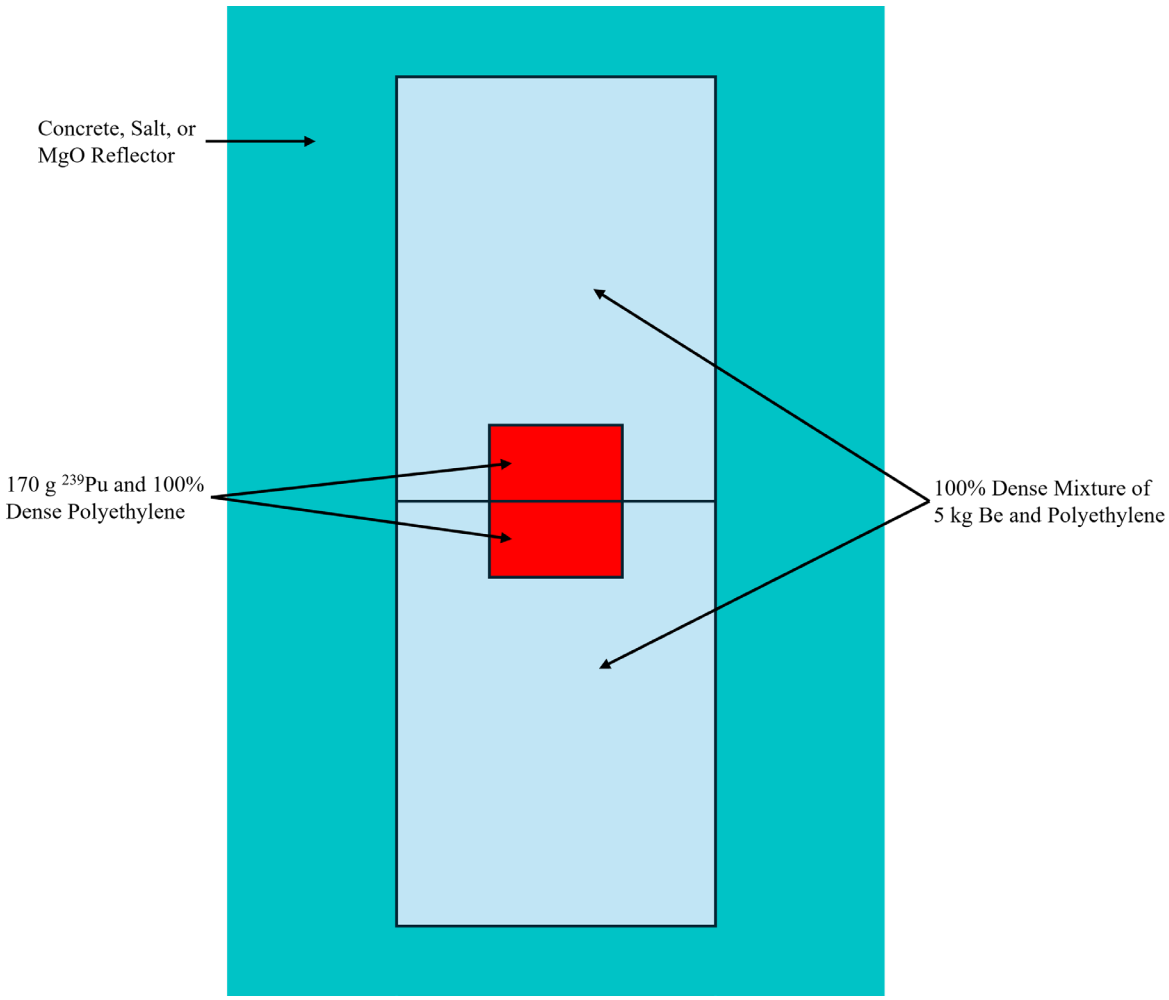

Figure C-6. Two-Drum Model for 100-gallon Drums Containing Fully Compacted Waste without Vertical Spacing Between Drums

C.3.1 100-gallon Drum Two-Container Models with Fully Compacted Waste

The first two-drum model involves two 100-gallon drums containing fully compacted waste. The intent of this calculation is to establish the FGE limit on 100% dense machine-compacted waste for 1) two-drum configurations where no credit is taken for vertical spacing between drums, and 2) the spacing between drums inherent in the container design is credited.

In the first two-drum model, the two drums are vertically stacked on top of each other with the fissile masses being separated only by the thickness of the container lid and bottom. In the more realistic model, a 0.5-inch space is modeled between the contents and the exterior bottom of the 100-gallon drum and an additional 0.5-inch separation is modeled between the contents and the drum exterior at the top of the drum to account for the recessed inner lid/lid ring closure mechanism. Drawing BNFL 53-9840 (BNFL 2001) for the 100-gallon drum shows that the space at the bottom of the drum is approximately 0.875 inches thick and the space at the top of the drum from the recessed inner lid is a minimum of 0.873 inches (ignoring the outer lid and ring clamp separation). Thus, the overall distance from the lid top surface to the bottom surface between two vertically adjacent drums is nominally 1.75 inches. The use of

0.5 inches at both the top and bottom is adequate to accommodate variations from the nominal container dimensions and is conservative compared to the actual design. Because there is an outer lid on top of the inner lid in a 100-gallon drum, even if a smaller 55-gallon drum is stacked on top of the 100-gallon drum, the upper spacing will be maintained. Furthermore, the slipsheets or reinforcing plates are not credited in this analysis.

The two-drum models described above were used to determine the FGE mass limit for the 100-gallon drum containing fully compacted waste. With respect to the bounding two-drum model without vertical spacing, a ^{239}Pu mass of 170 FGE is below the USL of 0.9659 as shown in Table C-5 and Figure C-7. The ^{239}Pu/polyethylene waste mixture in both drums was varied over a full range of H/Pu ratios to ascertain the most reactive state. Table C-5 tabulates the maximum k_{eff} and results for the optimum H/Pu ratio.

Table C-5. 100-gallon Drum Two-Container Model Reactivity at 170 FGE in Fully Compacted Waste with No Design Separation Credited

Reflector	Optimum H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
Concrete	800	0.95615	0.00025	0.95665	ml17016
Salt	800	0.95644	0.00026	0.95696	ms17016
MgO	800	0.95618	0.00025	0.95668	mm17016

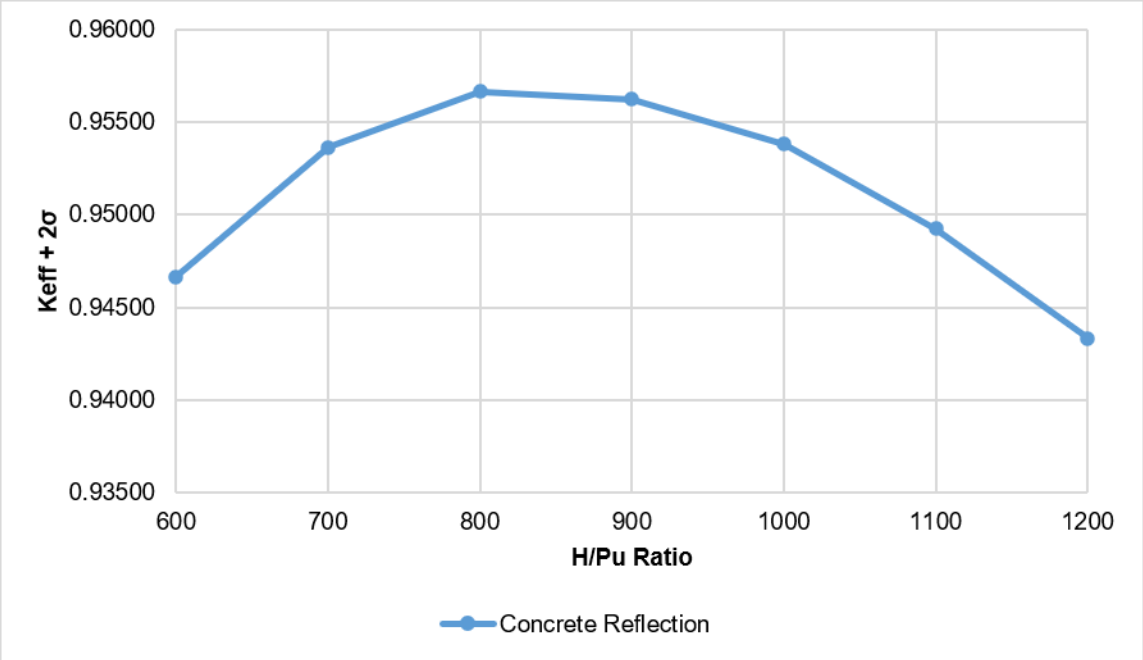

Figure C-7. Two-Container Results for 100% Machine-Compacted Waste in 100-gallon Drums at 170 FGE/drum

In the more realistic or representative two-drum model, the FGE was set at the maximum TRUPACT-II limit allowed (200 grams of ^{239}Pu) in any given 100-gallon drum. The computational results for this model shown in Table C-6 and Figure C-8 credit 0.5 inch of design spacing in each drum for a 1-inch separation between fissile units. These results indicate that the 200 FGE limit yields a two-drum system eigenvalue below 0.93.

Table C-6. System Reactivity for Two 100-gallon Drums with Design Spacing Containing 200 FGE in Fully Compacted Waste

Reflector	Optimum H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
Concrete	900	0.92780	0.00025	0.92830	tdmc258
Salt	900	0.92809	0.00025	0.92859	tdmc858
MgO	900	0.92754	0.00025	0.92804	tdc1458

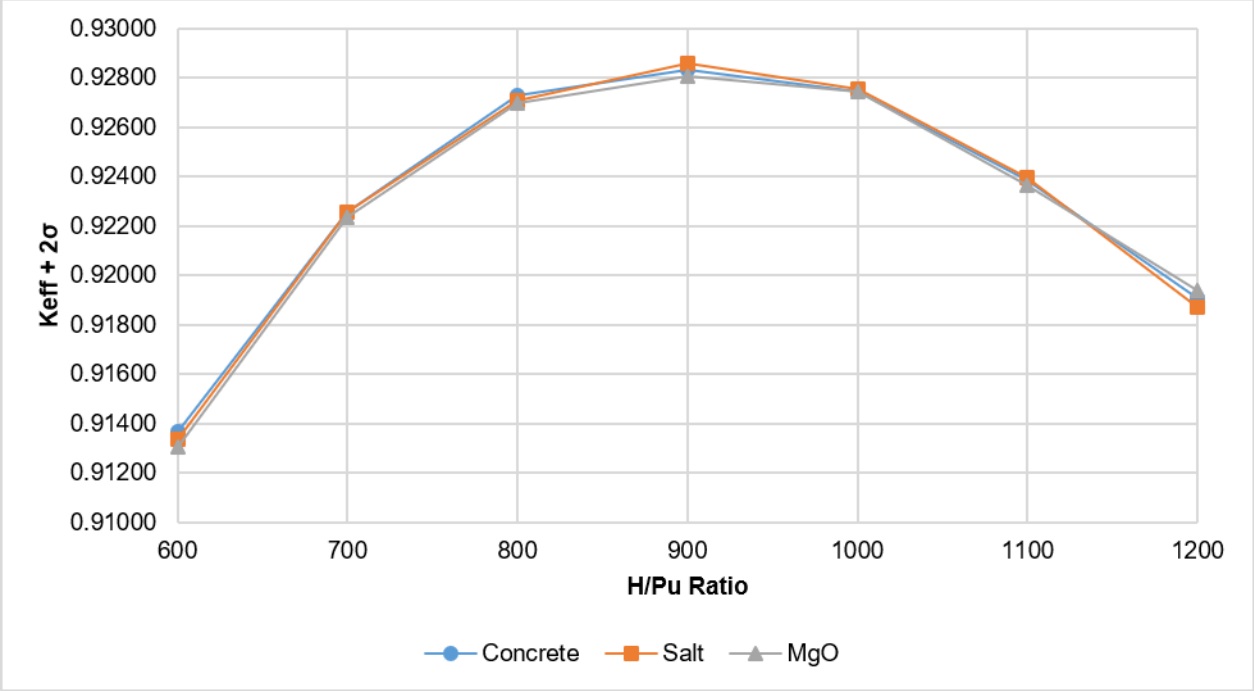

Figure C-8. Two 100-gallon Drums containing 200 g ^{239}Pu in Fully Compacted Waste with 0.5-inch Design Spacing per Drum

C.3.2 100-gallon Drum Two-Container Models with Partially Compacted Waste

The model for the partially compacted waste evaluates the fissile mass in the partially compacted drum contains 200 grams of ^{239}Pu moderated with a polyethylene-water mixture, which is 70% by volume polyethylene and 30% by volume water. The fissile mass is reflected by a mixture of 5 kilograms of beryllium homogenously mixed with 70% dense polyethylene. Geometrically, no credit is taken for design vertical spacing between axially adjacent drums in the partially compacted models, and the only separation is the steel of the drum lid and bottom.

The partially compacted waste drum model is used to evaluate three separate two-drum combinations as follows:

1. Two partially compacted drums each containing 200 grams of ^{239}Pu.

2. A fully compacted/partially compacted combination where no design vertical spacing is credited (170 grams of ^{239}Pu is modeled in the fully compacted drum);

3. A fully compacted/partially compacted combination where the fully compacted drum provides a 0.5-inch vertical separation between drums (200 grams of ^{239}Pu is modeled in the fully compacted drum); and

First two 100-gallon drums containing partially compacted waste are vertically stacked on top of each other with the fissile masses being separated only by the thickness of the container lid and bottom (i.e., no credit is taken for design spacing). The ^{239}Pu/70% polyethylene/30% water waste mixture in both drums was varied over a full range of H/Pu ratios to ascertain the most reactive state. The results show that the optimum H/Pu ratio is 900. Table C-7 tabulates the maximum k_{eff} and Figure C-9 shows the results with respect to H/Pu ratio with concrete reflection.

For the fully compacted/partially compacted drum combinations, the waste mixture concentration in the upper drum (partially compacted waste) was then fixed at the optimum H/Pu ratio of 900, and the bottom drum (fully compacted waste) was fixed at the respective optimum H/Pu ratio as determined in Section C.3.1, thereby encompassing the most reactive system state. Table C-8 summarize the computational results for the different two-drum combinations. The results indicate that the 200-FGE mass limit on partially compacted drums provides a sufficient margin to ensure that the reactivity of the two 100-gallon drum system remains below the USL of 0.9659, even when considering a partially compacted drum in combination with a fully compacted drum.

Table C-7. 100-gallon Drum Two-Container Model Reactivity at 200 FGE in Partially Compacted Waste with No Design Spacing Credited

Reflector	Optimum H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
Concrete	900	0.95621	0.00026	0.95673	PCPARA900
Salt	900	0.95569	0.00025	0.95619	PSPARA900
MgO	900	0.95605	0.00025	0.95655	PMPARA900

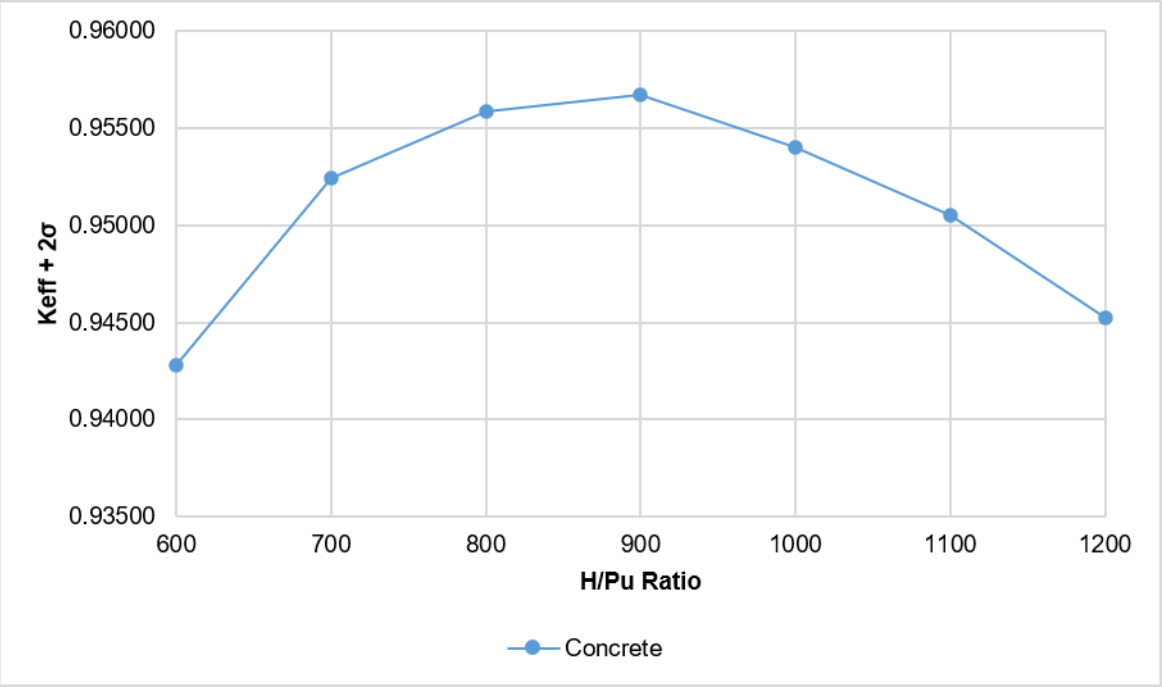

Figure C-9. Partial Compaction/Partial Compaction 100-gallon Drum Combination

Table C-8. 100-gallon Drum Combinations Involving Partially Compacted Drums

Optimum H/Pu Ratio		Reflector	k_{eff}	σ	k_{eff} + 2σ	Filename
Bottom Drum	Top Drum					
Fully Compacted/Partially Compacted 2-Drum Combination without Design Spacing						
800	900	Concrete	0.95619	0.00026	0.95671	tdmc617
800	900	Salt	0.95549	0.00026	0.95601	tdc1217
800	900	MgO	0.95608	0.00025	0.95658	tdc1817
Fully Compacted/Partially Compacted 2-Drum Combination with Design Spacing						
900	900	Concrete	0.89291	0.00025	0.89341	tdmc658
900	900	Salt	0.89216	0.00026	0.89268	tdc1258
900	900	MgO	0.89204	0.00025	0.89254	tdc1858

C.3.3 Two 55-gallon Drum Combinations of Compacted Waste

Although the fully compacted waste is expected to be shipped in 100-gallon drums, the limits for 55-gallon drums are also determined in this evaluation. The 55-gallon drum has a thinner wall than the 100-gallon drum. The 55-gallon drums are analyzed with the corresponding limits for machine-compacted waste in 100-gallon drums with and without design spacing and at 70% compaction. The vertical design spacing modeled in 55-gallon drums is 1.5 centimeters. This separation distance is conservative as the actual expected separation is 4.445 centimeters (found by subtracting the inner drum height from the outer drum height). Because of the possibility of bowing in the drum and possible slippage/misalignment when

stacking drum assemblies, only a fraction of the separation is credited. In reality, slipsheets are used between drum assemblies for ease of handling and also provide separation. The separation provided by slipsheets was not credited in the analysis. The value of 1.5 centimeters is approximately one third of the nominal separation. Other than the size of the drum and the use of the 1.5-centimeter versus 1-inch design separation, the 55-gallon drum models are identical to the 100-gallon drum two-container models.

The results of the two-drum computations are given in Table C-9 and shown in Figure C-10 (fully compacted waste with design separation), Figure C-11 (fully compacted waste without design separation), and Figure C-12 (partially compacted waste without design separation). All cases remain below the USL with 50% dense steel modeled in the drum wall, lid and bottom.

Further container combinations with a compacted 55-gallon drum are not necessary as the machine-compacted 100-gallon drum is modeled with each of the other approved container loadings at the WIPP, as is the machine-compacted SWB. The 100-gallon drum combinations illustrate that machine-compacted waste does not increase reactivity when combined with other waste types.

Table C-9. System Reactivity for 55-gallon Drum Two-Container Models with Compacted Waste

Optimum H/Pu Ratio	Reflector	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
200 g ^{239}Pu in Fully Compacted Waste with Vertical Design Spacing					
900	Concrete	0.95428	0.00024	0.95476	t55c118
900	Salt	0.95394	0.00025	0.95444	t55c218
800	MgO	0.95408	0.00027	0.95462	t55c317
170 g ^{239}Pu in Fully Compacted Waste without Vertical Design Spacing					
800	Concrete	0.96028	0.00026	0.96080	t55c157
800	Salt	0.96093	0.00026	0.96145	t55c257
800	MgO	0.96038	0.00025	0.96088	t55c357
200 g ^{239}Pu in Partially Compacted Waste without Vertical Design Spacing					
900	Concrete	0.96120	0.00024	0.96168	t55w318
900	Salt	0.96058	0.00026	0.96110	t55w618
900	MgO	0.96108	0.00026	0.96160	t55w918

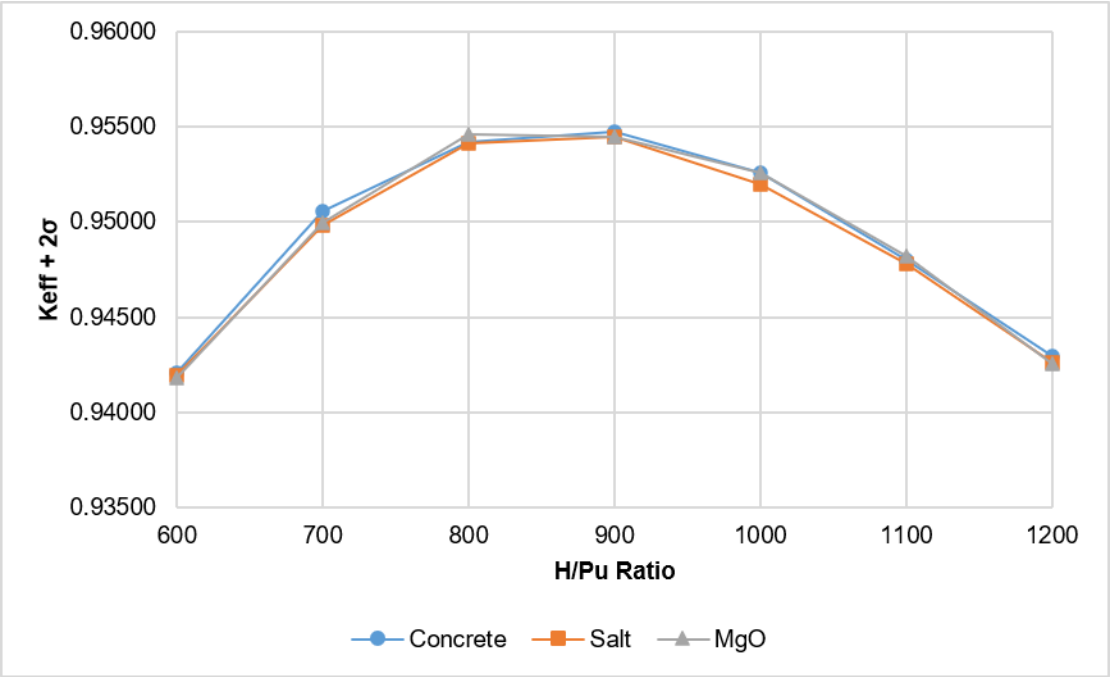

Figure C-10. Fully Compacted 55-gallon Drum Combination with Vertical Design Spacing at 50% Steel Density

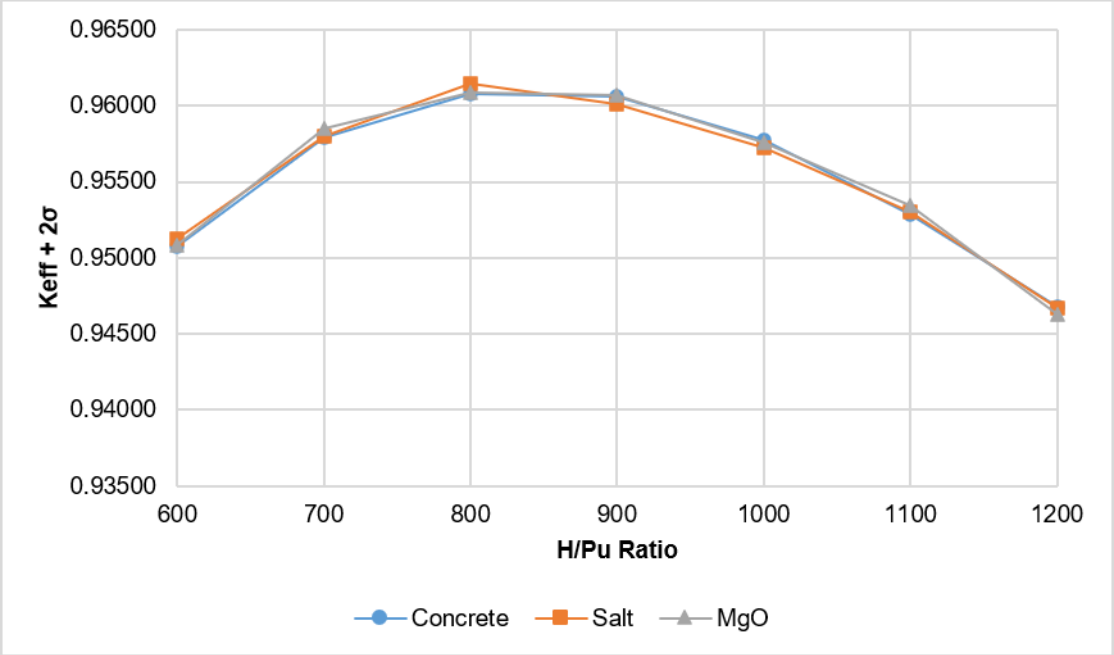

Figure C-11. Fully Compacted 55-gallon Drum Combination without Vertical Design Spacing at 50% Steel Density

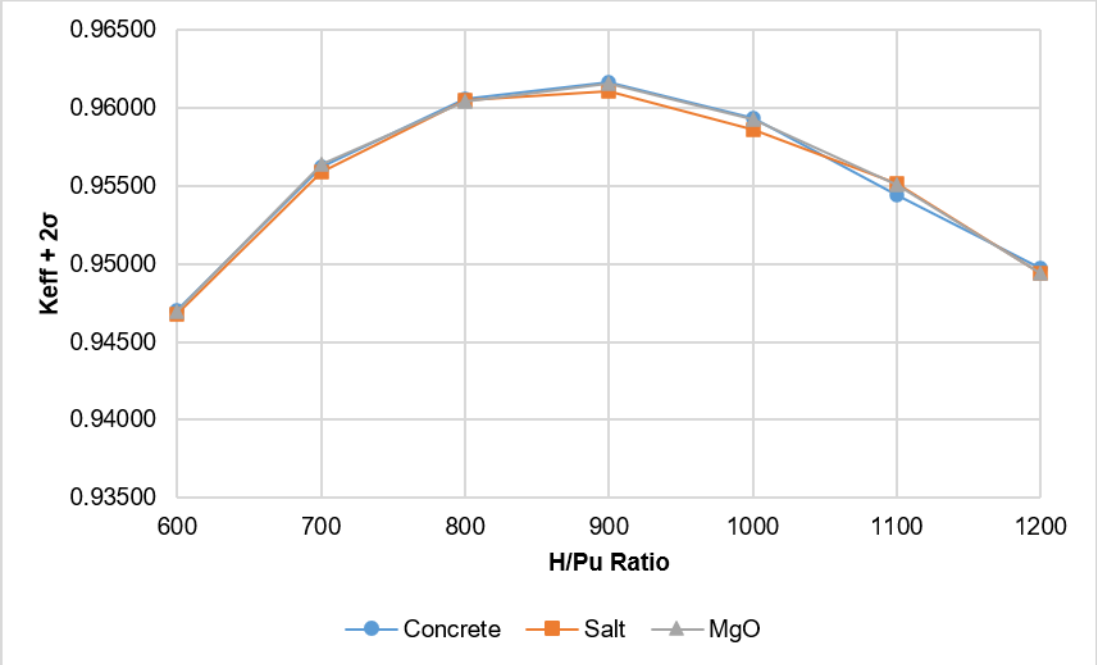

Figure C-12. Partially Compacted 55-gallon Drum Combination without Vertical Design Spacing at 50% Steel Density

C.4 Standard Waste Box 2-container Combinations

C.4.1 Two-Container SWBs Direct-Loaded with Fully Compacted Waste

The next sequence of calculations evaluates two stacked SWB containers containing fully compacted machine-compacted CH waste each containing 200 FGE. With no separation between the fissile masses, the USL is exceeded but only a small separation distance is needed to reduce the result below the USL of 0.9659. The H/Pu ratio is varied at each separation distance modeled and plotted in Figure C-13, with the highest $k_{eff} + 2\sigma$ values tabulated in Table C-10. For all separation distances, the optimum H/Pu ratio is 800. The fissile mass must be slightly less than 1 centimeter below the lid to meet the USL of 0.9659. This separation will be easily achieved in reality as the compacted puck drums would be randomly loaded into the SWB during the direct loading process and filling the SWB exactly to the top is not likely (see Assumption 4 in Section 9.3). Also, the probability of all fissile material being in only one puck drum within the large SWB is highly unlikely. The multiple, randomly loaded puck drums would not produce the 100% dense polyethylene reflector modeled around the fissile mass, but would allow multiple streaming paths for neutrons to escape and reduce the reactivity compared to the modeled result.

A parametric study is performed on the reflector material around the 2-drum model. The concrete reflector is replaced with either MgO, NaCl, or void. In all cases the results are identical and the k_{eff} is independent of reflector material. This indicates that the polyethylene filling the SWB is effectively infinitely thick and isolates the FGE mass from any external reflector. These results are shown in Table C-11.

The 200-FGE limit for SWBs direct loaded with machine-compacted waste is higher than the 170-FGE limit imposed on drums without design spacing. This is due to the increased wall thickness of an SWB

(0.3175 centimeters) compared to a 100-gallon (0.15189 centimeters) or a 55-gallon (0.12141 centimeters) drum.

Table C-10. Separation Parameter Study for Direct-Loaded Two-SWB 200 FGE Combinations of Fully Compacted Waste

Distance between Fissile Masses (cm)	Optimum H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
200 g ^{239}Pu/SWB with Concrete Reflector					
0	800	0.97398	0.00026	0.97450	fsw200_00_800
0.5	800	0.96937	0.00026	0.96989	fsw200_05_800
1.0	800	0.96227	0.00026	0.96279	fsw200_10_800
1.5	800	0.95493	0.00026	0.95545	fsw200_15_800
2.0	800	0.94629	0.00024	0.94677	fsw200_20_800

Table C-11. Reflector Parameter Study for Direct-Loaded Two-SWB 200 FGE of Fully Compacted Waste

Reflector	H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
200 g ^{239}Pu/SWB					
Concrete	800	0.96227	0.00026	0.96279	fsw200_10_800
Void	800	0.96227	0.00026	0.96279	fsw200_10_800v
MgO	800	0.96227	0.00026	0.96279	fsw200_10_800m
NaCl	800	0.96227	0.00026	0.96279	fsw200_10_800s

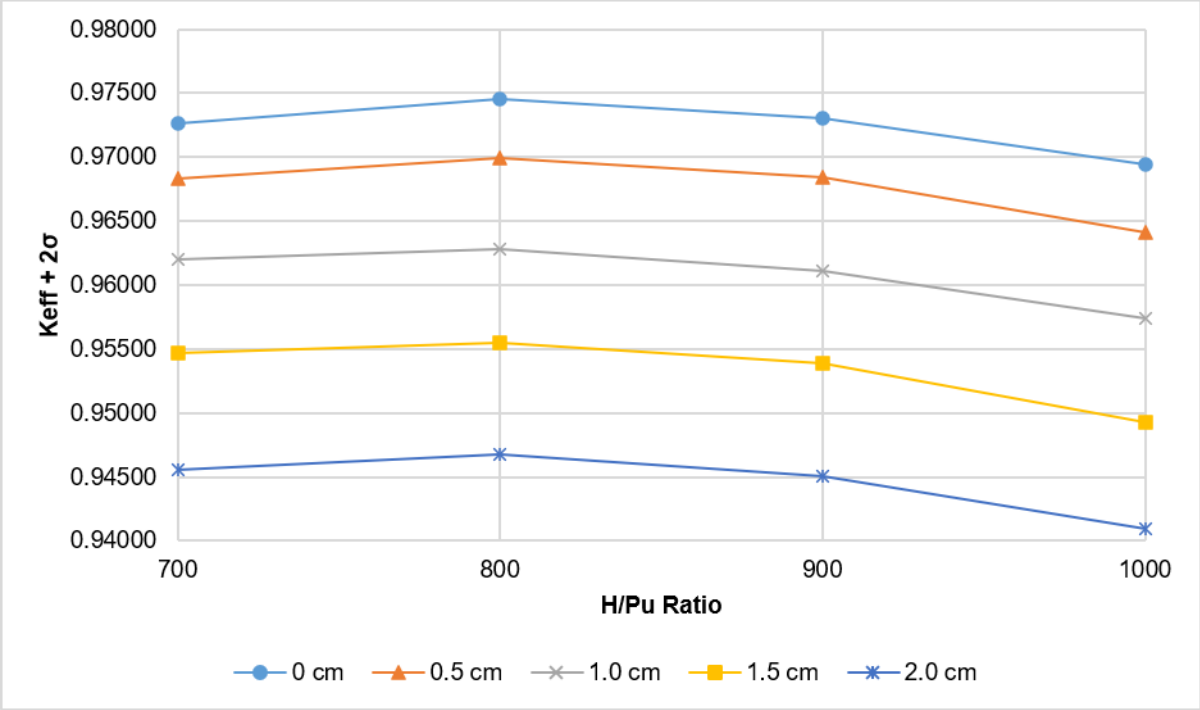

Figure C-13. Two-Container SWB Model with Fully Compacted Waste filling SWB at 200 FGE/SWB and Concrete Reflection

C.5 Bounding Array Model Including Two-container Configuration

The fissile mass configuration used in the two-configuration model with the tight reflection boundaries modeled is expected to bound any array configuration where a two-container unit is surrounded by other containers in the underground repository. Since a two-container configuration is highly unlikely, then an embedded two-container unit in an infinite storage array (which is mirrored on all lateral sides), will bound any probable geometric arrangement that could be encountered in the repository. Furthermore, this configuration will verify that the FGE mass limit placed on machine-compacted waste is conservative enough to ensure that a criticality accident at the WIPP is not a credible event.

A representative two-container combination of 100-gallon drums containing either fully or partially compacted waste is used in the bounding array model. The bounding array consists of a three-pack stack arranged in a hexagonal lattice. Each three-pack consists of three 100-gallon drums placed inside a cylindrical footprint with the centers of the drums being separated by 120 degrees. The three-packs are stacked three tiers high and the stack is mirrored on all lateral sides to simulate an infinite array. The top and bottom of the stack is reflected as in the array models discussed in Section C.2.

The two-drum arrangement is formed from one drum in the bottom tier and one drum in the middle tier that are vertically adjacent to one another. Both drums contained either fully compacted or partially compacted waste. All other drums contained fully compacted waste with the fissile material centrally located within the drum volume, consistent with the array model described in Section C.2.1. Note that since the three-pack of drums is infinitely reflected in x and y, there are two adjacent instances of the two-drum arrangement. Figure C-14 illustrates the model used in the bounding array calculation.

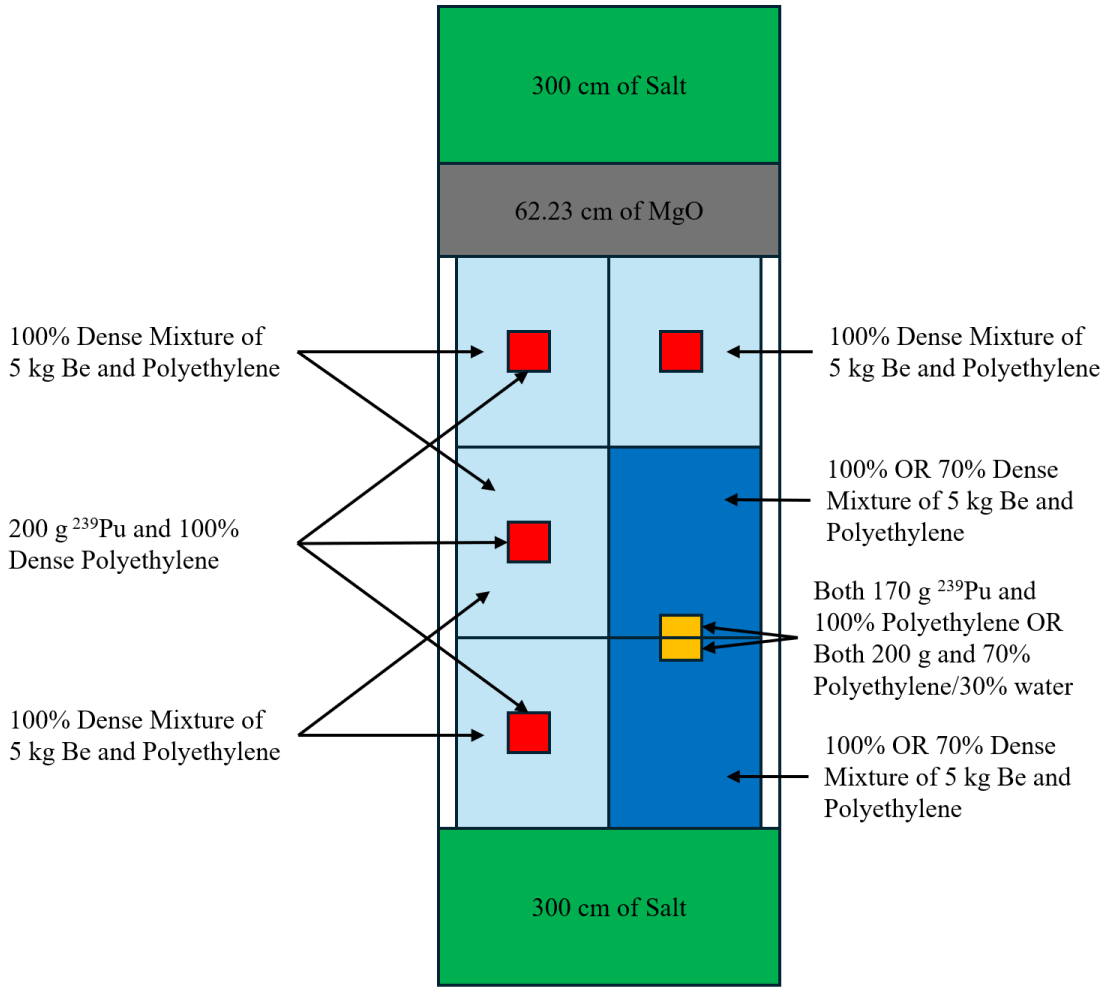

Figure C-14. Bounding Array Model for 100-gallon Drums containing Fully or Partially Compacted Waste

To ensure that the most reactive configurations were analyzed, the waste mixture concentration in all drums was fixed at the appropriate optimal H/Pu ratio. As previously determined, the optimal H/Pu ratios were 900 in the fully compacted infinite array model, 800 in the fully compacted two-container model, and 900 in the partially compacted two-container model. Table C-12 summarizes the computational results for the various drum arrangements. The system reactivity is statistically equivalent to the tightly reflected two-drum model results given in Table C-5, Table C-7, and Table C-8. Thus, the two-drum model is shown to bound the worst-case fissile material locations that could occur in the underground repository.

Table C-12. Bounding Arrays containing Fully and Partially Compacted Waste

Optimum H/Pu Ratio		Reflector	$k_{eff} + 2\sigma$	Filename
Two-Container Model Drums	Array Model Drums			
Array with 100-gallon Drums containing Fully Compacted Waste				
800	900	MgO/Salt	0.95714	arab117
Array with 100-gallon Drums containing Fully and Partially Compacted Waste				
900	900	MgO/Salt	0.95676	arab218

C.6 MCNP5 Machine-compacted Waste Contingency Models

To ensure that the computational analysis of compacted waste packages is bounding for all credible conditions, a few contingency conditions were evaluated for the underground storage array of various waste packages containing compacted, fissile-bearing waste. In this regard, only array configurations with centrally located fissile material were considered since the two-container models are sufficiently conservative to bound any contingency of more realistic or expected conditions related to the interaction between small numbers of containers.

The contingency events evaluated in this section include:

1. An overstacking event where 100-gallon drums in a three-pack configuration containing fully compacted waste were stacked four tiers high;

2. An FGE overbatching event where one 55-gallon drum containing fissile-bearing compacted waste in the middle tier of seven-packs contained 300 FGE;

3. An FGE overbatching event where the one 100-gallon fissile-bearing drum in the three-pack contained 300 FGE;

4. An FGE overbatching event where one SWB in the three-stack in the array contained 300 FGE;

5. A beryllium overbatching event where one of the fissile-bearing 100-gallon drums in a three-pack contained 10 kilograms of beryllium; and

6. A sprinkler activation event in the WHB resulting in interstitial moderation between the waste containers containing compacted waste.

C.6.1 100-gallon Drum Array Overstack Model

The WIPP disposal room heights in the underground repository are designed to accommodate three tiers of waste containers. In some areas, ground control activities have resulted in areas of the disposal rooms being mined to a height greater than 13 feet such that it is possible to stack greater than three tiers high including the MgO supersack. The computational results for a four-tier stack of three-packs of 100-gallon drums containing compacted waste yields a system eigenvalue well below the USL of 0.9659 as summarized in Table C-13. In fact, the four-tier array reactivity is not much greater than the three-tier reactivity because the polyethylene filling the drum isolates the fissile mass in adjacent tiers. An

overstack of machine-compacted 55-gallon drums or SWBs will follow the same trend and also remain subcritical.

Table C-13. Results for an Array of 100-Gallon Drums Stacked Four Tiers High

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
700	0.85296	0.00028	0.85352	aray414
800	0.85894	0.00027	0.85948	aray416
900	0.86117	0.00026	0.86169	aray418
1000	0.86124	0.00025	0.86174	aray420
1100	0.85930	0.00024	0.85978	aray422
1200	0.85596	0.00024	0.85644	aray424

C.6.2 55-gallon Drum Array Overbatch Model

Since rigorous non-destructive quality assurance techniques are employed at the waste generator site to verify compliance to mass loading limits and these limits are confirmed via paperwork checks by the WIPP facility before shipment and on receipt of the waste material, an overbatch event is highly unlikely. However, in compliance with standard nuclear criticality practices and to ensure a potential criticality event is not credible, a series of overbatching contingency scenarios for waste packages containing compacted waste were analyzed. Specifically, with respect to a 55-gallon drum containing compacted waste, a scenario was evaluated where one container in a three-tier stack is overbatched by 50% of its nominal value. From a modeling perspective, one container in the bottom or middle tier is overbatched and the stack is infinitely reflected on the lateral surfaces as in the base array model. This is highly conservative as it results in one of every twenty-one 55-gallon drums being overbatched. The results of these cases, as summarized in Table C-14, are below the USL of 0.9659.

Table C-14. Results for an Overbatching Event where One 55-Gallon Drum in the Middle Tier Contained 300 FGE

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
700	0.94557	0.00027	0.94611	ara5554
800	0.94927	0.00027	0.94981	ara5556
900	0.94942	0.00027	0.94996	ara5558
1000	0.94702	0.00025	0.94752	ara5560
1100	0.94342	0.00025	0.94392	ara5562
1200	0.93824	0.00023	0.93870	ara5564

C.6.3 100-gallon Drum Array Overbatch Model

A model similar to that discussed in Section C.6.2 was created for 100-gallon drums containing compacted waste. One drum in a three-tier stack of three-packs was overbatched by 50% to 300 grams of ^{239}Pu while the other two drums contained 200 FGE. As shown in Table C-15, the results remain below the USL of 0.9659.

Table C-15. Results for an FGE Overbatching Event where One 100-Gallon Drum in the Bottom Tier Contained 300 FGE

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
700	0.94417	0.00027	0.94471	aray214
800	0.94873	0.00025	0.94923	aray216
900	0.94888	0.00026	0.94940	aray218
1000	0.94707	0.00025	0.94757	aray220
1100	0.94261	0.00024	0.94309	aray222
1200	0.93744	0.00024	0.93792	aray224

C.6.4 Standard Waste Box Array Overbatch Model

The final FGE overbatching scenario evaluated as part of this contingency evaluated overbatching the middle tier in the SWB array by 50% of the nominal value of 200 FGE, or 300 FGE. The results of the SWB overbatching contingency are shown in Table C-16 with the maximum k_{eff} less than the USL of 0.9659. The computational results indicate that the double contingency requirement for the ^{239}Pu mass content in the SWB is met as multiple overbatching events will not result in the USL being exceeded.

Table C-16. Array Results with Middle SWB in a Three-pack Stack Containing 300 FGE

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
700	0.93842	0.00027	0.93896	aro700_300
800	0.94455	0.00026	0.94507	aro800_300
900	0.94108	0.00026	0.94160	aro900_300
1000	0.93887	0.00025	0.93937	aro1000_300
1100	0.93464	0.00025	0.93514	aro1100_300

C.6.5 100-gallon Drum Array Excess Beryllium Model

The beryllium overbatching contingency is similar to the fissile mass overbatching event in that one drum in every three three-packs exceeds its mass limit. However, this case evaluated a double-batch event where the beryllium mass content in the overloaded drum is 10 kilograms. The beryllium overbatch model has the fissile contents of two of the three three-packs in the stack at their optimum H/Pu state while the composition in the 100-gallon drums in the remaining three-pack, including the excess beryllium drum, was varied over a range of H/Pu ratios. The results of the overbatching contingency are tabulated in Table C-17. As expected, the system eigenvalue is well below the USL.

Table C-17. Results for a Beryllium Overbatching Event with One 100-Gallon Drum Three-pack Stack Containing 10 kg of Beryllium

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
700	0.85417	0.00026	0.85469	aray314
800	0.86004	0.00026	0.86056	aray316
900	0.86180	0.00025	0.86230	aray318
1000	0.86164	0.00024	0.86212	aray320
1100	0.85978	0.00023	0.86024	aray322
1200	0.85632	0.00024	0.85680	aray324

C.6.6 Array Model with Sprinkler Activation

The final contingency considered in this analysis addresses the potential activation of the sprinkler system in the WHB resulting in interspersed moderation between the waste containers. The model employed to simulate this event includes a bounding three-tier stack of seven-packs of 55-gallon drums containing compacted waste where the ceiling and floor are modeled as 2-foot (60.96-centimeter) thick concrete while the sides are mirrored for infinite reflection as shown in Figure C-15. The cases were evaluated at the mass limits and at the optimum H/Pu ratio where water from a sprinkler activation was allowed to fill the spaces between the drums. The water density is varied from 0.05 to 1 g/cm^3, and the results are shown in Table C-18. The computational results show no trend in k_{eff} which suggests that the fissile masses are isolated from one another by the compacted polyethylene in the drums. Sprinkler activation or flooding of the array will not result in a critical configuration.

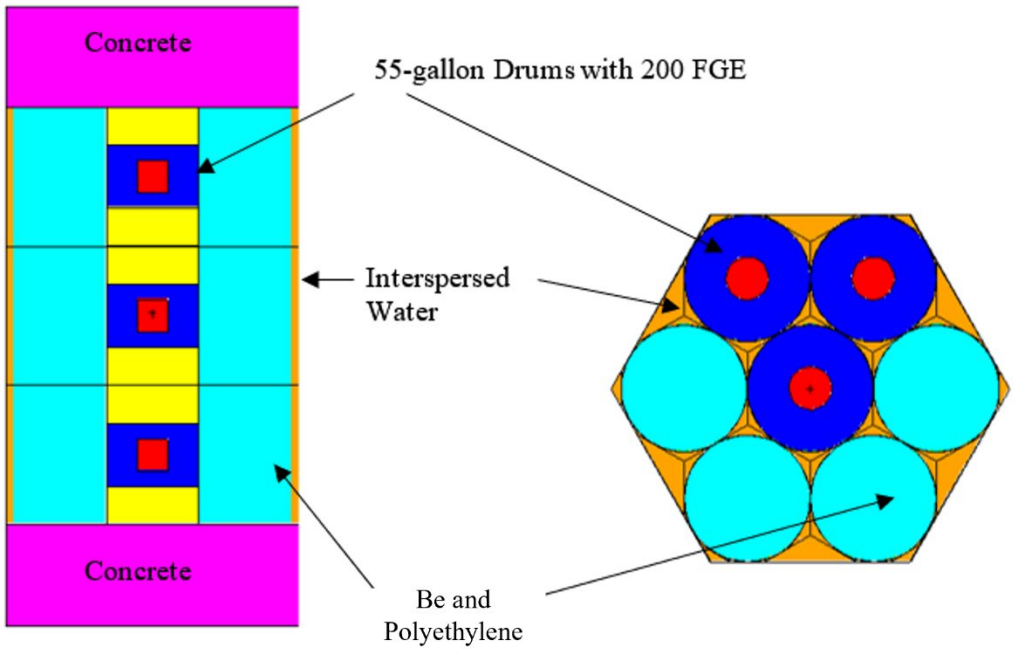

Figure C-15. Sprinkler Activation Contingency Model with Interspersed Water

Table C-18. Sprinkler Activation Results for Array of 55-Gallon Drums Containing Compacted Waste

Water density (g/cm^3)	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
0.05	0.86198	0.00026	0.86250	55arw05
0.10	0.86162	0.00025	0.86212	55arw10
0.15	0.86167	0.00026	0.86219	55arw15
0.20	0.86164	0.00025	0.86214	55arw20
0.25	0.86205	0.00026	0.86257	55arw25
0.30	0.86111	0.00025	0.86161	55arw30
0.35	0.86169	0.00025	0.86219	55arw35
0.40	0.86163	0.00025	0.86213	55arw40
0.45	0.86218	0.00026	0.86270	55arw45
0.50	0.86207	0.00025	0.86257	55arw50
0.55	0.86168	0.00025	0.86218	55arw55
0.60	0.86173	0.00025	0.86223	55arw60
0.65	0.86229	0.00026	0.86281	55arw65
0.70	0.86128	0.00025	0.86178	55arw70
0.75	0.86157	0.00026	0.86209	55arw75
0.80	0.86152	0.00026	0.86204	55arw80
0.85	0.86187	0.00025	0.86237	55arw85
0.90	0.86162	0.00026	0.86214	55arw90
0.95	0.86189	0.00025	0.86239	55arw95
1.00	0.86157	0.00026	0.86209	5arw100

C.7 Conclusions

This appendix demonstrates that containers of machine-compacted waste containing less than or equal to 1 wt% special reflector materials will remain below the USL in the two-container configuration as well in the underground array with the following limits:

- 55-, 85- or 100- gallon drums of fully compacted waste:
  - Maximum 170 FGE/drum,
  - Maximum 5 kilograms of particulate beryllium/drum, and
  - Maximum 600 FGE per pack of drums
- 55-, 85- or 100- gallon drums of fully compacted waste:
  - Maximum 200 FGE/drum if minimum 0.5-inch spacing between drum content and exterior top and bottom is maintained, even if a smaller drum were placed on top of the drum,
  - Maximum 5 kilograms of particulate beryllium/drum, and
  - Maximum 600 FGE per pack of drums
- 55-, 85- or 100- gallon drums of partially (less than or equal to 70%) compacted waste:
  - Maximum 200 FGE/drum,
  - Maximum 5 kilograms of particulate beryllium/drum, and

  - Maximum 600 FGE per pack of drums

- SWB containers of fully or partially compacted waste:
  - Maximum 200 FGE/SWB, and
  - Maximum 18.14 kilograms of particulate beryllium/SWB

C.8 References

BNFL, 2001. *General Arrangement & Details 100-Gallon Puck Drum*, BNFL 53-9840, Revision 8, BNFL Inc., Idaho Falls, ID.

DOE-CBFO, 2022. *Contact-Handled Transuranic Waste Authorized Methods for Payload Control (CH-TRAMPAC)*, Revision 6, February 2022, U.S. Department of Energy, Carlsbad Field Office, Carlsbad, NM.

DOE-CBFO, 2025. *TRUPACT-II Safety Analysis Report*, Revision 27, May 2025, U.S. Department of Energy, Carlsbad Field Office, Carlsbad, NM.

C.9 Sample MCNP6.2 Input File Listings for Appendix C

C.9.1 MCNP Input File 100-gallon Drum Array (Filename aray118)

```
C CCCC
```

```
C                                                                                $
20    1    -0.95317   -40  -41  42                          U=1   IMP:N=1        $
21    2    -0.92650   -43  -44  45 (40:41:-42)              U=1   IMP:N=1        $
22    3    -0.92650   -46  -47  48  #20 #21                 U=1   IMP:N=1        $
23    7    -3.93000   -49  -50  51  (46:47:-48)             U=1   IMP:N=1        $
24    0               -52  -53  54  #20 #21 #22 #23         U=1   IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR THE FIRST 100 GALLON DRUM IN THE MIDDLE 3-PACK ARRANGMENT.  $
C     THE FISSILE MASS IS LOCATED IN THE MIDLE OF THE DRUM.                      $
C                                                                                $
30    1    -0.95317   -60  -61  62                          U=1   IMP:N=1        $
31    2    -0.92650   -63  -64  65 (60:61:-62)              U=1   IMP:N=1        $
32    3    -0.92650   -66  -67  68  #30 #31                 U=1   IMP:N=1        $
33    7    -3.93000   -69  -70  71  (66:67:-68)             U=1   IMP:N=1        $
34    0               -72  -73  74  #30 #31 #32 #33         U=1   IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR THE SECOND 100 GALLON DRUM IN THE MIDDLE 3-PACK ARRANGMENT.$
C     THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.                     $
C                                                                                $
40    1    -0.95317   -80  -81  82                          U=1   IMP:N=1        $
41    2    -0.92650   -83  -84  85 (80:81:-82)              U=1   IMP:N=1        $
42    3    -0.92650   -86  -87  88  #40 #41                 U=1   IMP:N=1        $
43    7    -3.93000   -89  -90  91  (86:87:-88)             U=1   IMP:N=1        $
44    0               -92  -93  94  #40 #41 #42 #43         U=1   IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR THE THIRD 100 GALLON DRUM IN THE MIDDLE 3-PACK ARRANGMENT.  $
C     THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.                     $
C                                                                                $
50    1    -0.95317  -100 -101 102                         U=1   IMP:N=1        $
51    2    -0.92650  -103 -104 105 (100:101:-102)          U=1   IMP:N=1        $
52    3    -0.92650  -106 -107 108  #50 #51                U=1   IMP:N=1        $
53    7    -3.93000  -109 -110 111  (106:107:-108)         U=1   IMP:N=1        $
54    0              -112 -113 114  #50 #51 #52 #53         U=1   IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR THE FIRST 100 GALLON DRUM IN THE UPPER 3-PACK ARRANGMENT.   $
C     THE FISSILE MASS IS LOCATED IN THE MIDLE OF THE DRUM.                      $
C                                                                                $
60    1    -0.95317  -120 -121 122                         U=1   IMP:N=1        $
61    2    -0.92650  -123 -124 125 (120:121:-122)          U=1   IMP:N=1        $
62    3    -0.92650  -126 -127 128 #60 #61                 U=1   IMP:N=1        $
63    7    -3.93000  -129 -130 131 (126:127:-128)          U=1   IMP:N=1        $
64    0              -132 -133 134 #60 #61 #62 #63         U=1   IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR THE SECOND 100 GALLON DRUM IN THE UPPER 3-PACK ARRANGMENT.  $
C     THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.                     $
C                                                                                $
70    1    -0.95317  -140 -141 142                         U=1   IMP:N=1        $
71    2    -0.92650  -143 -144 145 (140:141:-142)          U=1   IMP:N=1        $
72    3    -0.92650  -146 -147 148 #70 #71                 U=1   IMP:N=1        $
73    7    -3.93000  -149 -150 151 (146:147:-148)          U=1   IMP:N=1        $
74    0              -152 -153 154 #70 #71 #72 #73         U=1   IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR THE THIRD 100 GALLON DRUM IN THE UPPER 3-PACK ARRANGMENT.   $
C     THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.                     $
C                                                                                $
80    1    -0.95317  -160 -161 162                         U=1   IMP:N=1        $
81    2    -0.92650  -163 -164 165 (160:161:-162)          U=1   IMP:N=1        $
82    3    -0.92650  -166 -167 168  #80 #81                U=1   IMP:N=1        $
83    7    -3.93000  -169 -170 171  (166:167:-168)         U=1   IMP:N=1        $
84    0              -172 -173 174  #80 #81 #82 #83         U=1   IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR A 3-PACK UNIT PLACED ON A EQUILATERAL TRIANGULAR FOOTPRINT.$
C                                                                                $
90    0              -200 -201 202 #1  #2  #3  #4  #5            &              $
                                   #10 #11 #12 #13 #14          &              $
                                   #20 #21 #22 #23 #24          &              $
                                   #30 #31 #32 #33 #34          &              $
                                   #40 #41 #42 #43 #44          &              $
                                   #50 #51 #52 #53 #54          &              $
                                   #60 #61 #62 #63 #64          &              $
```

```
                                  #70 #71 #72 #73 #74          &              $
                                  #80 #81 #82 #83 #84     U=1  IMP:N=1        $
91    0              (200:201:-202)                       U=1  IMP:N=1        $
C                                                                             $
C     CELL CARDS FOR A HEXAPRISM LATTICE UNIT CONTAINING THE 3-PACKS.         $
C                                                                             $
100   0              -300 301 -302 303 -304 305 -306 307         &            $
                                              FILL=1          IMP:N=1         $
C                                                                             $
C     CELL CARDS FOR THE MgO ON THE TOP LAYER OF DRUMS.                       $
C                                                                             $
110   8    -1.4500   -400 401 -402 403 -404 405 -406 407 306     IMP:N=1       $
C                                                                             $
C     CELL CARDS FOR A HEXAGONAL ARRAY BOUNDARY WITH MIRROR REFLECTION IN THE $
C     X & Y PLANE AND 200 CM SALT REFLECTION IN THE UPPER AND LOWER Z PLANE.  $
C                                                                             $
120   0              -500 501 -502 503 -504 505 -506 507         &            $
                     (400:-401:402:-403:404:-405:406:-307)       IMP:N=1       $
130   9    -2.165    -500 501 -502 503 -504 505 -600 506         IMP:N=1       $
140   9    -2.165    -500 501 -502 503 -504 505 -507 601         IMP:N=1       $
C                                                                             $
C     CELL CARDS FOR EVERYTHING OUTSIDE THE COMPUTATIONAL SPACE.              $
C                                                                             $
150   0              (500:-501:502:-503:504:-505:600:-601)       IMP:N=0       $

C                                                                             $
C     SURFACE CARDS FOR THE FIRST 100 GALLON DRUM IN THE LOWER 3-PACK         $
C     ARRANGMENT.  THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.     $
C                                                                             $
1   1    CZ    9.70878                                                        $
2   1    PZ   52.88192                                                        $
3   1    PZ   33.46436                                                        $
4   1    CZ   38.10000                                                        $
5   1    PZ   67.07228                                                        $
6   1    PZ   19.27400                                                        $
7   1    CZ   38.10000                                                        $
8   1    PZ   86.19439                                                        $
9   1    PZ    0.15189                                                        $
10  1    CZ   38.25189                                                        $
11  1    PZ   86.34628                                                        $
12  1    PZ    0.00000                                                        $
13  1    CZ   38.81095                                                        $
14  1    PZ   86.34628                                                        $
15  1    PZ    0.00000                                                        $
C                                                                             $
C     SURFACE CARDS FOR THE SECOND 100 GALLON DRUM IN THE LOWER 3-PACK        $
C     ARRANGMENT. THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.      $
C                                                                             $
20  2    CZ    9.70878                                                        $
21  2    PZ   52.88192                                                        $
22  2    PZ   33.46436                                                        $
23  2    CZ   38.10000                                                        $
24  2    PZ   67.07228                                                        $
25  2    PZ   19.27400                                                        $
26  2    CZ   38.10000                                                        $
27  2    PZ   86.19439                                                        $
28  2    PZ    0.15189                                                        $
29  2    CZ   38.25189                                                        $
30  2    PZ   86.34628                                                        $
31  2    PZ    0.00000                                                        $
32  2    CZ   38.81095                                                        $
33  2    PZ   86.34628                                                        $
34  2    PZ    0.00000                                                        $
C                                                                             $
C     SURFACE CARDS FOR THE THIRD 100 GALLON DRUM IN THE LOWER 3-PACK         $
C     ARRANGMENT.  THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.     $
C                                                                             $
40  3    CZ    9.70878                                                        $
41  3    PZ   52.88192                                                        $
42  3    PZ   33.46436                                                        $
```

```
43  3    CZ   38.10000                                                    $
44  3    PZ   67.07228                                                    $
45  3    PZ   19.27400                                                    $
46  3    CZ   38.10000                                                    $
47  3    PZ   86.19439                                                    $
48  3    PZ    0.15189                                                    $
49  3    CZ   38.25189                                                    $
50  3    PZ   86.34628                                                    $
51  3    PZ    0.00000                                                    $
52  3    CZ   38.81095                                                    $
53  3    PZ   86.34628                                                    $
54  3    PZ    0.00000                                                    $
C                                                                        $
C     SURFACE CARDS FOR THE FIRST 100 GALLON DRUM IN THE MIDDLE 3-PACK   $
C     ARRANGMENT.  THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM. $
C                                                                        $
60  4    CZ    9.70878                                                    $
61  4    PZ   52.88192                                                    $
62  4    PZ   33.46436                                                    $
63  4    CZ   38.10000                                                    $
64  4    PZ   67.07228                                                    $
65  4    PZ   19.27400                                                    $
66  4    CZ   38.10000                                                    $
67  4    PZ   86.19439                                                    $
68  4    PZ    0.15189                                                    $
69  4    CZ   38.25189                                                    $
70  4    PZ   86.34628                                                    $
71  4    PZ    0.00000                                                    $
72  4    CZ   38.81095                                                    $
73  4    PZ   86.34628                                                    $
74  4    PZ    0.00000                                                    $
C                                                                        $
C     SURFACE CARDS FOR THE SECOND 100 GALLON DRUM IN THE MIDDLE 3-PACK  $
C     ARRANGMENT. THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.  $
C                                                                        $
80  5    CZ    9.70878                                                    $
81  5    PZ   52.88192                                                    $
82  5    PZ   33.46436                                                    $
83  5    CZ   38.10000                                                    $
84  5    PZ   67.07228                                                    $
85  5    PZ   19.27400                                                    $
86  5    CZ   38.10000                                                    $
87  5    PZ   86.19439                                                    $
88  5    PZ    0.15189                                                    $
89  5    CZ   38.25189                                                    $
90  5    PZ   86.34628                                                    $
91  5    PZ    0.00000                                                    $
92  5    CZ   38.81095                                                    $
93  5    PZ   86.34628                                                    $
94  5    PZ    0.00000                                                    $
C                                                                        $
C     SURFACE CARDS FOR THE THIRD 100 GALLON DRUM IN THE MIDDLE 3-PACK   $
C     ARRANGMENT.  THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM. $
C                                                                        $
100 6    CZ    9.70878                                                   $
101 6    PZ   52.88192                                                   $
102 6    PZ   33.46436                                                   $
103 6    CZ   38.10000                                                   $
104 6    PZ   67.07228                                                   $
105 6    PZ   19.27400                                                   $
106 6    CZ   38.10000                                                   $
107 6    PZ   86.19439                                                   $
108 6    PZ    0.15189                                                   $
109 6    CZ   38.25189                                                   $
110 6    PZ   86.34628                                                   $
111 6    PZ    0.00000                                                   $
112 6    CZ   38.81095                                                   $
113 6    PZ   86.34628                                                   $
114 6    PZ    0.00000                                                   $
C                                                                        $
```

```
C     SURFACE CARDS FOR THE FIRST 100 GALLON DRUM IN THE UPPER 3-PACK          $
C     ARRANGMENT.  THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.      $
C                                                                              $
120 7    CZ    9.70878                                                         $
121 7    PZ   52.88192                                                         $
122 7    PZ   33.46436                                                         $
123 7    CZ   38.10000                                                         $
124 7    PZ   67.07228                                                         $
125 7    PZ   19.27400                                                         $
126 7    CZ   38.10000                                                         $
127 7    PZ   86.19439                                                         $
128 7    PZ    0.15189                                                         $
129 7    CZ   38.25189                                                         $
130 7    PZ   86.34628                                                         $
131 7    PZ    0.00000                                                         $
132 7    CZ   38.81095                                                         $
133 7    PZ   86.34628                                                         $
134 7    PZ    0.00000                                                         $
C                                                                              $
C     SURFACE CARDS FOR THE SECOND 100 GALLON DRUM IN THE UPPER 3-PACK         $
C     ARRANGMENT.  THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.      $
C                                                                              $
140 8    CZ    9.70878                                                         $
141 8    PZ   52.88192                                                         $
142 8    PZ   33.46436                                                         $
143 8    CZ   38.10000                                                         $
144 8    PZ   67.07228                                                         $
145 8    PZ   19.27400                                                         $
146 8    CZ   38.10000                                                         $
147 8    PZ   86.19439                                                         $
148 8    PZ    0.15189                                                         $
149 8    CZ   38.25189                                                         $
150 8    PZ   86.34628                                                         $
151 8    PZ    0.00000                                                         $
152 8    CZ   38.81095                                                         $
153 8    PZ   86.34628                                                         $
154 8    PZ    0.00000                                                         $
C                                                                              $
C     SURFACE CARDS FOR THE THIRD 100 GALLON DRUM IN THE UPPER 3-PACK          $
C     ARRANGMENT.  THE FISSILE MASS IS LOCATED IN THE MIDDLE OF THE DRUM.      $
C                                                                              $
160 9    CZ    9.70878                                                         $
161 9    PZ   52.88192                                                         $
162 9    PZ   33.46436                                                         $
163 9    CZ   38.10000                                                         $
164 9    PZ   67.07228                                                         $
165 9    PZ   19.27400                                                         $
166 9    CZ   38.10000                                                         $
167 9    PZ   86.19439                                                         $
168 9    PZ    0.15189                                                         $
169 9    CZ   38.25189                                                         $
170 9    PZ   86.34628                                                         $
171 9    PZ    0.00000                                                         $
172 9    CZ   38.81095                                                         $
173 9    PZ   86.34628                                                         $
174 9    PZ    0.00000                                                         $
C                                                                              $
C     SURFACE CARDS FOR A BOUNDARY AROUND THE 3-PACK STACK.                    $
C                                                                              $
200      CZ   83.62598                                                         $
201      PZ  259.03884                                                         $
202      PZ    0.00000                                                         $
C                                                                              $
C     SURFACE CARDS FOR A HEXAPRISM LATTICE UNIT CONTAINING THE 3-PACK STACK.  $
C                                                                              $
300      PX   83.62598                                                         $
301      PX  -83.62598                                                         $
302      P  1  1.73205  0  167.25196                                          $
303      P  1  1.73205  0 -167.25196                                          $
304      P -1  1.73205  0  167.25196                                          $
```

```
305      P -1  1.73205  0 -167.25196                                          $
306      PZ  259.03884                                                       $
307      PZ    0.00000                                                       $
C                                                                            $
C     SURFACE CARDS FOR THE MgO ON THE TOP LAYER OF DRUMS.                   $
C                                                                            $
400      PX   83.62598                                                       $
401      PX  -83.62598                                                       $
402      P  1  1.73205  0  167.25196                                         $
403      P  1  1.73205  0 -167.25196                                         $
404      P -1  1.73205  0  167.25196                                         $
405      P -1  1.73205  0 -167.25196                                         $
406      PZ  321.26884                                                       $
407      PZ  259.03884                                                       $
C                                                                            $
C     CELL CARDS FOR A HEXAGONAL ARRAY BOUNDARY WITH MIRROR REFLECTION IN THE $
C     X & Y PLANE AND 300 CM SALT REFLECTION IN THE UPPER AND LOWER Z PLANE.  $
C                                                                            $
*500    PX   83.87598                                                        $
*501    PX  -83.87598                                                        $
*502    P  1  1.73205  0  167.75196                                          $
*503    P  1  1.73205  0 -167.75196                                          $
*504    P -1  1.73205  0  167.75196                                          $
*505    P -1  1.73205  0 -167.75196                                          $
506    PZ  321.51884                                                        $
507    PZ   -0.25000                                                        $
600    PZ  621.51884                                                        $
601    PZ -300.25000                                                        $

C                                                                            $
C     MODE CARD.                                                             $
C                                                                            $
MODE N                                                                       $
C                                                                            $
C     TRANSFORMATION CARDS FOR THE 3-PACK STACK.                             $
C                                                                            $
TR1   38.81095    22.40751     0.00000                                       $
TR2  -38.81095    22.40751     0.00000                                       $
TR3    0.00000   -44.81503     0.00000                                       $
TR4   38.81095    22.40751    86.34628                                       $
TR5  -38.81095    22.40751    86.34628                                       $
TR6    0.00000   -44.81503    86.34628                                       $
TR7   38.81095    22.40751   172.69256                                       $
TR8  -38.81095    22.40751   172.69256                                       $
TR9    0.00000   -44.81503   172.69256                                       $
C                                                                            $
C     MATERIAL CARDS                                                         $
C                                                                            $
C                                                                            $
C     PU-CH2                                                                 $
C                                                                            $
M1     1001.00C -0.138469  6012.00C -0.815482  6013.00C -9.5575E-03           $
         94239.00C -0.036491                                                 $
C                                                                            $
C     BE-CH2 REFLECTOR                                                       $
C                                                                            $
M2     4009.00C -0.01396  1001.00C -0.14171  6012.00C -0.83455               $
          6013.00C -9.7810E-03                                               $
C                                                                            $
C     CH2 DUNNAGE                                                            $
C                                                                            $
M3     4009.00C -0.01396  1001.00C -0.14171  6012.00C -0.83455               $
          6013.00C -9.7810E-03                                               $
C                                                                            $
C     CARBON STEEL DRUM.                                                     $
C                                                                            $
M7     6012.00C  1.4830E-03   6013.00C 1.7000E-05  15031.00C  3.5000E-04      $
      16032.00C  3.7861E-04  16033.00C 3.1258E-06  16034.00C  1.8178E-05      $
      16035.00C  8.9732E-08  25055.00C 6.0000E-03  26054.00C  5.5990E-02      $
      26056.00C  9.1143E-01  26057.00C 2.1425E-02  26058.00C  2.9013E-03      $
```

```
C                                                                               $
C     MgO                                                                       $
C                                                                               $
M8     8016.00C  0.5  12024.00C  0.39495  12025.00C  0.05  12026.00C  0.05505   $
C                                                                               $
C     SALT                                                                      $
C                                                                               $
M9     11023.00C  0.5  17035.00C  0.3789  17037.00C  0.1211                     $
C                                                                               $
C     S(ALPHA,BETA)                                                             $
C                                                                               $
MT1   H-POLY.40T                                                                $
MT2   H-POLY.40T   BE-MET.40T                                                   $
MT3   H-POLY.40T   BE-MET.40T                                                   $
C                                                                               $
C    SOURCE CARDS                                                               $
C                                                                               $
KCODE  10000     1.0      300  1300                                            $
KSRC   38.81095    22.40751   44.81503                                         $
PRINT                                                                           $
C                                                                               $
C    PRINT TO MCTAL FILE                                                        $
C                                                                               $
PRDMP 2j 1                                                                      $
```

C.9.2 MCNP Input File SWB Array (Filename ar900_200)

```
FULLY COMPACTED SWB ARRAY MODEL: 3 SWBs, 200G PU, H/PU=900            1/8/05   $
C     100% POLYETHYLENE MODERATOR; THE FISSILE MASS IN EACH VOLUME IS           $
C     REFLECTED BY A MIXTURE OF 18.14 KGS. OF BERYLLIUM AND 100% POLYETHYLENE.  $
C     THE FISSILE MASSES IN ALL THE CONTAINERS ARE CYLINDRICAL WITH H/D=1       $
C     AND CENTERED WITHIN THE VOLUME. THE STACK IS EMPLACED IN A HEXIPRISM      $
C     LATTICE WITH SIX LATERAL SIDES OF THE PRISM MIRRORED TO SIMULATE  AN      $
C     INFINITE ARRAY. THE TOP OF THE STACK CONSISTS OF 62.23 CM OF MgO AND      $
C     BOTH CEILING AND FLOOR ARE REFLECTED BY 300 CM OF SALT.                   $
C                                                                               $
C     WIPP-016, Rev. 8  08 JAN 2026                                             $
C        MACHINE COMPACTED SWB                                                  $
C        INCREASE SWB FGE TO 250G PU                                            $
C        UPDATED TO ENDF/B-VIII.0                                               $
C        MATERIALS CONVERTED FROM ELEMENTAL TO ISOTOPIC                         $
C        POLY DEN REVISED TO 0.92 G/CC                                          $
C        REMOVED GRPH TSL; STEEL SET TO 60% TD                                  $
C        REVISED MATERIALS TO WEIGHT PERCENTS MATCHING TABLES H-7, ETC.         $
C                                                                               $
C     WIPP-016, Rev. 8  06 MAY 2026                                             $
C        REVISED MATERIAL DENSITIES AND WEIGHT PERCENTS TO MATCH TABLES 5-1     $
C        UPDATED STEEL DENSITY TO 4.716 FROM 4.71                               $
C                                                                               $
C     WIPP-016, Rev. 8  08 JUN 2026                                             $
C        DECREASED SWB FGE TO 200G PU DUE TO PISA AND EXTENT OF COND.           $
C                                                                               $
C CCCC
```

```
C                                                                                $
C     CELL CARDS FOR THE UPPER UPPER SWB.                                        $
C                                                                                $
21    LIKE 1 BUT TRCL=2                                                          $
22    2    -0.92476   -47  -48  49  -50  51  #21           U=1   IMP:N=1        $
23    LIKE 3 BUT TRCL=2                                                          $
24    0               -57  -58  59  #21  #22  #23          U=1   IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR A 3 STACK UNIT.                                             $
C                                                                                $
90    0              -200 -201 202  #1  #2  #3  #4               &              $
                                  #11 #12 #13 #14               &              $
                                  #21 #22 #23 #24         U=1   IMP:N=1        $
91    0              (200:201:-202)                     U=1   IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR A HEXAPRISM LATTICE UNIT CONTAINING THE STACK.              $
C                                                                                $
100   0              -300 301 -302 303 -304 305 -306 307         &              $
                                             FILL=1         IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR THE MgO ON THE TOP LAYER.                                   $
C                                                                                $
110   10   -1.4500   -400 401 -402 403 -404 405 -406 407 306     IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR A HEXAGONAL ARRAY BOUNDARY WITH MIRROR REFLECTION IN THE    $
C     X & Y PLANE AND 200 CM SALT REFLECTION IN THE UPPER AND LOWER Z PLANE.     $
C                                                                                $
120   0              -500 501 -502 503 -504 505 -506 507         &              $
                     (400:-401:402:-403:404:-405:406:-307)       IMP:N=1        $
130   11   -2.165    -500 501 -502 503 -504 505 -600 506         IMP:N=1        $
140   11   -2.165    -500 501 -502 503 -504 505 -507 601         IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR EVERYTHING OUTSIDE THE COMPUTATIONAL SPACE.                 $
C                                                                                $
150   0              (500:-501:502:-503:504:-505:600:-601)       IMP:N=0        $

C                                                                                $
C     SURFACE CARDS FOR THE LOWER SWB.                                           $
C                                                                                $
1        CZ    9.70878                                                         $
2        PZ   56.69878                                                         $
3        PZ   37.28122                                                         $
7        CZ   87.31250                                                         $
8        PZ   93.66250                                                         $
9        PZ    0.31750                                                         $
10       PY   65.88125                                                         $
11       PY  -65.88125                                                         $
12       CZ   87.63000                                                         $
13       PZ   93.98000                                                         $
14       PZ    0.00000                                                         $
15       PY   66.19875                                                         $
16       PY  -66.19875                                                         $
17       CZ   87.63000                                                         $
18       PZ   93.98000                                                         $
19       PZ   -0.25000                                                         $
C                                                                                $
C     SURFACE CARDS FOR THE MIDDLE SWB.                                          $
C                                                                                $
27  1    CZ   87.31250                                                         $
28  1    PZ   93.66250                                                         $
29  1    PZ    0.31750                                                         $
30  1    PY   65.88125                                                         $
31  1    PY  -65.88125                                                         $
37  1    CZ   87.63000                                                         $
38  1    PZ   93.98000                                                         $
39  1    PZ    0.00000                                                         $
C                                                                                $
C     SURFACE CARDS FOR THE MIDDLE SWB.                                          $
C                                                                                $
47  2    CZ   87.31250                                                         $
```

```
48  2    PZ   93.66250                                                    $
49  2    PZ    0.31750                                                    $
50  2    PY   65.88125                                                    $
51  2    PY  -65.88125                                                    $
57  2    CZ   87.63000                                                    $
58  2    PZ   93.98000                                                    $
59  2    PZ    0.00000                                                    $
C                                                                        $
C     SURFACE CARDS FOR A BOUNDARY AROUND THE SWB STACK.                 $
C                                                                        $
200      CZ   87.63000                                                   $
201      PZ  281.94000                                                   $
202      PZ   -0.25000                                                   $
C                                                                        $
C     SURFACE CARDS FOR A HEXAPRISM LATTICE UNIT CONTAINING THE SWB STACK.  $
C                                                                        $
300      PX   87.63000                                                   $
301      PX  -87.63000                                                   $
302      P  1  1.73205  0  175.26000                                     $
303      P  1  1.73205  0 -175.26000                                     $
304      P -1  1.73205  0  175.26000                                     $
305      P -1  1.73205  0 -175.26000                                     $
306      PZ  281.94000                                                   $
307      PZ    0.00000                                                   $
C                                                                        $
C     SURFACE CARDS FOR THE MgO ON THE TOP.                              $
C                                                                        $
400      PX   87.63000                                                   $
401      PX  -87.63000                                                   $
402      P  1  1.73205  0  175.26000                                     $
403      P  1  1.73205  0 -175.26000                                     $
404      P -1  1.73205  0  175.26000                                     $
405      P -1  1.73205  0 -175.26000                                     $
406      PZ  344.17000                                                   $
407      PZ  281.94000                                                   $
C                                                                        $
C     CELL CARDS FOR A HEXAGONAL ARRAY BOUNDARY WITH MIRROR REFLECTION IN THE   $
C     X & Y PLANE AND 300 CM SALT REFLECTION IN THE UPPER AND LOWER Z PLANE.    $
C                                                                        $
*500    PX   87.88000                                                   $
*501    PX  -87.88000                                                   $
*502    P  1  1.73205  0  175.76000                                     $
*503    P  1  1.73205  0 -175.76000                                     $
*504    P -1  1.73205  0  175.76000                                     $
*505    P -1  1.73205  0 -175.76000                                     $
506     PZ  344.17000                                                   $
507     PZ   -0.25000                                                   $
600     PZ  644.17000                                                   $
601     PZ -300.25000                                                   $

C                                                                        $
C     MODE CARD.                                                         $
C                                                                        $
MODE N                                                                   $
C                                                                        $
C     TRANSFORMATION CARDS FOR THE STACK.                                $
C                                                                        $
TR1   0.0  0.0  93.98                                                    $
TR2   0.0  0.0 187.96                                                    $
C                                                                        $
C     MATERIAL CARDS                                                     $
C                                                                        $
C     PU-CH2 (SWB)                                                       $
C                                                                        $
M1   1001.00c -13.8469  6012.00c -81.5482  6013.00c -0.95575  94239.00c -3.6491 $
C                                                                        $
C     BE-CH2 REFLECTOR (SWB)                                             $
C                                                                        $
M2     4009.00C  -0.01025   1001.00C -0.14224                            $
       6012.00C  -0.83769   6013.00C -9.8178E-03                        $
```

```
C                                                                              $
C     CARBON STEEL DRUM.                                                       $
C                                                                              $
M9     6012.00C  1.4830E-03  6013.00C  1.7000E-05  15031.00C  3.5000E-04       $
      16032.00C  3.7861E-04  16033.00C 3.1258E-06  16034.00C  1.8178E-05       $
      16035.00C  8.9732E-08  25055.00C 6.0000E-03  26054.00C  5.5990E-02       $
      26056.00C  9.1143E-01  26057.00C 2.1425E-02  26058.00C  2.9013E-03       $
C                                                                              $
C     MgO                                                                      $
C                                                                              $
M10    8016.00C  0.5  12024.00C  0.39495  12025.00C  0.05  12026.00C  0.05505   $
C                                                                              $
C     SALT                                                                     $
C                                                                              $
M11   11023.00C 0.5  17035.00C  0.37890  17037.00C  0.1211                      $
C                                                                              $
C     S(ALPHA,BETA)                                                            $
C                                                                              $
MT1   H-POLY.40T                                                               $
MT2   H-POLY.40T   BE-MET.40T                                                  $
C                                                                              $
C    SOURCE CARDS                                                              $
C                                                                              $
KCODE  10000   1.0  500  1500                                                  $
KSRC   0.0  0.0  46.99    0.0  0.0  140.97    0.0  0.0  234.95                 $
PRINT                                                                          $
C                                                                              $
C    PRINT TO MCTAL FILE                                                       $
C                                                                              $
PRDMP 2j 1                                                                     $
```

C.9.3 MCNP Input File Partially Compacted/Fully Compacted 100-gallon drum Two-Container Model (Filename tdc1855)

```
C CCCC
```

```
13    7    -3.93000   -29  -30  31  (26:27:-28)            U=1   IMP:N=1        $
14    0               -32  -33  34  #10  #11  #12  #13     U=1   IMP:N=1        $
15    0               -32  -34  35                         U=1   IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR A BOUNDARY AROUND THE TWO-DRUM MODEL.                       $
C                                                                                $
30    8    -1.4500   -100 -101 102  #1  #2  #3  #4  #5           &              $
                                   #10 #11 #12 #13 #14 #15  U=1   IMP:N=1       $
31    8    -1.4500   (100:101:-102)                          U=1   IMP:N=1  $
C                                                                                $
C     CELL CARDS FOR A HEXAPRISM LATTICE UNIT CONTAINING THE TWO DRUMS.          $
C                                                                                $
50    8    -1.4500   -200 201 -202 203 -204 205 -206 207         &              $
                                              FILL=1         IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR A 300 CM MgO REFLECTOR AROUND THE TWO DRUMS WITH            $
C     MIRROR BOUNDARY CONDITIONS ON ALL SIX SIDES, FLOOR AND CEILING.            $
C                                                                                $
60    8    -1.4500   -300 301 -302 303 -304 305 -306 307         &              $
                     (200:-201:202:-203:204:-205:206:-207)       IMP:N=1        $
C                                                                                $
C     CELL CARDS FOR EVERYTHING OUTSIDE THE COMPUTATIONAL SPACE.                 $
C                                                                                $
100   0               (300:-301:302:-303:304:-305:306:-307)       IMP:N=0        $

C                                                                                $
C     SURFACE CARDS FOR THE LOWER 100 GALLON DRUM IN THE TWO-DRUM MODEL.         $
C                                                                                $
1   1    CZ   10.12536                                                           $
2   1    PZ   38.10000                                                           $
3   1    PZ   27.97464                                                           $
4   1    CZ   38.10000                                                           $
5   1    PZ   38.10000                                                           $
6   1    PZ    0.00000                                                           $
7        CZ   38.10000                                                           $
8        PZ   86.19439                                                           $
9        PZ    0.15189                                                           $
10       CZ   38.25189                                                           $
11       PZ   86.34628                                                           $
12       PZ    0.00000                                                           $
13       CZ   38.81095                                                           $
14       PZ   86.34628                                                           $
15       PZ    0.00000                                                           $
C                                                                                $
C     SURFACE CARDS FOR THE UPPER 100 GALLON DRUM IN THE TWO-DRUM MODEL.         $
C                                                                                $
20  2    CZ   12.42795                                                           $
21  2    PZ   12.57984                                                           $
22  2    PZ    0.15189                                                           $
23  2    CZ   38.10000                                                           $
24  2    PZ   38.25189                                                           $
25  2    PZ    0.15189                                                           $
26  2    CZ   38.10000                                                           $
27  2    PZ   86.19439                                                           $
28  2    PZ    0.15189                                                           $
29  2    CZ   38.25189                                                           $
30  2    PZ   86.34628                                                           $
31  2    PZ    0.00000                                                           $
32  2    CZ   38.81095                                                           $
33  2    PZ   86.34628                                                           $
34  2    PZ    0.00000                                                           $
35  2    PZ   -2.54000                                                           $
C                                                                                $
C     SURFACE CARDS FOR A BOUNDARY AROUND THE TWO-DRUM MODEL.                    $
C                                                                                $
100      CZ   38.81095                                                           $
101      PZ  175.23256                                                           $
102      PZ    0.00000                                                           $
C                                                                                $
C     SURFACE CARDS FOR A HEXAPRISM LATTICE UNIT CONTAINING THE TWO DRUMS.       $
```

```
C                                                                                $
200      PX   38.81095                                                          $
201      PX  -38.81095                                                          $
202      P  1  1.73205  0   77.62190                                            $
203      P  1  1.73205  0  -77.62190                                            $
204      P -1  1.73205  0   77.62190                                            $
205      P -1  1.73205  0  -77.62190                                            $
206      PZ  175.23256                                                          $
207      PZ    0.00000                                                          $
C                                                                                $
C     SURFACE CARDS FOR A 300 CM MgO REFLECTOR AROUND THE TWO DRUMS              $
C     WITH MIRROR BOUNDARY CONDITIONS ON ALL SIX SIDES, FLOOR AND CEILING.       $
C                                                                                $
*300      PX  338.81095                                                         $
*301      PX -338.81095                                                         $
*302      P  1  1.73205  0  677.62190                                           $
*303      P  1  1.73205  0 -677.62190                                           $
*304      P -1  1.73205  0  677.62190                                           $
*305      P -1  1.73205  0 -677.62190                                           $
*306      PZ  475.23256                                                         $
*307      PZ -300.00000                                                         $

C                                                                                $
C     MODE CARD.                                                                 $
C                                                                                $
MODE N                                                                           $
C                                                                                $
C     TRANSFORMATION CARDS FOR THE TWO-DRUM MODEL.                               $
C                                                                                $
TR1   0.00000     0.00000    48.09438                                            $
TR2   0.00000     0.00000    88.88628                                            $
C                                                                                $
C     MATERIAL CARDS                                                             $
C                                                                                $
C                                                                                $
C     PU-CH2 (LOWER DRUM)                                                        $
C                                                                                $
M1     1001.00C -0.135988  6012.00C -0.800870        6013.00C -9.3862E-03       $
          94239.00C -0.053756                                                    $
C                                                                                $
C     BE-CH2 REFLECTOR (LOWER DRUM)                                              $
C                                                                                $
M2     4009.00C -0.01387  1001.00C -0.14172  6012.00C -0.83463                   $
          6013.00C -9.7819E-03                                                   $
C                                                                                $
C     CH2 DUNNAGE (LOWER DRUM)                                                   $
C                                                                                $
M3     4009.00C -0.01387  1001.00C -0.14172  6012.00C -0.83463                   $
          6013.00C -9.7819E-03                                                   $
C                                                                                $
C     PU-CH2-H2O (UPPER DRUM)                                                    $
C                                                                                $
M4     1001.00C -0.129069     6012.00C -0.558074   6013.00C -6.5407E-03         $
          8016.00C -0.272302    94239.00C -0.034014                              $
C                                                                                $
C     BE-CH2 REFLECTOR (UPPER DRUM)                                              $
C                                                                                $
M5     4009.00C -0.01984  1001.00C -0.14086  6012.00C -0.82958                   $
          6013.00C -9.7227E-03                                                   $
C                                                                                $
C     CH2 DUNNAGE  (UPPER DRUM)                                                  $
C                                                                                $
M6     4009.00C -0.01984  1001.00C -0.14086  6012.00C -0.82958                   $
          6013.00C -9.7227E-03                                                   $
C                                                                                $
C     CARBON STEEL DRUM.                                                         $
C                                                                                $
M7     6012.00C  1.4830E-03   6013.00C 1.7000E-05  15031.00C  3.5000E-04         $
      16032.00C  3.7861E-04  16033.00C 3.1258E-06  16034.00C  1.8178E-05         $
      16035.00C  8.9732E-08  25055.00C 6.0000E-03  26054.00C  5.5990E-02         $
```

```
      26056.00C  9.1143E-01  26057.00C 2.1425E-02  26058.00C  2.9013E-03        $
C                                                                               $
C     MgO                                                                       $
C                                                                               $
M8     8016.00C  0.5  12024.00C  0.39495  12025.00C  0.05  12026.00C  0.05505   $
C                                                                               $
C     S(ALPHA,BETA)                                                             $
C                                                                               $
MT1   H-POLY.40T                                                                $
MT2   H-POLY.40T    BE-MET.40T                                                  $
MT3   H-POLY.40T    BE-MET.40T                                                  $
MT4   H-POLY.40T                                                                $
MT5   H-POLY.40T    BE-MET.40T                                                  $
MT6   H-POLY.40T    BE-MET.40T                                                  $
C                                                                               $
C     SOURCE CARDS                                                              $
C                                                                               $
KCODE  10000     1.0      300  1300                                            $
KSRC  0.00000  0.00000  80.00000                                                $
PRINT                                                                           $
C                                                                               $
C     PRINT TO MCTAL FILE                                                       $
C                                                                               $
PRDMP 2j 1                                                                      $
```

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Appendix D 55-gallon Drums Containing Pipe Overpacks

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Note: Appendix D is unaffected by Revision 8 and no changes were made from the previous revision. Original signatures are on file with WIPP-016 Revision 6.

Analyst NCS Engineer in Training	N. Dickes	Date
Analyst Senior NCS Engineer	S. L. Larson	Date
Peer Reviewer Senior NCS Engineer	W.D. Newmyer	Date

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Introduction

In order to allow for increased fissile content in a single shipment and to allow for certain wastes to be CH, several 55-gallon drum Pipe Overpack Containers (POCs) have been approved. The waste is contained within the cylindrical containers that are constructed of 304 stainless steel. Additional shielding can be provided using inserts either inside the pipes or as part of the surrounding dunnage. The waste may be direct loaded (non-compacted) or compacted in a POC. Sample MCNP6.2 input file listings for the models contained in this appendix are included in Section D.6.

This appendix was revised in Revision 6 to evaluate compacted waste in the POCs. The calculations were revised to evaluate machine-compacted waste moderated with 100% dense polyethylene in all loadings, although restrictions, as listed in Section D.4, were required to ensure subcriticality under contingent conditions. Calculations in this appendix were performed with MCNP6.2, and thus the applicable USL is 0.9659 as discussed in Section 4.2.2.

D.1 Pipe Overpack Configurations

The various pipe overpack configurations are described below. Additional details can be found in Sections 2.9.2 through 2.9.5 of the *Contact-Handled Transuranic Waste Authorized Methods for Payload Control (CH-TRAMPAC)* (DOE-CBFO 2020a).

D.1.1 Standard Pipe Overpack

The standard pipe overpack consists of a pipe component positioned by fiberboard/plywood dunnage within a 55-gallon drum with a high-density polyethylene rigid liner and lid as shown in Figure D-1. The pipe components are cylindrical containers with the dimensions given in Table D-1. A standard 12-inch pipe component is shown in Figure D-2. The dunnage consists of cane fiberboard packing in accordance with *Standard Specification for Cellulosic Fiber Insulating Board* [ASTM-C208-95(2001)] and 1/2- or 1/4-inch plywood. In the case of the shielded 6-inch pipe component, a large portion of the dunnage is replaced by a water extended polyester/polyethylene composite or equivalent neutron shielding material.

Table D-1. Pipe Component Dimensions

Pipe Component Size	Dimension	Measurement (in.)
6-inch	Outer Diameter	6.7 Max
	Overall Height	27.5 Max
12-inch	Inner Diameter	12.362 Max
	Outer Diameter	12.8 Max
	Wall Thickness	0.219 Min
	Inner Height	25.45 Max
	Outer Height	27.5 Max
	Lid Thickness	0.9
	Bottom Thickness	0.25 Min

D.1.2 S100 Pipe Overpack

As shown in Figure D-3 and Figure D-4, the S100 pipe overpack is based closely on the standard 6-inch pipe component. It differs from the standard pipe component in that most of the cane fiberboard dunnage is replaced with neutron shielding material. In addition, neutron shielding material is placed within the pipe component, above, below, and around the payload. It is intended for the shipment of sealed neutron

sources. The S100 pipe overpack uses the 6-inch diameter pipe component described in Table D-1. The 12-inch diameter pipe component is not used in the S100 pipe overpack.

The neutron shield around the side of the pipe component may be in the form of a casting (such as a commercial neutron shielding casting compound), a solid monolith (such as a molded or machined unit of solid plastic), or fabricated component (such as a tightly wound roll of plastic film or other built-up fabrication). The end plugs and shield sleeve within the pipe component are made of a rigid plastic.

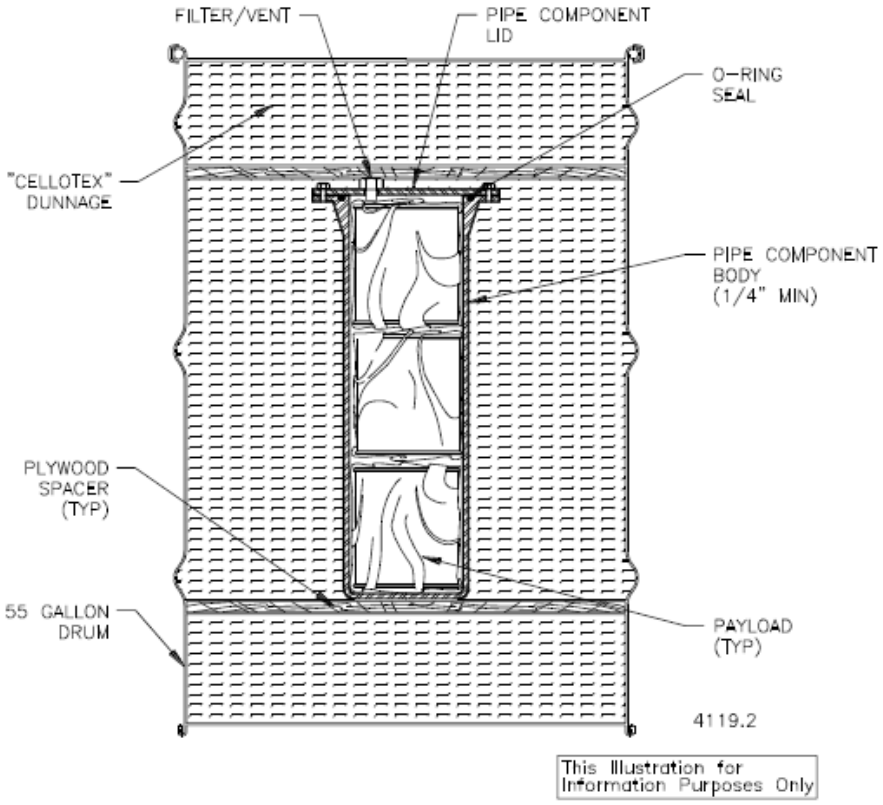

Figure D-1. Standard 6-inch Pipe Component in Overpack Assembly

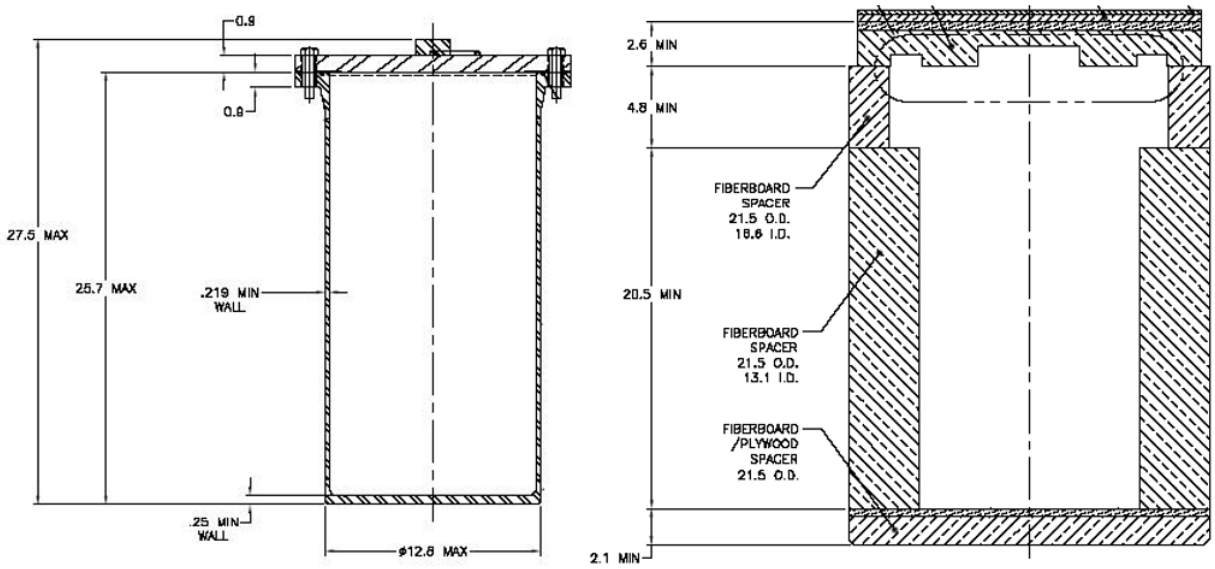

Figure D-2. Standard 12-inch Pipe Component and Dunnage

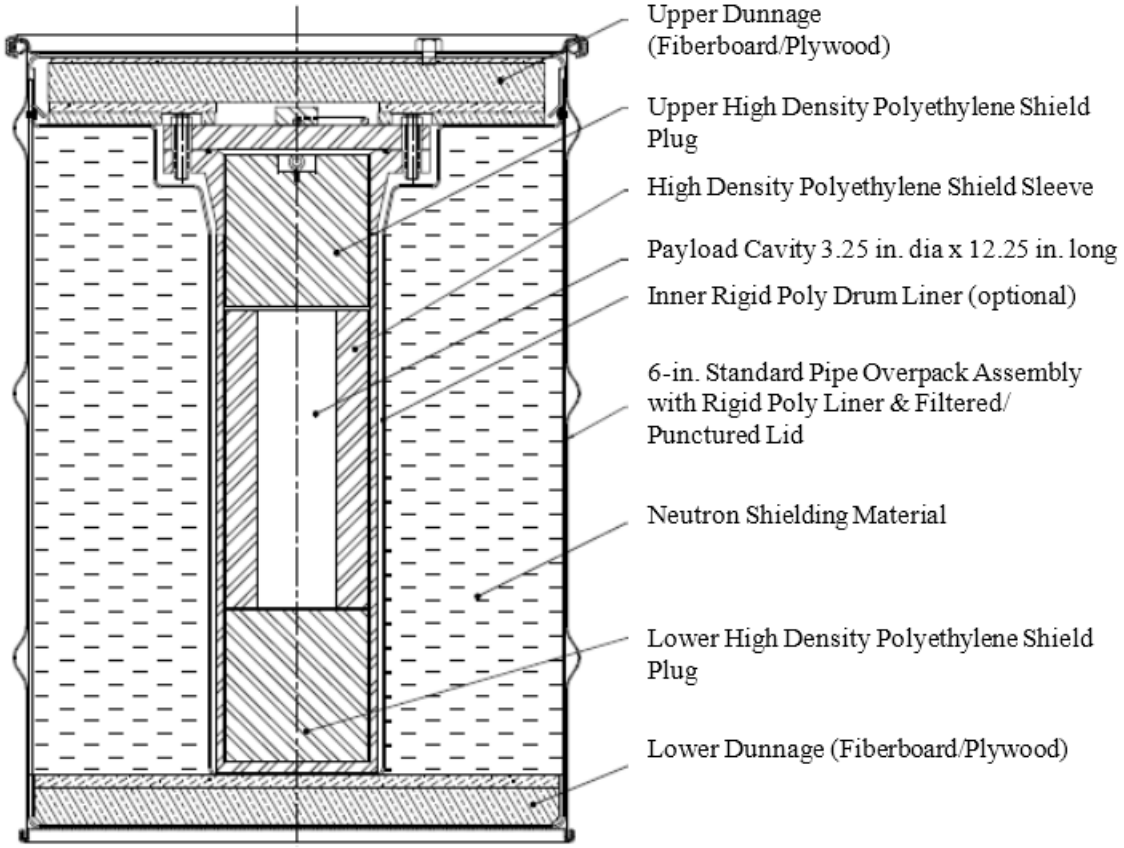

Figure D-3. Configuration for the S100 6-inch Shielded Pipe Overpack

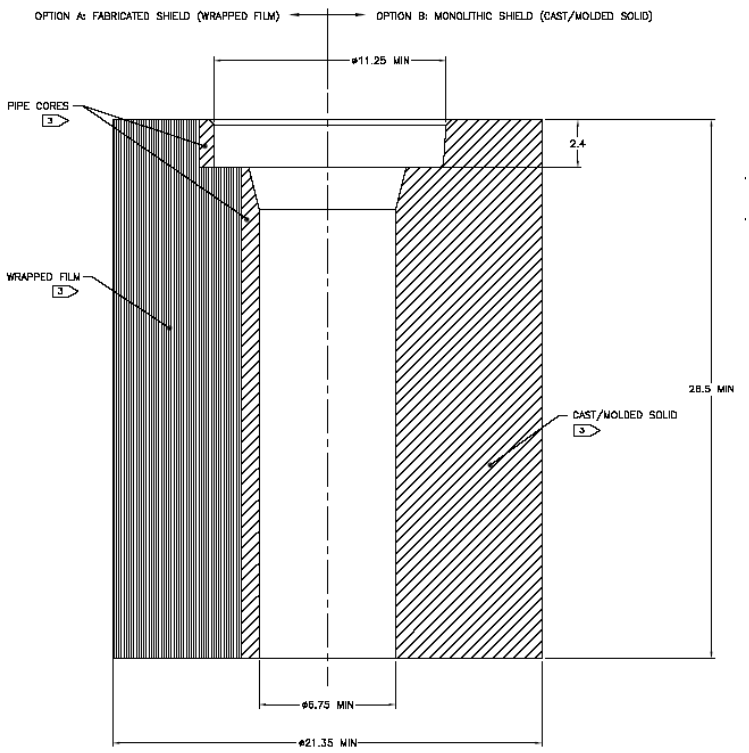

Figure D-4. Dunnage and Shielding for the S100 Shielded 6-inch Pipe Component

D.1.3 S200 Pipe Overpack

The S200 pipe overpack is a shielded version of the standard pipe overpack. It consists of a gamma shield insert located by rigid polyurethane foam dunnage inside a standard 12-inch pipe component which is, in turn, located by cane fiberboard and plywood dunnage within a standard 55-gallon drum with a rigid polyethylene liner and lid. The 12-inch pipe component, cane fiberboard and plywood dunnage, and 55-gallon drum with rigid polyethylene liner and lid are identical to the standard pipe overpack described in Section D.1.1. It differs from the standard pipe overpack through the addition of a gamma shield insert inside the pipe component. It is intended for the shipment and storage of TRU waste forms with high gamma energies. Note that the 6-inch pipe component is not used in the S200 pipe overpack.

The gamma shield insert is a two-component lead assembly consisting of a cylindrical body with an integral bottom cap and a detachable lid. The shield insert is available in two sizes: the S200-A shield insert has a nominal thickness of 1.000 inch and the S200-B shield insert has a nominal thickness of 0.600 inch. Both shield inserts have a nominal inner diameter of 8.125 inches, but the S200-B is significantly longer. The inner height of the S200-A insert is 8.125 inches compared to 16.125 inches for the S200-B. The rigid polyurethane foam dunnage fills the bottom and annular space between the shield insert and the 12-inch pipe component to position the insert near the lid of the pipe component. Figure D-5 shows the S200 pipe overpack assembly and Figure D-6 shows the shielded insert options that may be used within the S200 assembly.

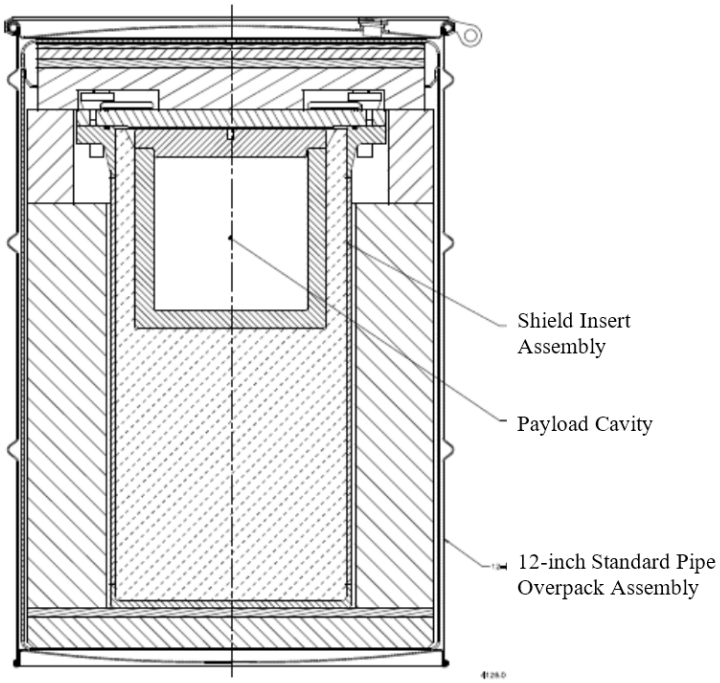

Figure D-5. S200 Shielded 12-inch Pipe Component Overpack Assembly

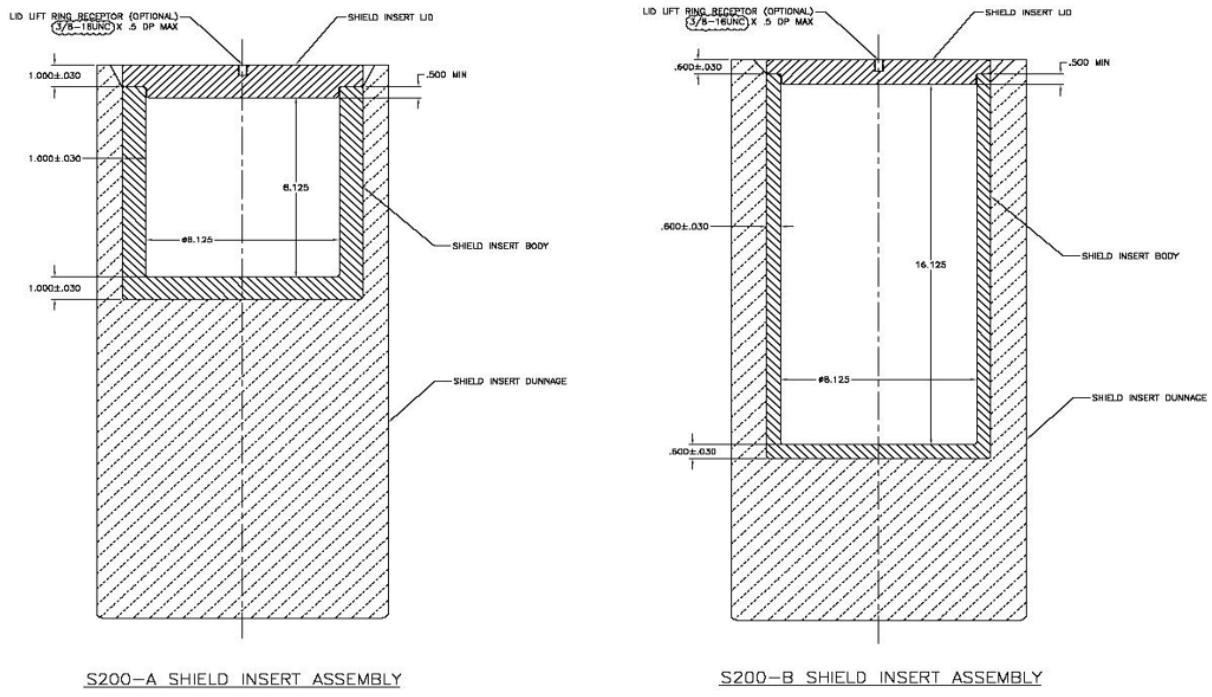

Figure D-6. Shielded Insert Options for the S200 12-inch Pipe Components

D.1.4 S300 Pipe Overpack

The S300 pipe overpack is based closely on the standard pipe overpack described in Section D.1.1. It differs from the standard pipe overpack through the addition of neutron shielding within the pipe component. It is intended for the shipment and storage of sealed neutron sources. The S300 pipe overpack consists of a neutron shield insert placed inside a standard 12-inch pipe component which is, in turn, located by cane fiberboard and plywood dunnage within a standard 55-gallon drum with a rigid polyethylene liner and lid. A schematic of the S300 pipe overpack is shown in Figure D-7. All of the components of the S300 pipe overpack, except the neutron shield insert, are identical to the 12-inch version of the standard pipe overpack. Note that the 6-inch pipe component is not used in the S300 pipe overpack.

The neutron shield insert is a two-part assembly consisting of a cylindrical body and stepped lid shown in Figure D-8. With the exception of necessary clearances, the insert fits within and fills the 12-inch pipe component. The insert lid is held in place by the lid of the pipe component. The insert is made from solid, high-density polyethylene, and has a nominal wall thickness of 4.13 inches.

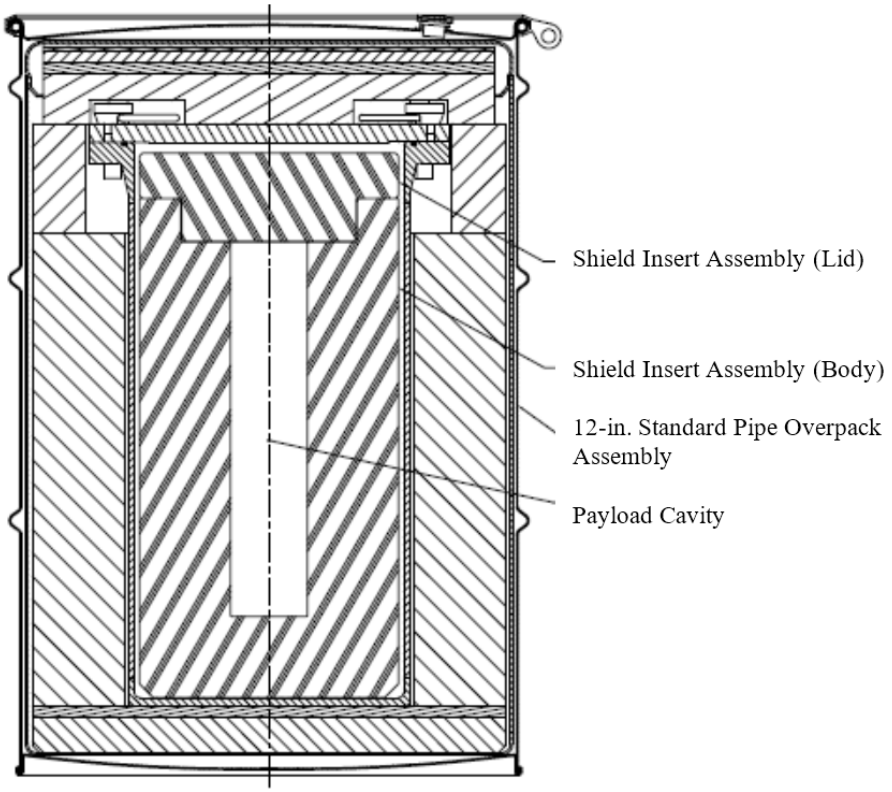

Figure D-7. S300 Pipe Overpack Assembly

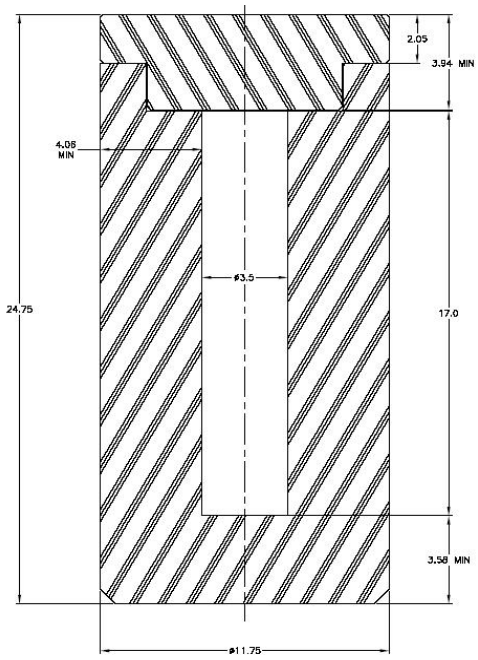

Figure D-8. S300 Shield Insert Assembly

D.2 55-gallon Pipe Overpack MCNP6.2 Models

The unshielded 12-inch pipe overpack is modeled as the bounding pipe overpack configuration as shown in calculation ED-076 supporting the *TRUPACT-II Safety Analysis Report* (DOE-CBFO 2020b). In the reference, each pipe overpack configuration was modeled in an array of TRUPACT-II containers with 14 pipe overpack drums per TRUPACT-II and the unshielded 12-inch pipe overpack resulted in the highest reactivity. The unshielded 12-inch pipe overpack assembly design allows for greater interaction between drums compared to the shielded designs and the larger diameter allows for a more optimum fissile material geometry (i.e., larger radius) over that of the smaller 6-inch pipe overpack and the shielded 12-inch designs. The pipe overpack is modeled using the dimensions in Table D-1. The pipe walls and lid are modeled as 304 stainless steel using the composition from ASTM standard A276/A276M-17 using the midpoint of the range specified for nickel and chromium with the balance being iron, as given in Table D-2. The cane fiberboard used in the pipe overpack assembly as shock-absorbing dunnage is represented by cellulose ($C_6H_{10}O_5$) at a maximum density of 0.2248 g/cm^3. The drum containing the pipe overpack is modeled using the dimensions given in Table 2-1 with a carbon steel wall at the composition given in Table 5-5 and 50% density to account for possible corrosion. The mixture parameters for non-compacted waste moderated by 100% polyethylene representative of fully compacted waste as given in were used to model the fissile mass.

Table D-2. Material Composition for 304 Stainless Steel for Pipe Overpack Structure

Element	MCNP Library Specification	Wt. Fraction	Element	MCNP Library Specification	Wt. Fraction
Density – 7.93 g/cm^3					
^{12}C	6012.00c	0.000790733	^{50}Cr	24050.00c	0.00793
^{13}C	6013.00c	0.00000926744	^{52}Cr	24052.00c	0.159029
^{28}Si	14028.00c	0.00918734	^{53}Cr	24053.00c	0.0183798
^{29}Si	14029.00c	0.000483179	^{54}Cr	24054.00c	0.00466139
^{30}Si	14030.00c	0.000329477	^{54}Fe	26054.00c	0.0385846
P	15031.00c	0.00045	^{56}Fe	26056.00c	0.628101
^{32}S	16032.00c	0.000283955	^{57}Fe	26057.00c	0.0147650
^{33}S	16033.00c	0.00000234437	^{58}Fe	26058.00c	0.00199939
^{34}S	16034.00c	0.000013633	^{58}Ni	28058.00c	0.0638378
^{36}S	16036.00c	0.000000067299	^{60}Ni	28060.00c	0.0254372
Mn	25055.00c	0.02	^{61}Ni	28061.00c	0.00112419
			^{62}Ni	28062.00c	0.00364308
			^{64}Ni	28064.00c	0.000957743

D.2.1 Array Model

The array models for the pipe overpack configurations are similar to those of the direct loaded drums described in Appendix A. The difference is that the fissile material is confined within the pipe component and that the shock-absorbing dunnage of the pipe overpack configuration is included in the drum geometry modeled. The models are based on the 12-inch standard pipe overpack and the cane fiberboard in the drum is modeled as $C_6H_{10}O_5$ at 0.1 g/cm^3, which is less than its nominal density, in order to maximize interaction between containers. The limits determined for this configuration will bound other array configurations of pipe overpacks as the reduced interspersed material increases interaction between the individual units in the array. Figure D-9 and Figure D-10 show the beryllium-reflected models with cylindrical source geometry from pipe overpacks containing less than or equal to 1 wt% beryllium. The 1 wt% beryllium is modeled as 5 kilograms of beryllium split between the top and bottom of the fissile cylinder. In the model for the unlimited beryllium case, the beryllium fills the remainder of the pipe overpack. In both cases, the beryllium is modeled at its theoretical density of 1.85 g/cm^3. For models with the 5 kilograms of beryllium split between top and bottom, the area surrounding it is either modeled as void or filled with polyethylene at 100% of theoretical density (TD).

Both non-compacted and machine-compacted waste are allowed to be shipped to WIPP in the TRUPACT-II (DOE-CBFO 2020b). Although fully compacted waste is not anticipated to be shipped in the POC, polyethylene is modeled at up to its theoretical density as a bounding value for machine-compacted waste, both intermixed within the fissile waste region and as packaging surrounding the fissile region. The H/Pu ratio in the fissile region, the polyethylene pipe fill density, and the configuration of the 5 kilograms of beryllium are varied to determine the most reactive condition. Each overpack is modeled with 200 FGE and 5 kilograms of beryllium or 140 FGE with unlimited beryllium (filling the remainder of the pipe), consistent with the FGE limits for transportation. The fissile region for all models consists of ^{239}Pu mixed with 100% dense polyethylene. Table D-3 and Figure D-11 give the results of a parametric study versus H/Pu ratio. All results remain below the MCNP6.2 USL of 0.9659 with the most reactive model being that of the POC filled with Be surrounding the 140 FGE region, followed by the solid split 5 kilograms of beryllium and polyethelyene fill surrounding the 200 FGE region. The density of the polyethylene fill was further varied from 0 to 100% TD. The results in Table D-4 confirm that the polyethylene fill at 100% TD is the most reactive.

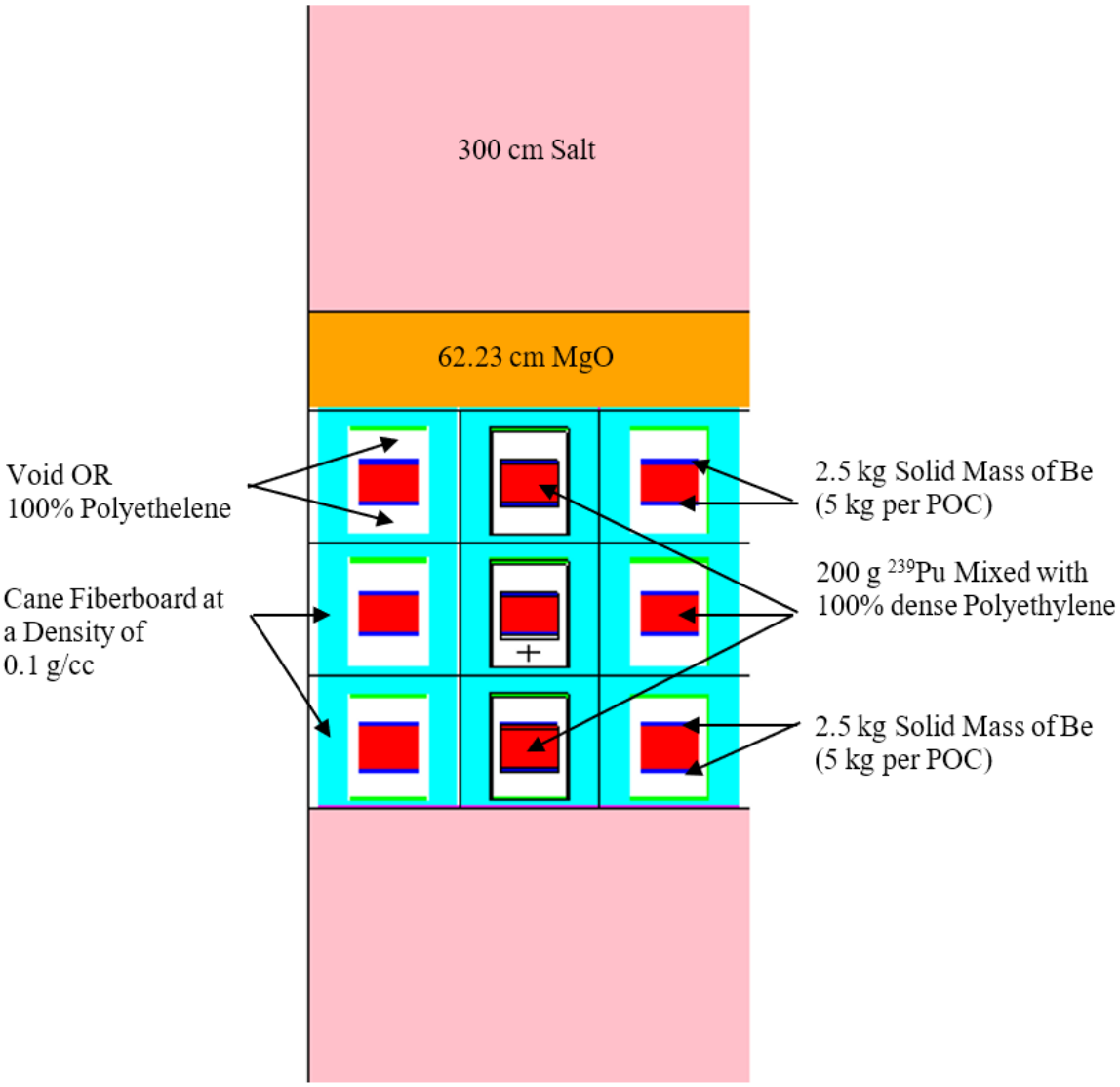

Figure D-9. Base Array Geometry for Pipe Overpacks Containing Less Than or Equal to 1 Weight Percent Beryllium

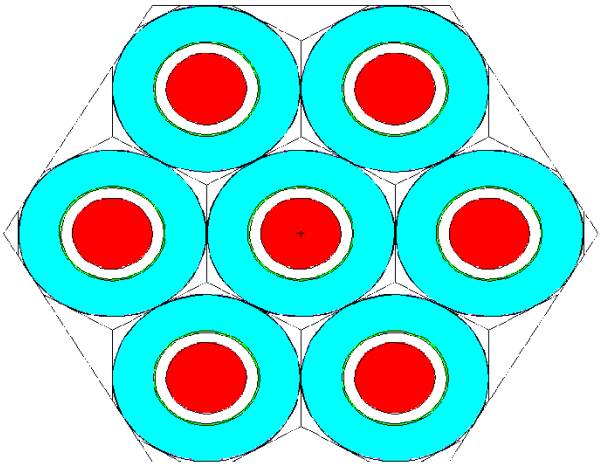

Figure D-10. Cross Section of Seven-pack of 12-inch Pipe Overpack Drums Containing Less Than or Equal to 1 Weight Percent Beryllium

Table D-3. Pipe Overpack Array Results

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
200 FGE and 5 kg Solid Beryllium in Voided Pipe Overpack				
500	0.77625	0.00026	0.77677	pa20010p
600	0.80795	0.00028	0.80851	pa20012p
700	0.82949	0.00026	0.83001	pa20014p
800	0.84462	0.00026	0.84514	pa20016p
900	0.85434	0.00027	0.85488	pa20018p
1000	0.86076	0.00025	0.86126	pa20020p
1100	0.86345	0.00026	0.86397	pa20022p
1200	0.86458	0.00024	0.86506	pa20024p
1300	0.86306	0.00022	0.86350	pa20026p
1400	0.86063	0.00021	0.86105	pa20028p
1500	0.85733	0.00022	0.85777	pa20030p
200 FGE and 5 kg Beryllium Dispersed in Poly filled Pipe Overpack				
500	0.83813	0.00012	0.83837	pa20010pd
600	0.85421	0.00028	0.85477	pa20012pd
700	0.86506	0.00026	0.86558	pa20014pd
800	0.87066	0.00025	0.87116	pa20016pd
900	0.87346	0.00025	0.87396	pa20018pd
1000	0.87270	0.00025	0.87320	pa20020pd
1100	0.87126	0.00024	0.87174	pa20022pd
1200	0.86814	0.00024	0.86862	pa20024pd
1300	0.86395	0.00023	0.86441	pa20026pd
200 FGE and 5 kg Solid Beryllium in Poly filled Pipe Overpack				
500	0.86210	0.00026	0.86262	pa20010pf
600	0.87827	0.00028	0.87883	pa20012pf
700	0.88779	0.00027	0.88833	pa20014pf
800	0.89243	0.00024	0.89291	pa20016pf
900	0.89419	0.00026	0.89471	pa20018pf
1000	0.89260	0.00025	0.89310	pa20020pf
1100	0.88947	0.00024	0.88995	pa20022pf

Table D-3. Pipe Overpack Array Results

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
1200	0.88525	0.00023	0.88571	pa20024pf
1300	0.88040	0.00023	0.88086	pa20026pf
1400	0.87387	0.00023	0.87433	pa20028pf
1500	0.86749	0.00022	0.86793	pa20030pf
140 FGE in Beryllium (unlimited) filled Pipe Overpack				
500	0.91332	0.00028	0.91388	pa14010p
600	0.92509	0.00028	0.92565	pa14012p
700	0.92982	0.00027	0.93036	pa14014p
800	0.93000	0.00025	0.93050	pa14016p
900	0.92764	0.00025	0.92814	pa14018p
1000	0.92327	0.00024	0.92375	pa14020p
1100	0.91637	0.00023	0.91683	pa14022p

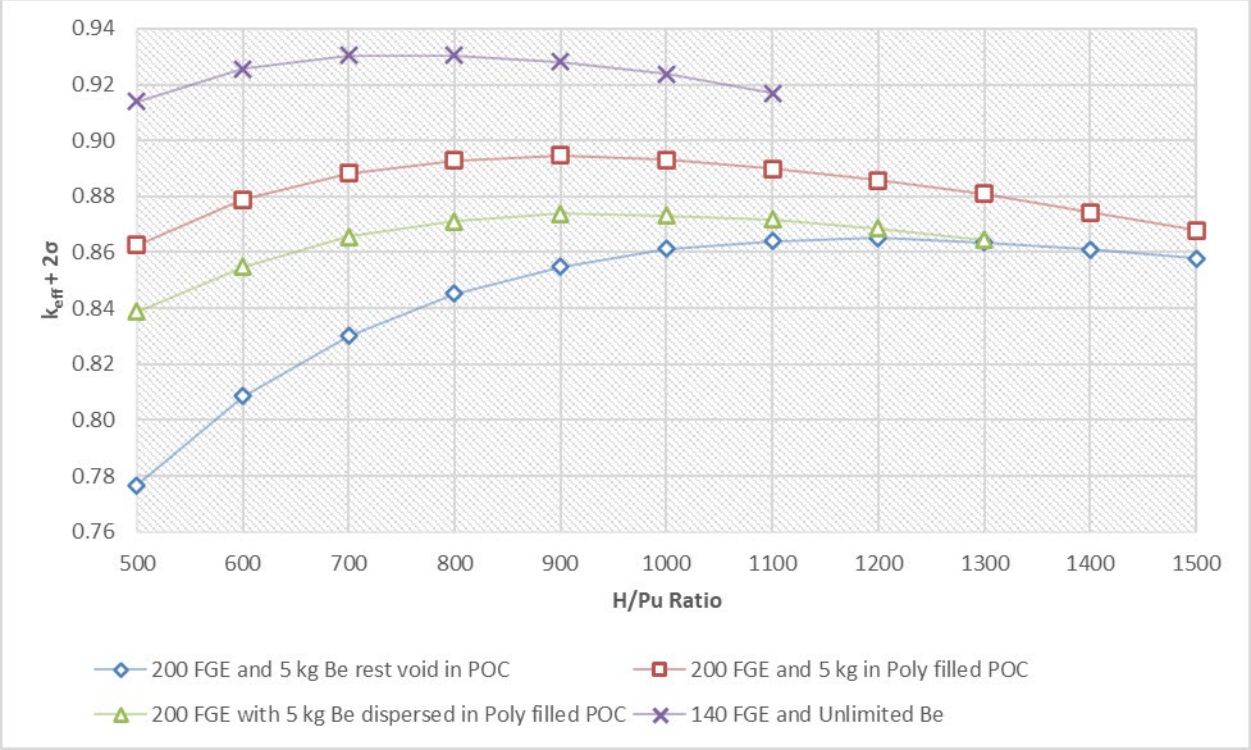

Figure D-11. Pipe Overpack Array Reactivity

Table D-4. k_{eff} vs. Polyethylene Fill Density for H/Pu = 900

H/Pu Ratio	Polyethylene Density (% of TD)	$k_{eff} + 2\sigma$	Filename
200 FGE and 5 kg Solid Beryllium in varied density Polyethylene filled Pipe Overpack			
900	0.00	0.85488	pa20018pv0
900	0.10	0.84467	pa20018pv10
900	0.25	0.85130	pa20018pv25
900	0.50	0.86958	pa20018pv50
900	0.75	0.88414	pa20018pv75
900	1.00	0.89471	pa20018pv100

D.2.2 Two-Container Model

A two-container model is developed to evaluate the reactivity of the pipe overpacks with maximum interaction between the fissile material in the two containers and maximum reflection. Whereas the fissile material is centered in each container in the array model, the two-container model considers a localized, well reflected, worst-case fissile placement. The geometry includes a standard (unshielded) 12-inch pipe component surrounded by cellulose ($C_6H_{10}O_5$) used to represent the cane fiberboard. The fissile source is modeled in a cylindrical geometry with an H/D ratio of 1. The fissile material in the lower overpack is modeled at the top of the pipe component while the fissile material in the upper overpack is modeled at the bottom of the pipe component. The position of the pipe component within the overpack is unchanged because it is fixed by the dunnage. Cellulose is modeled at its nominal density of 0.224 g/cm^3 to provide maximum reflection. Space within the pipe component not occupied by the fissile material is filled with 100% dense polyethylene for the 1 wt% beryllium case or filled with beryllium for the unlimited beryllium case. Figure D-12 shows an MCNP plot of the two-container model with a 300 cm concrete reflector. The two-container results in Appendix A indicate that MgO and salt reflectors yield a similar eigenvalue to a concrete reflector.

The computational analysis evaluated FGE values in the pipe overpacks at 200 grams of ^{239}Pu if the beryllium is limited to a maximum of 1 wt% (5 kg) or 140 grams of ^{239}Pu if the beryllium content is not restricted. The results as a function of H/Pu ratio are tabulated in Table D-5 and shown in Figure D-13, and are all well below the USL with the highest $k_{eff} + 2\sigma$ value being less than 0.88.

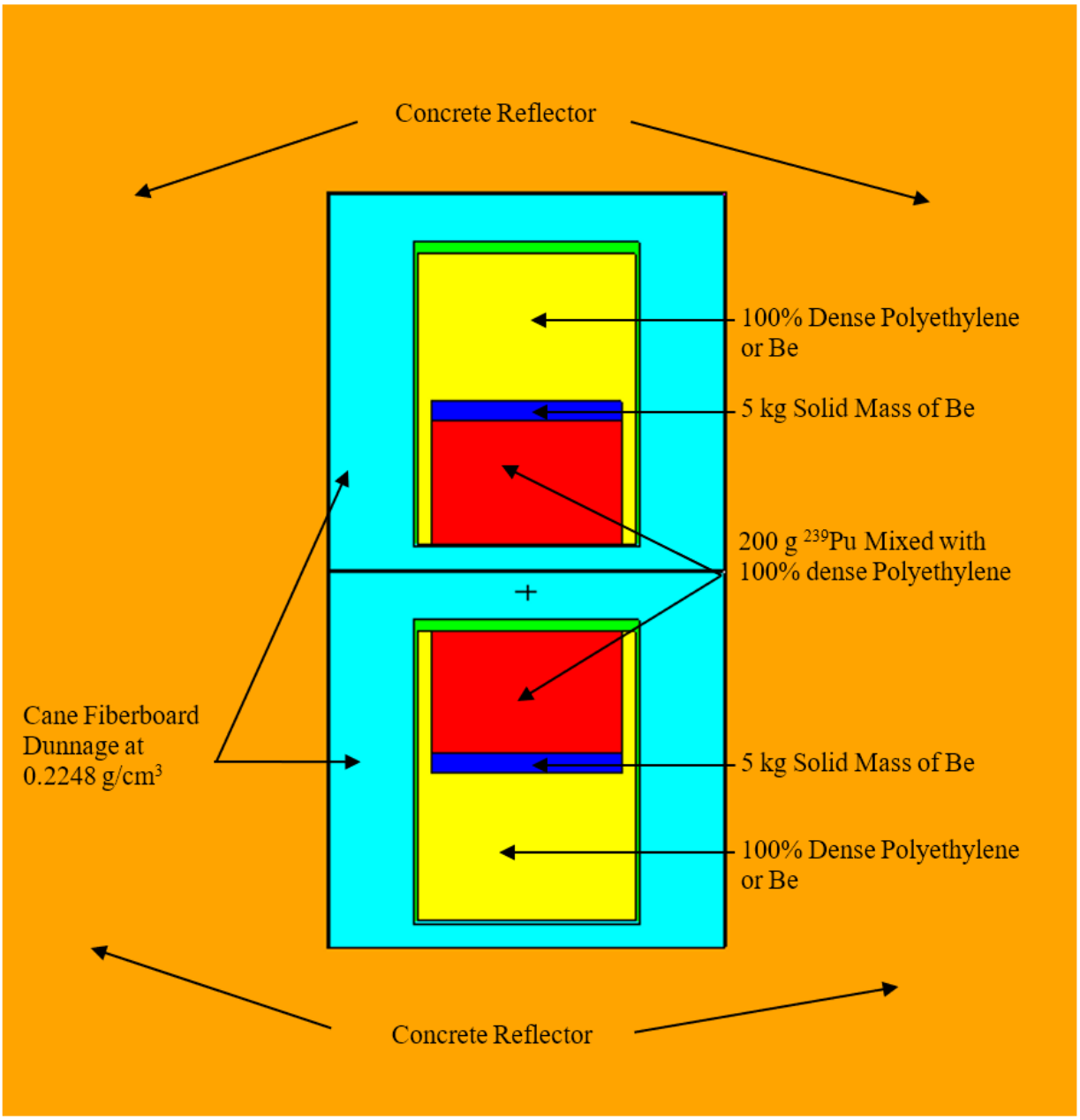

Figure D-12. MCNP Plot of 2-Drum 12-inch Standard Pipe Overpack Model with Less Than or Equal to 1 Weight Percent Beryllium and Concrete Reflection

Table D-5. MCNP Results for 2 Pipe Overpack Drum Concrete Reflected

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
200 g ^{239}Pu and 5 kg Beryllium				
500	0.73484	0.00028	0.73540	pd20010p
600	0.76253	0.00027	0.76307	pd20012p
700	0.77655	0.00027	0.77709	pd20014p
800	0.79481	0.00027	0.79535	pd20016p
900	0.80281	0.00027	0.80335	pd20018p
1000	0.80776	0.00026	0.80828	pd20020p
1100	0.81007	0.00023	0.81053	pd20022p
1200	0.81086	0.00025	0.81136	pd20024p
1300	0.80904	0.00024	0.80952	pd20026p
1400	0.80658	0.00025	0.80708	pd20028p
140 g ^{239}Pu and Unlimited Beryllium				
500	0.84479	0.00012	0.84503	pd14010p
600	0.85952	0.00028	0.86008	pd14012p
700	0.86723	0.00027	0.86777	pd14014p
800	0.86977	0.00026	0.87029	pd14016p
900	0.86916	0.00026	0.86968	pd14018p
1000	0.86572	0.00025	0.86622	pd14020p
1100	0.86090	0.00024	0.86138	pd14022p

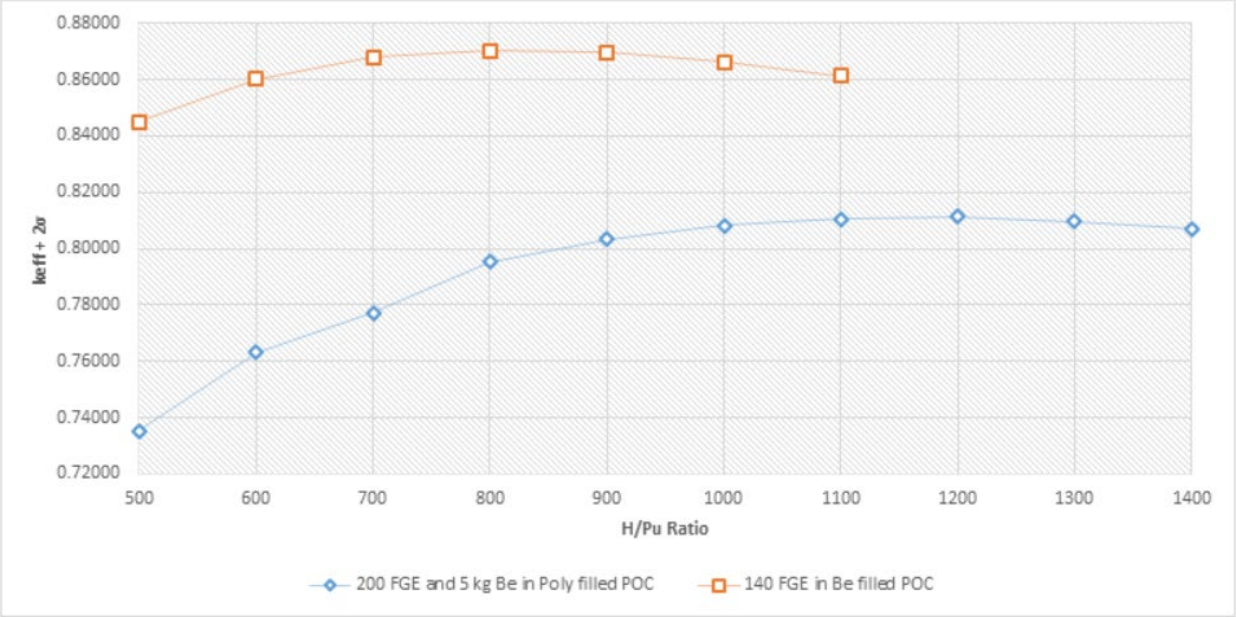

Figure D-13. Reactivity of the 55-gallon Pipe Overpack 2-Drum Model with Concrete Reflection

D.3 Pipe Overpack Contingency Models

To ensure a conservative bound on the analyses, a few contingency conditions were evaluated for the underground storage array of the 12-inch pipe overpacks. Specifically, an overbatching event and an overstacking event were considered. Since the two-container models are sufficiently conservative to bound any contingency of more realistic or expected conditions related to the interaction between small numbers of containers, only array configurations with centrally located fissile material will be considered. These upset condition models are based on the most reactive array models from Section D.2.1, namely the 140 FGE model with beryllium filling the remainder of the POC and the 200 FGE model with the 5 kilograms of Be split on either side of the fissile region followed by100% dense polyethylene filling the POC.

D.3.1 Pipe Overpack Array Overstack Model

Considering the overstacking events, it is important to note that although WIPP panel heights were designed to accommodate three layers of waste containers, ground control safety constraints have resulted in areas of the disposal rooms being mined to a height greater than 13 feet. As a result, it is possible to stack greater than three tiers high including the magnesium oxide (MgO). A contingency calculation was performed for a four-tier-high stack for both less than 1% beryllium and greater than 1% beryllium reflection states. Polyethylene is intermixed with the fissile mass in accordance to the H/Pu ratio and the area surrounding the fissile region is filled with polyethylene in pipe overpacks containing less than 1% beryllium in order to maximize the interaction between fissile masses in the array. The fissile loadings used in the computational analysis were in compliance to the maximum loading allowed by the TRUPACT-II SAR: 200 grams of ^{239}Pu with a maximum 5 kilograms of beryllium or 140 grams of ^{239}Pu with no limits on beryllium. The lateral boundaries again used reflection symmetry to simulate an infinite array and the vertical boundary were reflected with 300 centimeters of salt with an MgO layer modeled between the upper tier of pipe overpacks and the salt boundary. The computational results for a four-tier-high stack of seven-packs yielded a system eigenvalue less than 0.94, as summarized in Table D-6 and shown in Figure D-14.

Table D-6. MCNP Results for an Overstacking Contingency

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
200 g ^{239}Pu and 5 kg Beryllium Array Stacked Four Tiers High				
500	0.86221	0.00027	0.86275	pa20090pf
600	0.87866	0.00027	0.87920	pa20092pf
700	0.88765	0.00026	0.88817	pa20094pf
800	0.89283	0.00026	0.89335	pa20096pf
900	0.89430	0.00025	0.89480	pa20098pf
1000	0.89302	0.00024	0.89350	pa20100pf
1100	0.88961	0.00023	0.89007	pa20102pf
1200	0.88576	0.00022	0.88620	pa20104pf
1300	0.88057	0.00022	0.88101	pa20106pf
1400	0.87422	0.00022	0.87466	pa20108pf
1500	0.86783	0.00022	0.86827	pa20110pf

Table D-6. MCNP Results for an Overstacking Contingency

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
140 g ^{239}Pu and Unlimited Beryllium Array Stacked Four Tiers High				
500	0.91392	0.00027	0.91446	pa14090pb
600	0.92560	0.00028	0.92616	pa14092pb
700	0.93109	0.00027	0.93163	pa14094pb
800	0.93152	0.00026	0.93204	pa14096pb
900	0.92883	0.00025	0.92933	pa14098pb
1000	0.92415	0.00024	0.92463	pa14100pb
1100	0.91748	0.00024	0.91796	pa14102pb

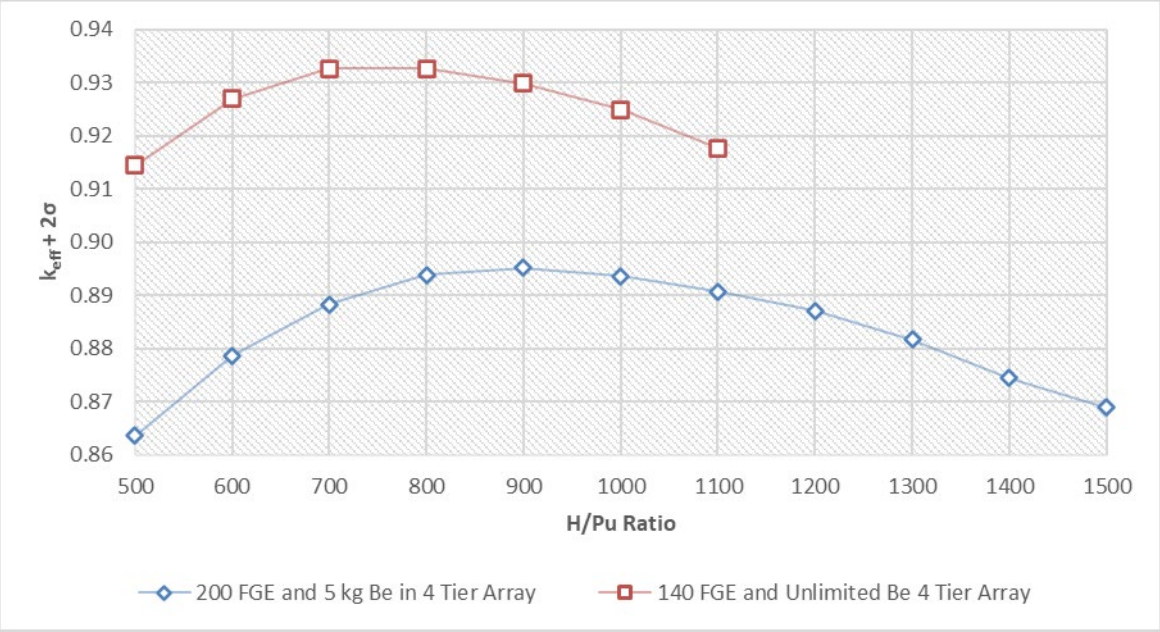

Figure D-14. Reactivity of a Four-Tier Array of 12-inch Pipe Overpacks

D.3.2 Pipe Overpack Array Overbatch Model

An overbatch scenario in the pipe overpacks was evaluated with one POC in the stack of three 7-packs overbatched by 50%. Because the sides of this model are mirrored, this is equivalent to an overbatch in one out of every 21 POCs in the underground array. As shown in Table D-7 and Figure D-15 MCNP calculations determined that pipe overpacks limited to 200 grams of ^{239}Pu with a maximum of 5 kilograms of beryllium and 86% dense polyethylene (limit of 33.9 kilograms polyethylene or plastic) are subcritical (i.e., below the USL of 0.9659). Although a polyethylene mass of 33.9 kilograms is not expected to be loaded into a POC, this limit is carried forward for machine-compacted waste. The 86% packing fraction exceeds the 25% polyethylene modeled in non-compacted waste, as discussed in Appendix A, and thus no limitation on polyethylene is required for non-compacted waste. The unlimited beryllium loading of 140 grams of ^{239}Pu does not allow for machine-compacted waste in this upset condition. As such, the composition for non-compacted waste is analyzed as waste moderated by a 25% polyethylene and 75% water mixture as given in Table 5-3. With these limitation on polyethylene moderation, all overbatch models remained below the USL of 0.9659 for these conditions. The limitations

are carried forward into the underground repository limits as summarized in Section D.4 below and listed in Section 9.2 of the NCSE.

Table D-7. Overbatched Pipe Overpack Array Results

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
200 FGE and 5 kg Beryllium in 100% Dense Poly filled Pipe Overpack with One Overbatched Container at 300 FGE Located on the Center Tier Edge				
500	0.95113	0.00027	0.95167	pa20010pc
600	0.96416	0.00027	0.96470	pa20012pc
700	0.97009	0.00027	0.97063	pa20014pc
800	0.97076	0.00025	0.97126	pa20016pc
900	0.96970	0.00025	0.97020	pa20018pc
1000	0.96471	0.00024	0.96519	pa20020pc
1100	0.95789	0.00024	0.95837	pa20022pc
1200	0.95075	0.00023	0.95121	pa20024pc
1300	0.94269	0.00023	0.94315	pa20026pc
1400	0.93209	0.00024	0.93257	pa20028pc
200 FGE and 5 kg Beryllium in 86% Dense Poly filled Pipe Overpack with One Overbatched Container at 300 FGE Located on the Center Tier Edge				
500	0.94169	0.00029	0.94227	pa20010pm
600	0.95540	0.00028	0.95596	pa20012pm
700	0.96157	0.00027	0.96211	pa20014pm
800	0.96378	0.00025	0.96428	pa20016pm
900	0.96201	0.00026	0.96253	pa20018pm
1000	0.95759	0.00024	0.95807	pa20020pm
1100	0.95162	0.00024	0.95210	pa20022pm
1200	0.94380	0.00024	0.94428	pa20024pm
1300	0.93720	0.00024	0.93768	pa20026pm
1400	0.92694	0.00023	0.92740	pa20028pm
140 FGE and Unlimited Beryllium/Pipe Overpack with One Overbatched Container at 210 FGE Located on the Center Tier Edge with 25% Poly and 75% Water				
500	0.92934	0.00029	0.92992	pa14010pn
600	0.93408	0.00027	0.93462	pa14012pn
700	0.93429	0.00027	0.93483	pa14014pn
800	0.93009	0.00026	0.93061	pa14016pn
900	0.92431	0.00026	0.92483	pa14018pn
1000	0.91598	0.00025	0.91648	pa14020pn
1100	0.90668	0.00023	0.90714	pa14022pn

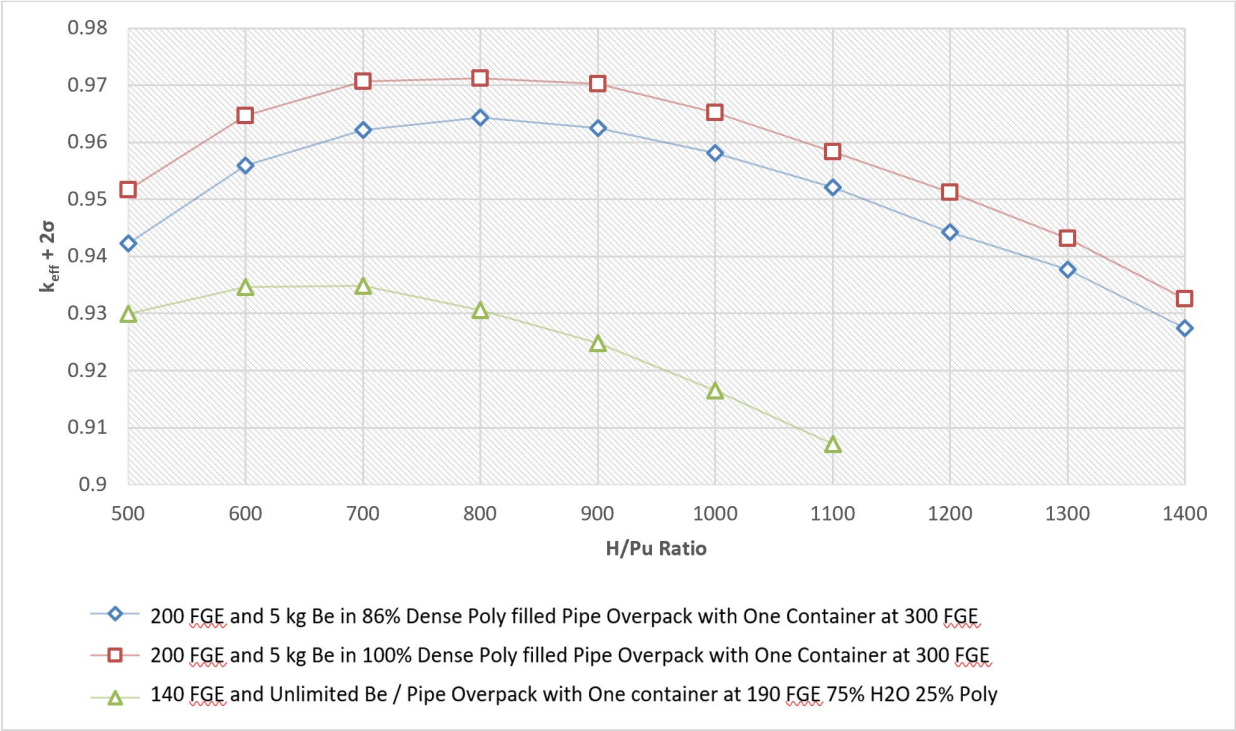

Figure D-15. Pipe Overpack Array Reactivity

D.4 Conclusions

This appendix demonstrates that pipe overpack drums will remain subcritical in the two-container configuration as well in the underground repository array with one of the following maximum limits:

- 200 FGE per pipe component and maximum 5 kilograms of beryllium per drum for non-compacted waste.
- 200 FGE per pipe component and maximum 5 kilograms of beryllium per drum and maximum 33.9 kilograms of polyethylene/plastics for machine-compacted waste.
- 140 FGE per pipe component with unlimited special reflector materials for non-compacted waste.

Note: compacted waste with > 5 kilograms of beryllium is not allowed in a POC.

D.5 References

ASTM A76/A276M-17, *Standard Specification for Stainless Steel Bars and Shapes*, ASTM International, West Conshohocken, PA.

ASTM C208-95(2001). *Standard Specification for Cellulosic Fiber Insulating Board*, American Society for Testing and Materials, West Conshohocken, PA.

DOE-CBFO, 2020a. *Contact-Handled Transuranic Waste Authorized Methods for Payload Control (CH-TRAMPAC)*, Revision 5, October 2020, U.S. Department of Energy, Carlsbad Field Office, Carlsbad, NM.

DOE-CBFO, 2020b. *TRUPACT-II Safety Analysis Report*, Revision 24, October 2020, U.S. Department of Energy, Carlsbad Field Office, Carlsbad, NM.

Packaging Technology, Inc., May 2004, "Pipe Overpack Criticality Analysis for the TRUPACT-II Package," ED-076 Rev. 3, Packaging Technology, Inc., Tacoma, Washington.

D.6 Sample MCNP6.2 Input File Listings for Appendix D

D.6.1 MCNP Input File (pd20024p) Listing for Two-Container Concrete Reflected Case with 5 kg Beryllium:

```
Title
CCCC
```

```
                                FILL=1        IMP:N=1
C
C    CELL CARDS FOR A 300 CM CONCRETE REFLECTOR AROUND THE TWO DRUMS WITH
C    MIRROR BOUNDARY CONDITIONS ON ALL SIX SIDES, FLOOR AND CEILING.
C
60   7   -2.3500   -300 301 -302 303 -304 305 -306 307        &
               (200:-201:202:-203:204:-205:206:-207)      IMP:N=1
C
C    CELL CARDS FOR EVERYTHING OUTSIDE THE COMPUTATIONAL SPACE.
C
100  0            (300:-301:302:-303:304:-305:306:-307)      IMP:N=0

C
C    SURFACE CARDS FOR THE LOWER 55 GALLON DRUM IN THE TWO-DRUM MODEL.
C
1       CZ   10.67287
2       PZ   71.36841
3       PZ   50.02267
4       CZ   10.67287
5       PZ   71.36841
6       PZ   42.47025
7       CZ   15.69974
8       PZ   71.38841
9       PZ    6.72541
10      CZ   16.25600
11      PZ   73.65441
12      PZ    6.09041
13      CZ   28.57500
14      PZ   84.57641
15      PZ    0.12141
16      CZ   28.69641
17      PZ   84.69782
18      PZ    0.00000
19      CZ   28.69641
20      PZ   84.69782
21      PZ    0.00000
C
C    SURFACE CARDS FOR THE UPPER 55 GALLON DRUM IN THE TWO-DRUM MODEL.
C
30  1   CZ   10.67287
31  1   PZ   28.07115
32  1   PZ    6.72541
33  1   CZ   10.67287
34  1   PZ   35.62357
35  1   PZ    6.09041
36  1   CZ   15.69974
37  1   PZ   71.36841
38  1   PZ    6.09041
39  1   CZ   16.25600
40  1   PZ   73.65441
41  1   PZ    6.09041
42  1   CZ   28.57500
43  1   PZ   84.57641
44  1   PZ    0.12141
45  1   CZ   28.69641
46  1   PZ   84.69782
47  1   PZ    0.00000
48  1   CZ   28.69641
49  1   PZ   84.69782
50  1   PZ    0.00000
C
C    SURFACE CARDS FOR A BOUNDARY AROUND THE TWO-DRUM MODEL.
C
100     CZ   28.69641
101     PZ  169.39564
102     PZ    0.00000
C
C    SURFACE CARDS FOR A HEXAPRISM LATTICE UNIT CONTAINING THE TWO DRUMS.
C
```

```
200     PX   28.69641
201     PX  -28.69641
202     P  1  1.73205  0   57.39282
203     P  1  1.73205  0  -57.39282
204     P -1  1.73205  0   57.39282
205     P -1  1.73205  0  -57.39282
206     PZ  169.39564
207     PZ    0.00000
C
C    SURFACE CARDS FOR A 300 CM CONCRETE REFLECTOR AROUND THE TWO DRUMS
C    WITH MIRROR BOUNDARY CONDITIONS ON ALL SIX SIDES, FLOOR AND CEILING.
C
*300     PX  328.69641
*301     PX -328.69641
*302     P  1  1.73205  0  657.39282
*303     P  1  1.73205  0 -657.39282
*304     P -1  1.73205  0  657.39282
*305     P -1  1.73205  0 -657.39282
*306     PZ  469.39564
*307     PZ -300.00000

C
C    MODE CARD.
C
MODE N
C
C    TRANSFORMATION CARDS FOR THE TWO-DRUM MODEL.
C
TR1   0.00000     0.00000    84.69782
C
C    MATERIAL CARDS
C
C    PU-CH2 (LOWER AND UPPER DRUMS)
C
M1     1001.00C -0.139750  6012.00C -0.822986  6013.00C -0.009645
       94239.00C -0.027619
MT1    h-poly.40t
C
C    BE REFLECTOR (LOWER AND UPPER DRUMS)
C
M2     4009.00C -1.000000
MT2    be-met.40t
C
C    POLYETHYLENE
C
M3     1001.00C -0.143718  6012.00C -0.846362  6013.00C -0.00991942
MT3    h-poly.40T
C
C    304 STAINLESS STEEL
C
M4     26054.00C -0.038585  26056.00C -6.2810-01 26057.00C -1.4765-02
       26058.00C -1.9994-03 24050.00C -7.9300-03 24052.00C -1.5903-01
       24053.00C -1.8380-02 24054.00C -4.6614-03 28058.00C -6.3838-02
       28060.00C -2.5437-02 28061.00C -1.1242-03 28062.00C -3.6431-03
       28064.00C -9.5774-04 25055.00C -0.0200000  6012.00C -7.9073-04
      6013.00C -9.2674-06 15031.00C -0.0004500 14028.00C -9.18734-03
      14029.00C -4.83179-04 14030.00C -3.29477-04 16032.00c -2.8396-04
      16033.00C -2.3444-06 16034.00C -1.3633-05  16036.00C -6.7299-08
C
C    CANE FIBERBOARD DUNNAGE (LOWER AND UPPER DRUMS)
C
M5     6012.00C  5.9358  6013.00C .06420  1001.00C 10  8016.00C  5
C
C    CARBON STEEL DRUM.
C
M6     6012.00C -0.001483  6013.00C -0.000017  25055.00C -0.006000
       15031.00C -0.000350  16032.00C -3.7861-04  16033.00C -3.1258-06
       16034.00C -1.8178-05  16036.00C -8.9732-08  26054.00C -5.5990-02
        26056.00C -9.1143-01  26057.00C -2.1425-02  26058.00C -2.9013-03
```

```
C
C    CONCRETE
C
M7    1001.00C -0.00560000  8016.00C -0.4981000  11023.00C -0.0171000
      12024.00C -2.02670-03  12025.00C  -2.67283-04  12026.00C  -3.06018-04
      13027.00C -0.0457000  14028.00C -2.89493-01  14029.00C -1.52250-02
      14030.00C -1.03818-02  16032.00C -1.23047-03 16033.00C -1.01590-05
      16034.00C -5.90776-05 16036.00C -2.91630-07  19039.00C -1.78439-02
      19040.00C -2.29614-06  19041.00C -1.35379-03  20040.00C -8.01326-02
      20042.00C -5.61531-04  20043.00C -1.19959-04  20044.00C -1.89660-03
      20046.00C -3.80214-06  20048.00C -1.85482-04  26054.00C -7.0005-04
      26056.00C -0.011396  26057.00C -2.6789-04  26058.00C -3.6276-05
MT7   h-h2o.40t
C
C    SOURCE CARDS
C
KCODE 20000 0.9 150 650
KSRC  0.0  0.0  65  0.0 0.0 100
PRINT
C
C    PRINT TO MCTAL FILE
C
PRDMP 2j 1
```

D.6.2 MCNP Input File (pa20016pm) Modified overbatch case with 86% dense polyethylene with one container at 300 FGE:

```
Title
C CCCC
```

```
12    4   -7.93000   -10  -11  12  #9 #10 #11                    U=3  IMP:N=1
13    5   -0.10000   -13  -14  15  (10:11:-12)                   U=3  IMP:N=1
14    6   -3.93000   -16  -17  18  (13:14:-15)                   U=3  IMP:N=1
15    0               -19  -20  21  #9 #10 #11 #12 #13 #14  U=3  IMP:N=1
16    0                    (19:20:-21)                      U=3  IMP:N=1
C
C    CELL CARDS FOR THE HEXAGONAL 7-PACK STACK.
C
20    0            -31 30 -32 35 -33 34 -37 36 LAT=2 U=2      IMP:N=1
                  FILL=-3:3 -3:3 0:2
                  2 16R
                     1 1   2 2 2 2
                    1 1 1  2 2 2 2
                     1 1   2 16R
                  2 16R
                     1 1   2 2 2 2
                    1 1 3  2 2 2 2
                     1 1   2 16R
                  2 16R
                     1 1   2 2 2 2
                    1 1 1  2 2 2 2
                     1 1   2 16R
21    0            -61 60 -62 65 -63 64 -67 66 FILL=2        IMP:N=1
C
C    CELL CARDS FOR THE MGO AND SALT LAYERS.
C
22    8   -2.165     (53:-66) -61 60 -62 65 -63 64 50 -52      IMP:N=1
23    7   -1.45      -61 60 -62 65 -63 64 67 -53               IMP:N=1
C
C    CELL CARDS FOR THE REST OF THE UNIVERSE.
C
24    0            -50:52:61:-60:62:-65:63:-64               IMP:N=0

C
C    SURFACE CARDS FOR THE 55 GALLON DRUM WITH 12-INCH PIPE OVERPACK.
C
1      CZ    9.32559
2      PZ   47.73750
3      PZ   29.08632
4      CZ    9.32559
5      PZ   52.68363
6      PZ   24.14019
7      CZ   15.69974
8      PZ   70.73341
9      PZ    6.09041
10     CZ   16.25600
11     PZ   73.01941
12     PZ    5.45541
13     CZ   28.57500
14     PZ   84.57641
15     PZ    0.12141
16     CZ   28.69641
17     PZ   84.69782
18     PZ    0.00000
19     CZ   28.69641
20     PZ   84.69782
21     PZ    0.00000
C
C    SURFACE CARDS FOR 300 FGE MATERIAL AND BE
C
22     RCC 0 0  27.73678 0 0  21.35027   10.67513
23     RCC 0 0  23.96217 0 0  28.89948   10.67513
C
C    SURFACE CARDS FOR THE HEXAGONAL 7-PACK.
C
30   PX -28.75
31   PX  28.75
32   P   1    1.7321    0    57.5
33   P  -1    1.7321    0    57.5
```

```
34   P  -1   1.7321   0   -57.5
35   P   1   1.7321   0   -57.5
36   PZ  0.0
37   PZ  84.69782
C
C    SURFACE CARDS FOR THE MGO AND SALT LAYERS.
C
50   PZ -300.00
52   PZ  616.321
53   PZ  316.321
C
C    SURFACE CARDS FOR THE 7-PACK STACK INFINITE ARRAY.
C
*60   PY -78.5
*61   PY  78.5
*62   P   1.7321   1    0   157
*63   P   1.7321  -1    0   157
*64   P   1.7321  -1    0  -157
*65   P   1.7321   1    0  -157
66    PZ -0.0
67    PZ  254.09346

C
C    MODE CARD.
C
MODE N
C
C    MATERIAL CARDS
C
C    PU-CH2 (LOWER AND UPPER DRUMS)
C
M1    1001.00C -0.137845  6012.00C -8.11775-01  6013.00C -9.514-03
       94239.00C -0.040866
MT1    h-poly.40T
C
C    BE REFLECTOR (LOWER AND UPPER DRUMS)
C
M2    4009.00C -1.000000
MT2    be-met.40t
C
C    POLYETHYLENE
C
M3    1001.00C -0.143718  6012.00C -0.846362  6013.00C -0.00991942
MT3    h-poly.40T
C
C    304 STAINLESS STEEL
C
M4    26054.00C -0.038585  26056.00C -6.2810-01 26057.00C -1.4765-02
       26058.00C -1.9994-03 24050.00C -7.9300-03 24052.00C -1.5903-01
       24053.00C -1.8380-02 24054.00C -4.6614-03 28058.00C -6.3838-02
       28060.00C -2.5437-02 28061.00C -1.1242-03 28062.00C -3.6431-03
       28064.00C -9.5774-04 25055.00C -0.0200000  6012.00C -7.9073-04
       6013.00C -9.2674-06 15031.00C -0.0004500 14028.00C -9.18734-03
       14029.00C -4.83179-04 14030.00C -3.29477-04 16032.00c -2.8396-04
       16033.00C -2.3444-06 16034.00C -1.3633-05  16036.00C -6.7299-08
C
C    CANE FIBERBOARD DUNNAGE (LOWER AND UPPER DRUMS)
C
M5    6012.00C  5.9358  6013.00C .06420  1001.00C 10  8016.00C  5
C
C    CARBON STEEL DRUM.
C
M6     6012.00C -0.001483  6013.00C -0.000017  25055.00C -0.006000
       15031.00C -0.000350  16032.00C -3.7861-04  16033.00C -3.1258-06
       16034.00C -1.8178-05  16036.00C -8.9732-08  26054.00C -5.5990-02
        26056.00C -9.1143-01  26057.00C -2.1425-02  26058.00C -2.9013-03
C
C
C    MGO LAYER.
```

```
C
M7    12024.00C 0.39495  12025.00C 0.05 12026.00C 0.05505 8016.00C 0.5
C
C    SALT REFLECTOR.
C
M8    11023.00C 0.5  17035.00C 0.3789  17037.00C 0.1211
C
C    OVERBATCH PU-CH2
C
M9     1001.00C -0.137845  6012.00C -8.11775-01  6013.00C -9.514-03
        94239.00C -0.040866
MT9     h-poly.40t
C
C    SOURCE CARDS.
C
KCODE 20000 .965 200 700
KSRC   0 0 38  28 49 38  -28 -50 38
         -57 0 38  57 0 38  -28 50 38
          0 0 122  28 49 122  -28 -50 122
         -57 0 122  57 0 122  -28 50 122
          0 0 207  28 49 207  -28 -50 207
         -57 0 207  57 0 207  -28 50 207
         -28 50 38  -28 50 122  -28 -50 207
          47 0 110  67 0 135  57 10 122
           57 -10 122
PRINT
C
C    PRINT TO MCTAL FILE
C
PRDMP 2j 1
```

D.6.3 MCNP Input File (pa14014pn) Overbatch case for containers with 140 FGE mixed with 75% water and 25% Polyethylene and unlimited Beryllium with one container at 190 FGE:

```
 Title
C CCCC
```

```
6    6   -3.93000   -16  -17  18  (13:14:-15)              U=1  IMP:N=1
7    0                -19  -20  21  #1 #2 #3 #4 #5 #6      U=1  IMP:N=1
8    0                     (19:20:-21)                     U=1  IMP:N=1
C
C    CELL CARDS FOR THE 55 GALLON DRUM WITH 12-INCH PIPE OVERPACK 210.
C
9    9   -1.018385    -22                                  U=3  IMP:N=1
10   2   -1.85000     -4   -5   6  22                      U=3  IMP:N=1
11   0                -7   -8   9  (4:5:-6)                U=3  IMP:N=1
12   4   -7.93000   -10  -11  12  #9 #10 #11               U=3  IMP:N=1
13   5   -0.10000   -13  -14  15  (10:11:-12)              U=3  IMP:N=1
14   6   -3.93000   -16  -17  18  (13:14:-15)              U=3  IMP:N=1
15   0                -19  -20  21  #9 #10 #11 #12 #13 #14  U=3  IMP:N=1
16   0                     (19:20:-21)                     U=3  IMP:N=1
C
C    CELL CARDS FOR THE HEXAGONAL 7-PACK STACK.
C
20   0            -31 30 -32 35 -33 34 -37 36 LAT=2 U=2     IMP:N=1
                  FILL=-3:3 -3:3 0:2
                  2 16R
                     1 1   2 2 2 2
                    1 1 1  2 2 2 2
                     1 1   2 16R
                  2 16R
                     1 1   2 2 2 2
                    1 1 3  2 2 2 2
                     1 1   2 16R
                  2 16R
                     1 1   2 2 2 2
                    1 1 1  2 2 2 2
                     1 1   2 16R
21   0            -61 60 -62 65 -63 64 -67 66 FILL=2        IMP:N=1
C
C    CELL CARDS FOR THE MGO AND SALT LAYERS.
C
22   8   -2.165     (53:-66) -61 60 -62 65 -63 64 50 -52     IMP:N=1
23   7   -1.45      -61 60 -62 65 -63 64 67 -53              IMP:N=1
C
C    CELL CARDS FOR THE REST OF THE UNIVERSE.
C
24   0            -50:52:61:-60:62:-65:63:-64              IMP:N=0

C
C    SURFACE CARDS FOR THE 55 GALLON DRUM WITH 12-INCH PIPE OVERPACK.
C
1      CZ   8.25550
2      PZ   46.66741
3      PZ   30.15641
4      CZ   15.69974
5      PZ   70.73341
6      PZ    6.09041
7      CZ   15.69974
8      PZ   70.73341
9      PZ    6.09041
10     CZ   16.25600
11     PZ   73.01941
12     PZ    5.45541
13     CZ   28.57500
14     PZ   84.57641
15     PZ    0.12141
16     CZ   28.69641
17     PZ   84.69782
18     PZ    0.00000
19     CZ   28.69641
20     PZ   84.69782
21     PZ    0.00000
C
C    SURFACE CARDS FOR 190 FGE MATERIAL
C
```

```
22      RCC 0 0  28.96172 0 0  18.90039   9.45019
C
C    SURFACE CARDS FOR THE HEXAGONAL 7-PACK.
C
30 PX -28.75
31 PX  28.75
32 P   1    1.7321    0    57.5
33 P  -1    1.7321    0    57.5
34 P  -1    1.7321    0   -57.5
35 P   1    1.7321    0   -57.5
36 PZ  0.0
37 PZ  84.69782
C
C    SURFACE CARDS FOR THE MGO AND SALT LAYERS.
C
50 PZ -300.00
52 PZ  616.321
53 PZ  316.321
C
C    SURFACE CARDS FOR THE 7-PACK STACK INFINITE ARRAY.
C
*60 PY -78.5
*61 PY  78.5
*62 P   1.7321   1    0   157
*63 P   1.7321  -1    0   157
*64 P   1.7321  -1    0  -157
*65 P   1.7321   1    0  -157
66 PZ -0.0
67 PZ  254.09346

C
C    MODE CARD.
C
MODE N
C
C    MATERIAL CARDS
C
C    PU-CH2 (LOWER AND UPPER DRUMS)
C
M1     1001.00C -0.114745  6012.00C -0.191390 6013.00C -0.002243
        94239.00C -0.038877 8016.00C -0.652745
MT1     h-poly.40T  h-h2o.40t
C
C    BE REFLECTOR (LOWER AND UPPER DRUMS)
C
M2     4009.00C -1.000000
MT2     be-met.40t
C
C    POLYETHYLENE
C
M3     1001.00C -0.143718  6012.00C -0.846362  6013.00C -0.00991942
MT3     h-poly.40T
C
C    304 STAINLESS STEEL
C
M4     26054.00C -0.038585  26056.00C -6.2810-01 26057.00C -1.4765-02
        26058.00C -1.9994-03 24050.00C -7.9300-03 24052.00C -1.5903-01
        24053.00C -1.8380-02 24054.00C -4.6614-03 28058.00C -6.3838-02
        28060.00C -2.5437-02 28061.00C -1.1242-03 28062.00C -3.6431-03
        28064.00C -9.5774-04 25055.00C -0.0200000  6012.00C -7.9073-04
         6013.00C -9.2674-06 15031.00C -0.0004500 14028.00C -9.18734-03
        14029.00C -4.83179-04 14030.00C -3.29477-04 16032.00c -2.8396-04
        16033.00C -2.3444-06 16034.00C -1.3633-05  16036.00C -6.7299-08
C
C    CANE FIBERBOARD DUNNAGE (LOWER AND UPPER DRUMS)
C
M5     6012.00C  5.9358  6013.00C .06420  1001.00C 10  8016.00C  5
C
C    CARBON STEEL DRUM.
```

```
C
M6       6012.00C -0.001483  6013.00C -0.000017  25055.00C -0.006000
         15031.00C -0.000350  16032.00C -3.7861-04  16033.00C -3.1258-06
         16034.00C -1.8178-05  16036.00C -8.9732-08  26054.00C -5.5990-02
         26056.00C -9.1143-01  26057.00C -2.1425-02  26058.00C -2.9013-03
C
C
C    MGO LAYER.
C
M7    12024.00C 0.39495  12025.00C 0.05 12026.00C 0.05505 8016.00C 0.5
C
C    SALT REFLECTOR.
C
M8    11023.00C 0.5  17035.00C 0.3789  17037.00C 0.1211
C
C    OVERBATCH PU-CH2
C
M9     1001.00C -0.114745  6012.00C -0.191390 6013.00C -0.002243
         94239.00C -0.038877 8016.00C -0.652745
MT9     h-poly.40T  h-h2o.40t
C
C    SOURCE CARDS.
C
KCODE 20000 1.0 200 700
KSRC   0 0 38  28 49 38  -28 -50 38
      -57 0 38  57 0 38  -28 50 38
       0 0 122  28 49 122  -28 -50 122
      -57 0 122  57 0 122  -28 50 122
       0 0 207  28 49 207  -28 -50 207
      -57 0 207  57 0 207  -28 50 207
      -28 50 38  -28 50 122  -28 -50 207
       47 0 110  67 0 135  57 10 122
       57 -10 122

PRINT
C
C    PRINT TO MCTAL FILE
C
PRDMP 2j 1
```

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Appendix E Two-Container Combinations

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Note: Appendix E is unaffected by Revision 8 and no changes were made except an editorial correction in the introduction section. The stated conclusion, that models with two different container loadings and/or container types are always less reactive than the more reactive configuration of two of the same container type, is true based on the cases performed in prior revisions using MCNP5. WIPP-099 (*Extent of Condition Review for WIPP-016, Rev. 7*) documents the analysis for the two-container combinations for the updated 200 FGE limit for machine-compacted waste in an SWB introduced in Revision 8 of this NCSE. This appendix will be updated when Appendix A and Appendix B are updated to MCNP6.2. Original signatures are on file with WIPP-016 Revision 0.

Analyst		
Senior NCS Engineer	G. W. Neeley	Date
Peer Reviewer		
Senior NCS Engineer	S. L. Larson	Date

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Introduction

The two-container model described in the Appendices A, B, C, and D is further evaluated in this appendix. Previously, both containers in the two-container stack were of the same type. This appendix evaluates two different containers or loadings in the two-container stack to determine if a more reactive configuration can occur. The pipe overpack configurations are not considered because the results for the two-container model are lower than those for the array model as discussed in Appendix D and because the overpack configuration keeps the fissile material centered in the drum. The details of the modeled containers are given in the previous appendices and not fully repeated here. These calculations were originally performed to a USL of 0.97. Subsequently, the USL was further reduced by an administrative margin of 0.01, resulting in a USL of 0.96. The models containing two containers of the same type were re-evaluated to meet the lower USL. Because the objective of these calculations is only to verify that a combination of two different types of containers is less reactive than a model with two of the same container type, these calculations were not revised.

E.1 Fully Compacted 100-gallon Drum/ Non-Compacted 55-gallon Drum Combination

The first sequence of the two-drum calculations showed a 55-gallon drum containing non-compacted CH waste with 1 weight percent (wt%) beryllium from Appendix A is stacked on a 100-gallon drum containing fully compacted waste from Appendix C. Furthermore, two models were employed for the fully compacted 100-gallon drums: a 170-FGE mass without design vertical spacing between drums, and the more representative design, which accounts for design spacing and contains 200 FGE.

A series of parametric computations were performed to ascertain the most reactive H/Pu ratio for the 100-gallon/55-gallon drum combination. A limited range calculation was performed by fixing the H/Pu concentration of the ^{239}Pu/polyethylene-water waste mixture in the 55-gallon drum and varying the fissile mixture H/Pu ratio in the 100-gallon drum to find the peak value. The H/Pu concentration in the 55-gallon drum was then changed and the calculation repeated until a reactivity map was generated over a limited range. The most reactive state was then selected for the 55-gallon drum and the full spectrum run on the H/Pu range for the 100-gallon drum. The results of the parametric study indicated that the optimal H/Pu ratio for the 55-gallon drum in the two-drum system ranged between 800 and 850. The results of the 2-drum computations are summarized in Table E-1, Figure E-1, and Figure E-2.

Table E-1. MCNP Results for 100-gallon Drum (Fully Compacted)/55-gallon Drum (Particulate Beryllium) Combination

Optimum H/Pu Ratio		Reflector	k_{eff}	σ	k_{eff} + 2σ	Filename
100-gal Drum	55-gal Drum					
100-gal Drum Modeled without Design Separation containing 170 g ^{239}Pu						
900	800	Concrete	0.94928	0.00083	0.95094	tdmp118
900	800	Salt	0.94986	0.00083	0.95152	tdmp718
950	800	MgO	0.94956	0.00086	0.95128	tdp1319
100-gal Drum Modeled with Design Separation containing 200 g ^{239}Pu						
900	800	Concrete	0.93586	0.00081	0.93748	tdmp158
800	800	Salt	0.93505	0.00085	0.93675	tdmp756

900	800	MgO	0.93638	0.00083	0.93804	tdp1358

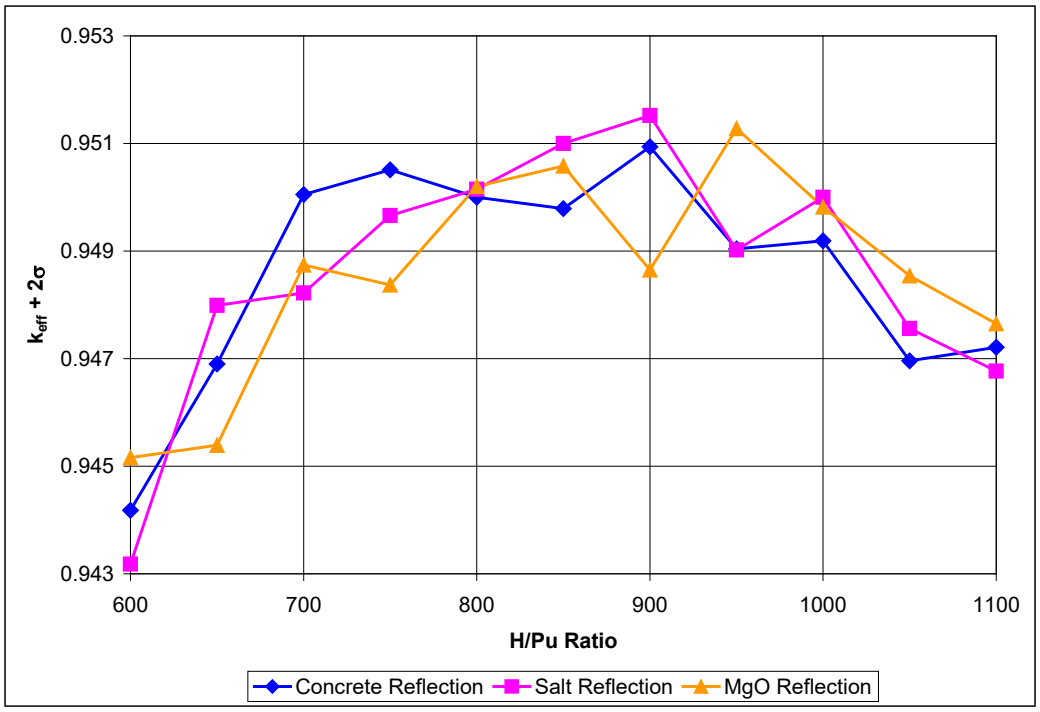

Figure E-1. 100-gallon (Fully Compacted) / 55-gallon (Particulate Beryllium) Drum Combination without Design Separation

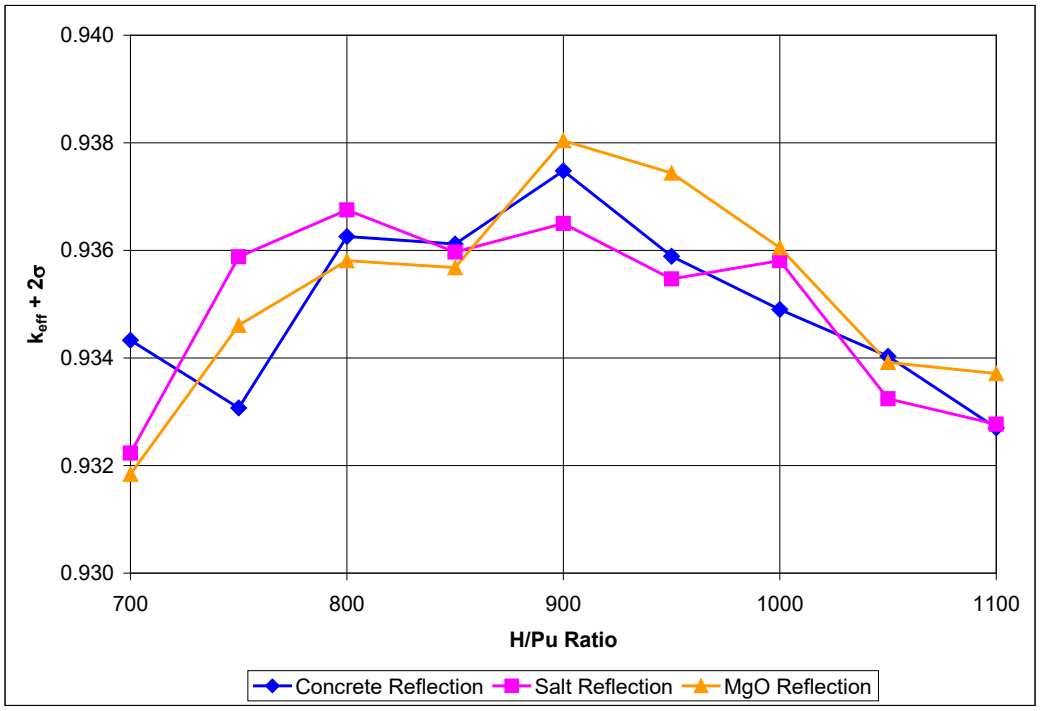

Figure E-2. 100-gallon (Fully Compacted) / 55-gallon (Particulate Beryllium) Drum Combination with Design Separation

E.2 Fully Compacted 100-gallon Drum/55-gallon Drum with High Beryllium Combination

In the next two-drum combination, a 55-gallon drum containing non-compacted CH waste with 100 kilograms of beryllium from Appendix B is stacked on a 100-gallon drum containing fully compacted waste from Appendix C. No vertical design spacing is modeled in the 55-gallon drum in either configuration. The 55-gallon drum model evaluates 100 kilograms of beryllium surrounding the fissile mass at a bulk density of 70% of theoretical density. The beryllium reflector is backed by 70% dense polyethylene, which fills the remaining volume of the container. This density bounds all non-compacted waste streams since the maximum theoretical density for randomly packed uniform spheres ("Is random packing of spheres well defined?" [Torquato et al. 2007] and "Recursive packing of dense particle mixtures" [Elliot et al. 2002]) is 70%. Furthermore, the assumption that the beryllium will not form a consistent compact reflector around the fissile mass, as modeled in Appendix B. Such a form would effectively have to be constructed and packaged intentionally to become a tight reflector shell around the optimally moderated fuel volume.

A limited range parametric computation was performed to determine the optimal H/Pu ratio for the 55-gallon drum in the two-drum system. The fissile mixture in the 55-gallon drum is maintained in its most reactive state (in this case, an H/Pu ratio of approximately 800), while the composition in the 100-gallon drum was varied over a full range of H/Pu ratios to ensure that the most reactive combination state is achieved. Table E-2, Figure E-3, and Figure E-4 summarize the results of the calculation. The results of the calculation indicate that depending on the 100-gallon model employed, either the 170 grams or the 200 grams of ^{239}Pu mass limit on the fully compacted drum ensures that the eigenvalue of the two-drum system remains at or below the USL.

Table E-2. 100-gallon Drum (Fully Compacted)/55-gallon Drum (100 kg Beryllium) Combination

Optimum H/Pu Ratio		Reflector	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
100-gal Drum	55-gal Drum					
100-gal Drum Modeled without Design Separation containing 170 g ^{239}Pu						
950	800	Concrete	0.94099	0.00082	0.94263	tdmp419
900	800	Salt	0.93880	0.00086	0.94052	tdp1018
900	800	MgO	0.94018	0.00084	0.94186	tdp1618
100-gal Drum Modeled with Design Separation containing 200 g ^{239}Pu						
850	800	Concrete	0.93174	0.00083	0.93340	tdmp457
900	800	Salt	0.92848	0.00082	0.93012	tdp1058
950	800	MgO	0.92999	0.00081	0.93161	tdp1659

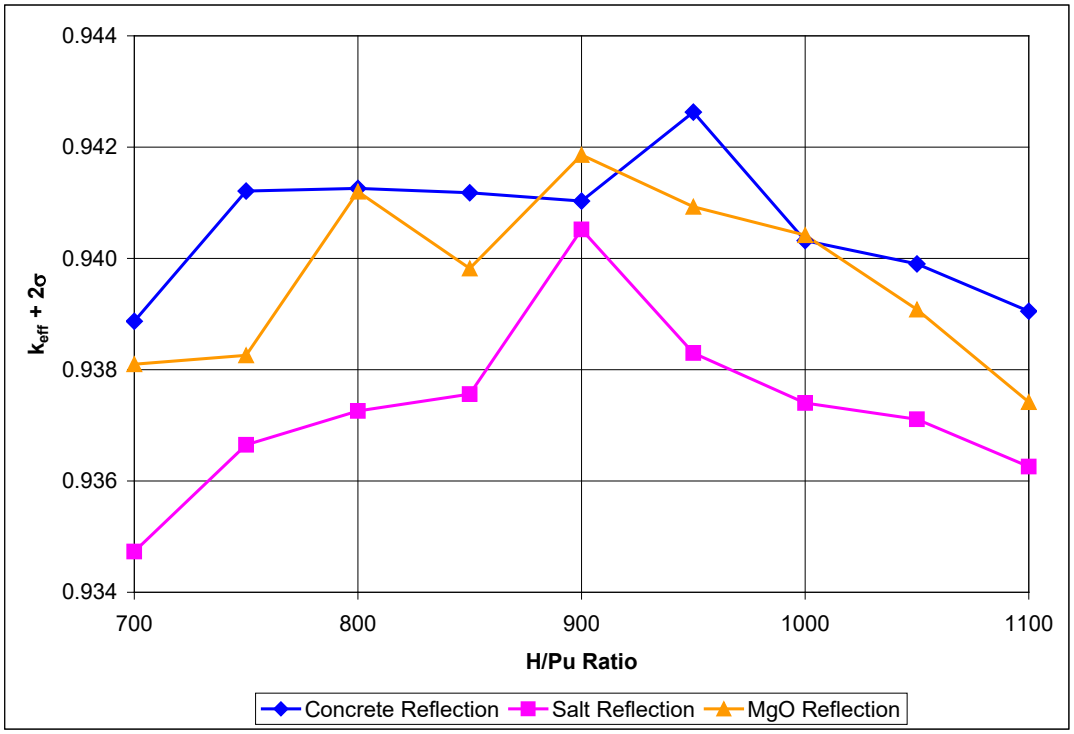

Figure E-3. 100-gallon (Fully Compacted) / 55-gallon (100 kg Beryllium) Drum Combination without Design Spacing

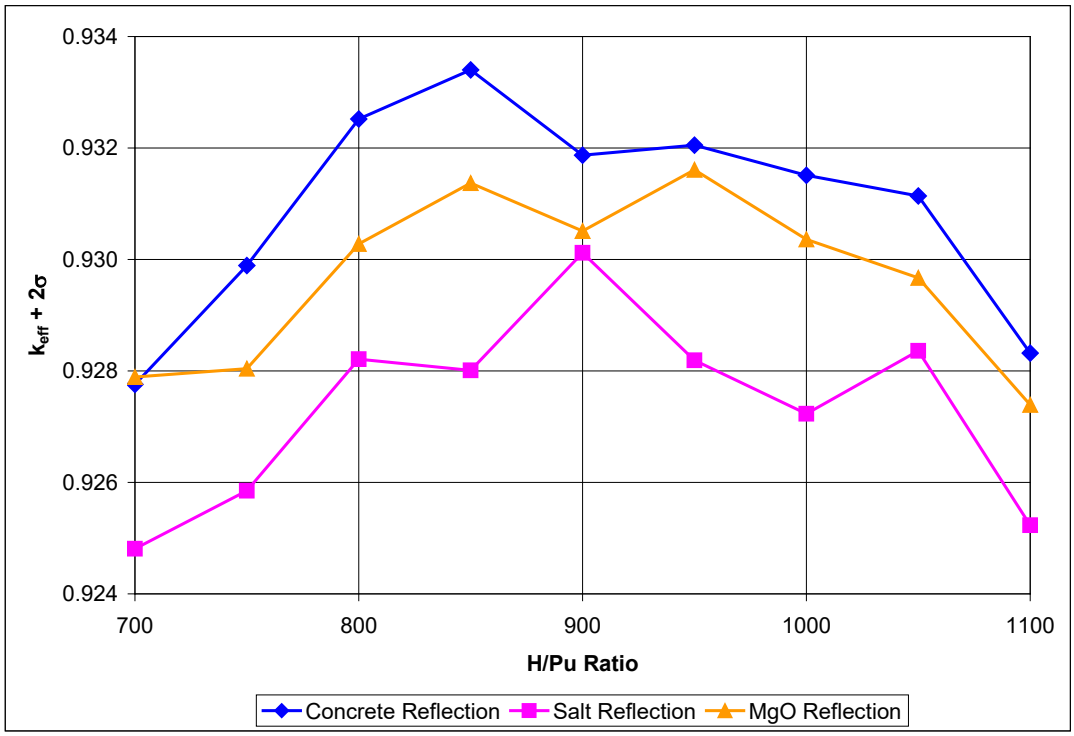

Figure E-4. 100-gallon (Fully Compacted) / 55-gallon (100 kg Beryllium) Drum Combination with Design Spacing

E.3 Direct-Loaded Machine-Compacted SWB/ Non-Compacted 55-gallon Drum Combination

In the next sequence of two-container calculations, a 55-gallon drum containing non-compacted CH waste from Appendix A is stacked on an SWB direct loaded with fully compacted waste from Appendix C.

Calculations were performed fixing the H/Pu concentration of the ^{239}Pu-polyethylene-water waste mixture in the 55-gallon drum at the most reactive state as shown in Table E-1 and varying the H/Pu range for the direct-loaded SWB containing fully compacted waste. The results of the two-container computations are summarized in Table E-3 and Figure E-5, indicating that the 200 grams of ^{239}Pu mass limit on the 55 gallon drum with particulate beryllium ensures the two-container system remains at or below the USL.

Table E-3. SWB (Direct Loaded Fully Compacted)/55-gallon Drum (Particulate Beryllium) Combination

Optimum H/Pu Ratio		Reflector	k_{eff}	σ	k_{eff} + 2σ	Filename
SWB	55-gal Drum					
900	800	Concrete	0.95127	0.00096	0.95319	cs95580
800	800	Salt	0.95189	0.00095	0.95379	ss85580
800	800	MgO	0.95176	0.00092	0.95360	ms85580

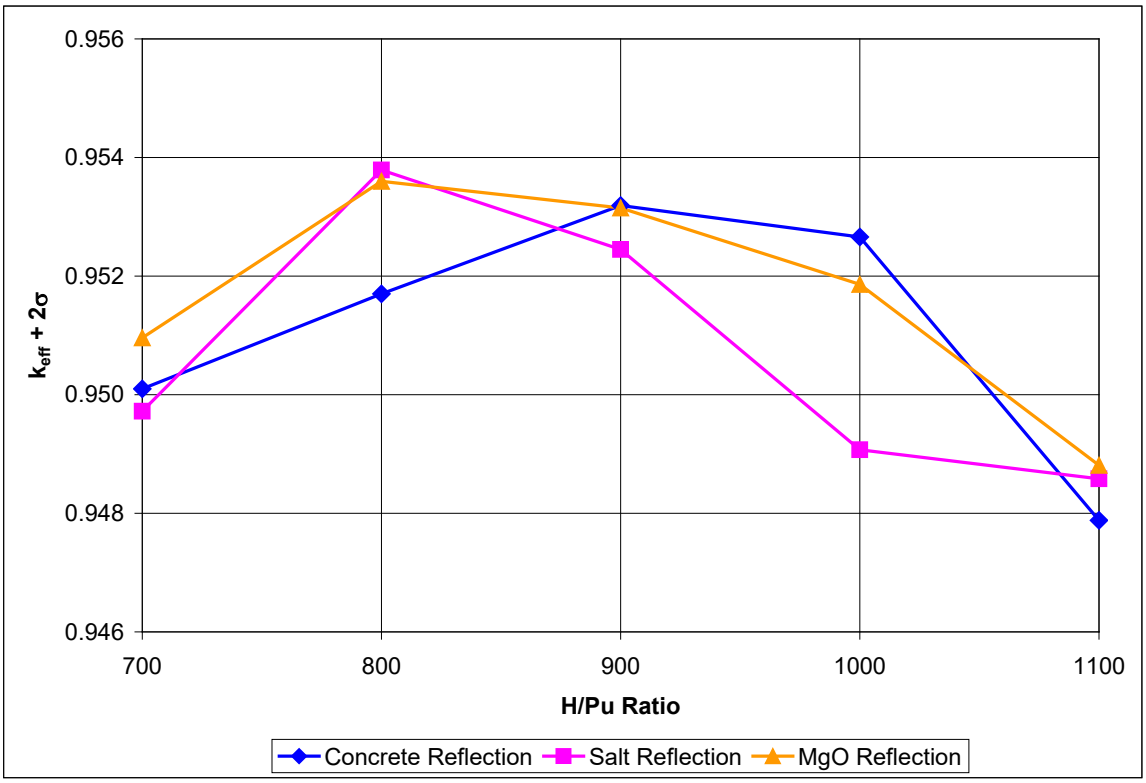

Figure E-5. SWB (Direct Loaded Fully Compacted) / 55-gallon (Particulate Beryllium) Drum Combination

E.4 Direct-Loaded Machine-Compacted SWB/55-gallon Drum with High beryllium Combination

The next two-container combination (the 55-gallon drum containing 100 grams of ^{239}Pu fissile mass reflected by 100 kilograms of beryllium, as described in Section E.2), is stacked on top of an SWB that has been direct loaded with grams of ^{239}Pu of fully compacted waste as described in Appendix C.

The computation was performed consistently with the previous section. Calculations were performed fixing the H/Pu concentration of the ^{239}Pu-polyethylene-water waste mixture in the 55-gallon drum at 800 and varying the H/Pu range for the fully compacted SWB. The results of the two-container computations are summarized in Table E-4 and Figure E-6. The eigenvalue of the two-container system remains below the USL, which includes allowance for administrative margin.**Error! Reference source not found.**

Table E-4. SWB (Direct Loaded Fully Compacted)/55-gallon Drum (100 kg Beryllium) Combination

Optimum H/Pu Ratio		Reflector	k_{eff}	σ	k_{eff} + 2σ	Filename
SWB	55-gal Drum					
900	800	Concrete	0.94483	0.00092	0.94667	cs9f580
800	800	Salt	0.94200	0.00098	0.94396	ss8f580
800	800	MgO	0.94425	0.00096	0.94617	ms8f580

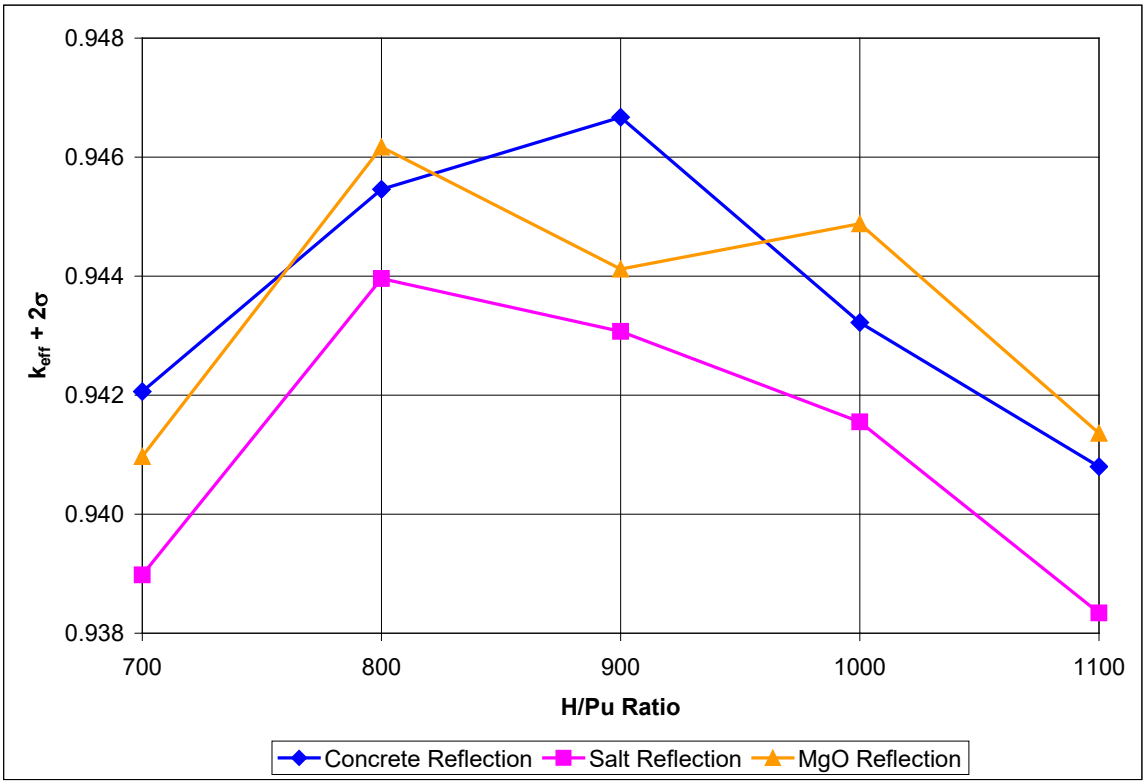

Figure E-6. SWB (Direct Loaded Fully Compacted) / 55-gallon (100 kg Beryllium) Drum Combination

E.5 Non-Compacted Direct-Loaded SWB/100-gallon Drum Combination

In this sequence of two-container calculations, a 100-gallon drum of fully compacted waste from Appendix C is stacked on top of a direct-loaded SWB containing non-compacted waste as described in Appendix A. The concrete, magnesium oxide (MgO), or salt reflection is conservatively placed as close as possible to each container, even though the reflector would most likely be outside the larger footprint of the SWB.

Calculations in Section A.3.2 found that the optimum H/Pu ratio in the non-compacted SWB is 900 to 1,000, thus a value of 950 was used here. (This value was also verified to be the optimum value for this configuration.) The results of the SWB/100-gallon drum calculations are summarized in Table E-5, Figure E-7, and Figure E-8. All results are below the USL of 0.97 and the results are also below the 0.96 USL with allowance for administrative margin when the design separation inherent in the 100-gallon drum is modeled.

Table E-5. Direct-loaded Non-compacted SWB/100-gallon Drum (Fully Compacted)

Optimum H/Pu Ratio		Reflector	k_{eff}	σ	k_{eff} + 2σ	Filename
Bottom SWB	100-gal Drum					
100-gal Drum Modeled without Design Separation containing 170 g ^{239}Pu						
950	950	Concrete	0.96552	0.00081	0.96714	tdms819
950	750	Salt	0.96443	0.00087	0.96617	tds1715
950	850	MgO	0.96516	0.00086	0.96688	tds2617
100-gal Drum Modeled with Design Separation containing 200 g ^{239}Pu						
950	900	Concrete	0.95216	0.00086	0.95388	tdms858
950	850	Salt	0.95138	0.00085	0.95308	tds1757
950	800	MgO	0.95085	0.00084	0.95253	tds2656

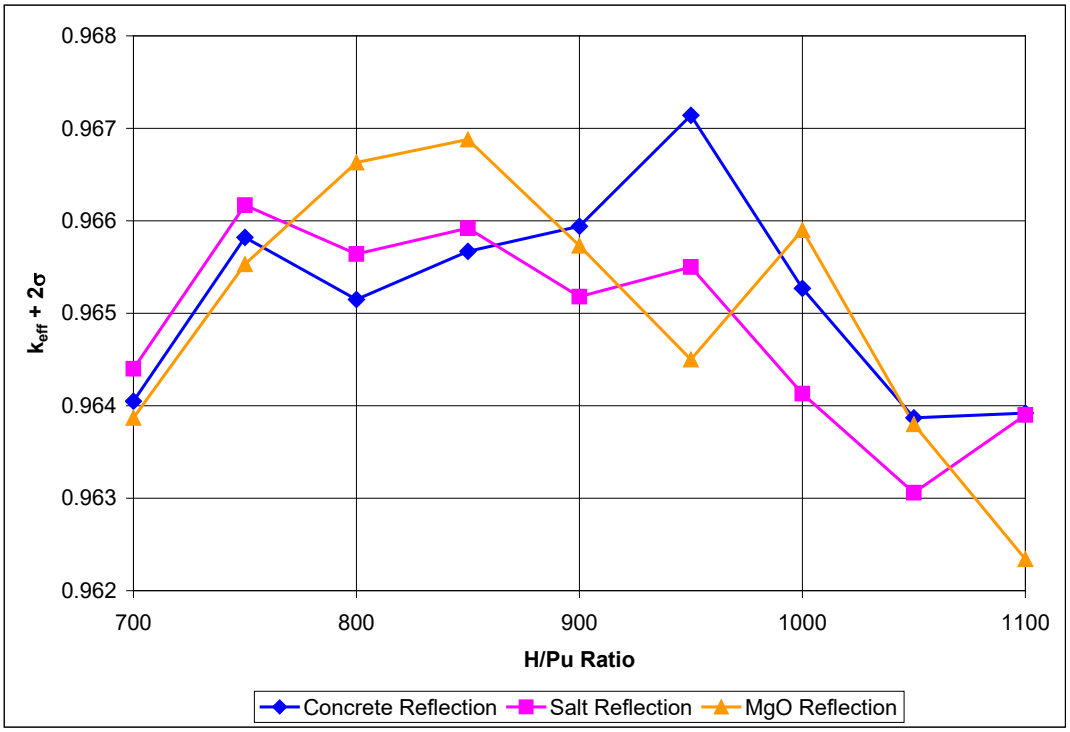

Figure E-7. Direct-loaded Non-compacted SWB / 100-gallon (Full Compaction) Drum without Design Separation

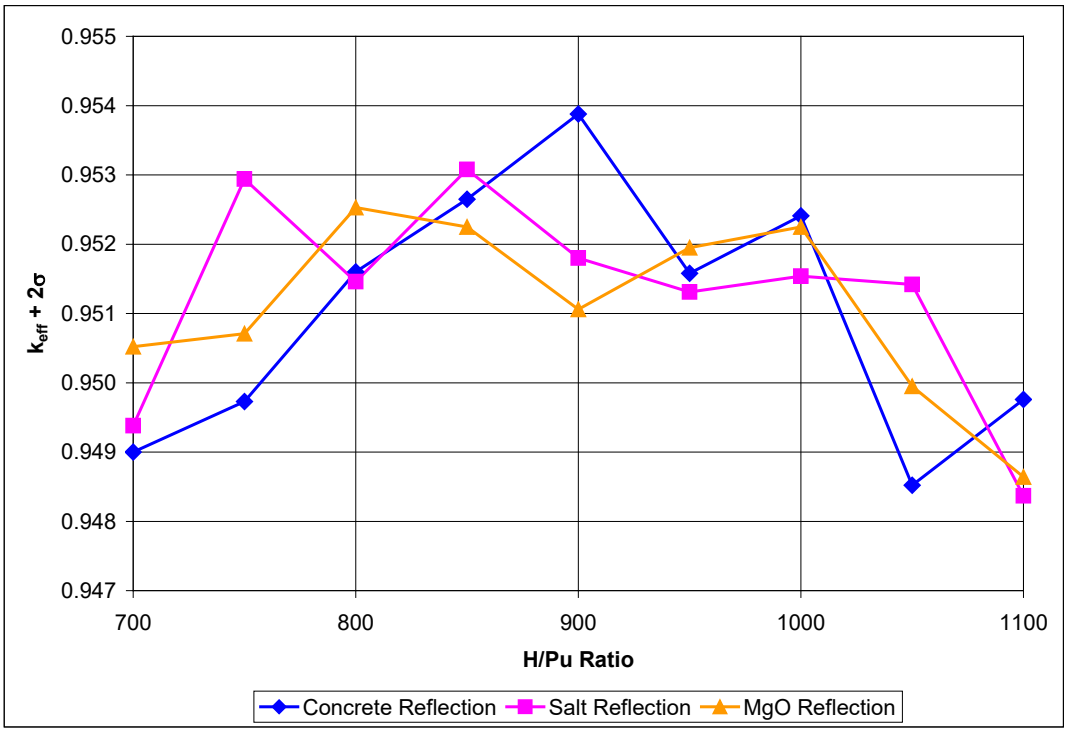

Figure E-8. Direct-Loaded Non-compacted SWB / 100-gallon (Full Compaction) Drum with Design Separation

E.6 Direct-Loaded SWB with Compacted Waste/100-gallon Drum Combination

- Both containers in this combination contain fully compacted waste as described in Appendix C, where a 100-gallon drum is stacked on a direct-loaded SWB. Again, two models are considered for the 100-gallon drum containing the fully compacted waste: with and without design spacing.

Calculations were performed fixing the H/Pu ratio of the FGE waste mixture in the 100-gallon drum at the most reactive state (800 per Table C-5 for 170 FGE and 900 per Table C-6 for 200 FGE) and varying the H/Pu range for the fully compacted SWB. The results of the compacted SWB/100-gallon drum calculations are summarized in Table E-6, Figure E-9, and Figure E-10. All results are below the original USL of 0.97.

Table E-6. Direct-Loaded SWB/100-gallon Drum (Both Fully Compacted)

Optimum H/Pu Ratio		Reflector	k_{eff}	σ	k_{eff} + 2σ	Filename
Bottom SWB	100-gal Drum					
100-gal Drum Modeled without Design Separation containing 170 g ^{239}Pu						
800	800	Concrete	0.96719	0.00096	0.96911	cs818
900	800	Salt	0.96697	0.00093	0.96883	ss918
900	800	MgO	0.96748	0.00094	0.96936	ms918

Table E-6. Direct-Loaded SWB/100-gallon Drum (Both Fully Compacted)

Optimum H/Pu Ratio		Reflector	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
Bottom SWB	100-gal Drum					
100-gal Drum Modeled with Design Separation containing 200 g ^{239}Pu						
800	900	Concrete	0.95223	0.00096	0.95415	cs8v19
800	900	Salt	0.95139	0.0009	0.95319	ss8v19
800	900	MgO	0.95188	0.0009	0.95368	ms8v19

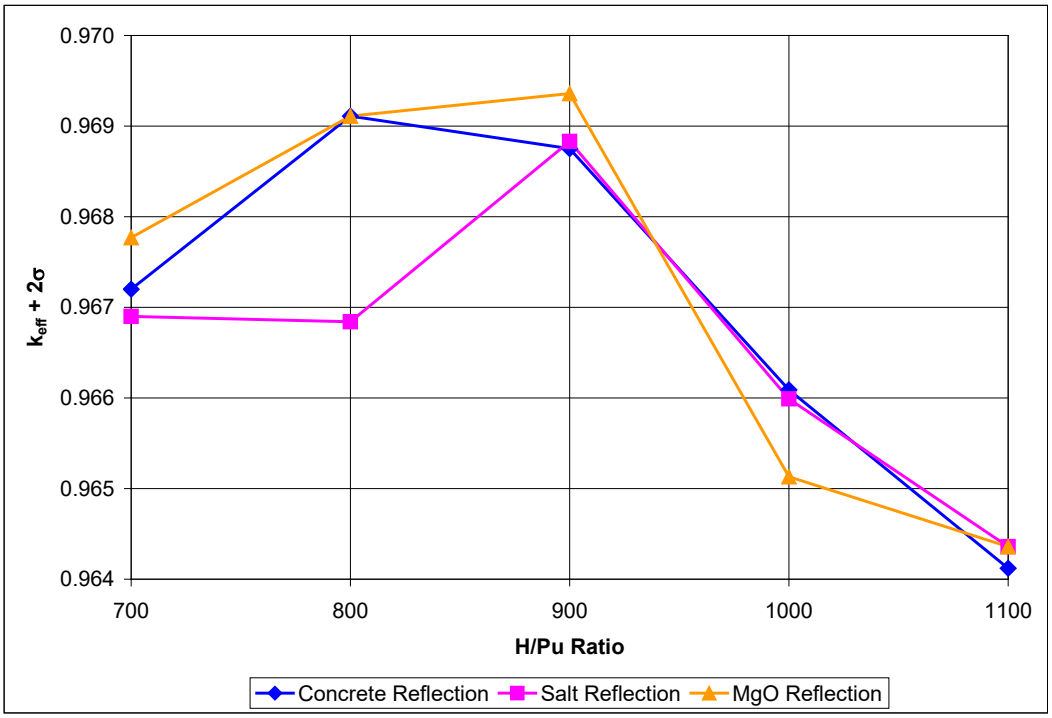

Figure E-9. SWB (Direct Loaded Full Compaction) / 100-gallon (Full Compaction) Drum without Design Separation

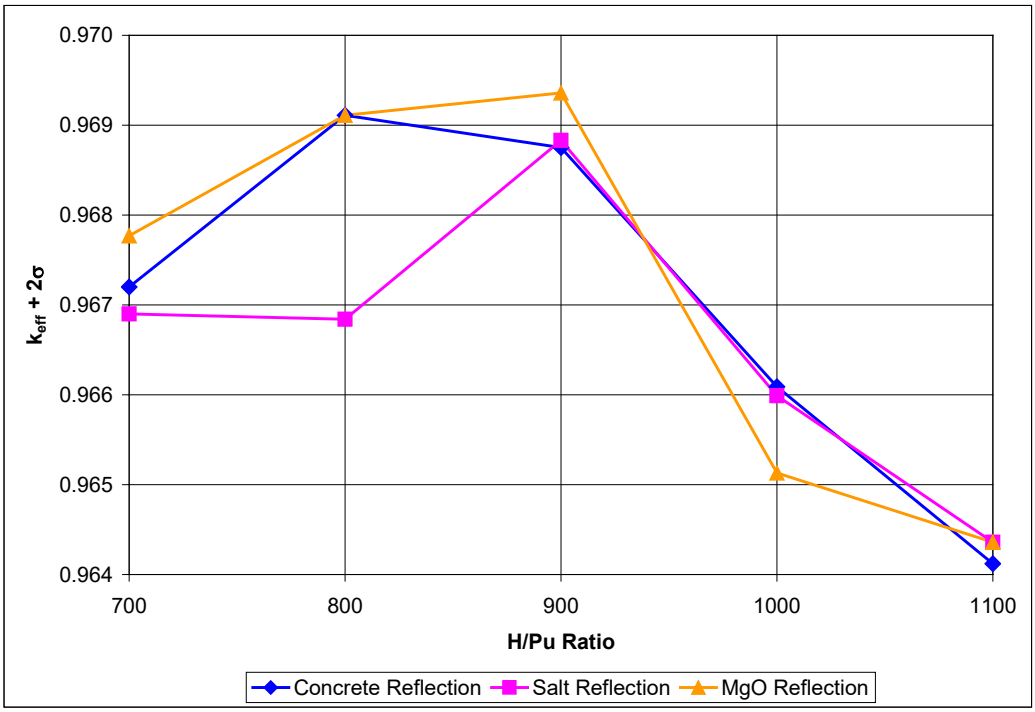

Figure E-10. SWB (Direct Laded Full Compaction) / 100-gallon (Full Compaction) Drum with Design Separation

E.7 Conclusions

The maximum reactivity from the various two-container models analyzed is summarized in Table E-7. In studying the results, the models with two different container loadings and/or container types are always less reactive than the more reactive configuration of two of the same container type. As expected, placing two different containers together results in an effective "averaging" of the reactivity of the two containers, and has a lower reactivity than the model with the most reactive containers. Note that the calculations performed for 55- and 100-gallon drums of compacted waste bound the 85-gallon drum. Also, the SWB cases bound the TDOP containers as they have the same footprint but are two tiers high with the same limits as an SWB. The results summary also shows that concrete, MgO, and salt are very comparable as infinite reflectors as each was the reflector resulting in the maximum reactivity in multiple cases. In fact, the results with the various reflectors are often within the statistical uncertainty of the code.

Subsequent to the performance of these calculations, the USL was reduced by an administrative margin of 0.01 resulting in a USL of 0.96. The models containing two containers of the same type were re-evaluated to meet the lower USL as discussed in the previous appendices. Because the objective of these calculations is only to verify that a combination of two different types of containers is less reactive than a model with two of the same container type, these calculations were not revised.

Table E-7. Summary of Two-Container Results

Section	Top Container	Bottom Container	Reflector of Max Reactivity	Maximum $k_{eff} + 2\sigma$
C.3.1	100-gal Drum w/o Design Spacing	100-gal Drum w/o Design Spacing	Salt/ Concrete	0.96642
C.3.2	Partially Compacted 100-gal Drum	Partially Compacted 100-gal Drum	Salt	0.96551
E.1	55-gal Drum with Particulate beryllium	100-gal Drum w/o Design Spacing	Salt	0.95152
E.2	55-gal Drum with Full Density beryllium	100-gal Drum w/o Design Spacing	Concrete	0.94263
E.5	100-gal Drum w/o Design Spacing	Non-compacted SWB	Concrete	0.96714*
E.6	100-gal Drum w/o Design Spacing	Fully Compacted Direct-Loaded SWB	MgO	0.96936
C.3.1	100-gal Drum with Design Spacing	100-gal Drum with Design Spacing	Concrete	0.93683
E.1	55-gal Drum with Particulate beryllium	100-gal Drum with Design Spacing	MgO	0.93804
E.2	55-gal Drum with Full Density beryllium	100-gal Drum with Design Spacing	Concrete	0.93340
E.5	100-gal Drum with Design Spacing	Non-compacted SWB	Concrete	0.95388[(a)]
E.6	100-gal Drum with Design Spacing	Fully Compacted Direct-Loaded SWB	Concrete	0.95415
C.4.1	Fully Compacted Direct-Loaded SWB	Fully Compacted Direct-Loaded SWB	All	0.96943
A.1.1	100-gal Drum Overpacked in SWB	100-gal Drum Overpacked in SWB	All	0.96691
E.3	55-gal Drum with Particulate beryllium	Fully Compacted Direct-Loaded SWB	Salt	0.95379
E.4	55-gal Drum with Full Density beryllium	Fully Compacted Direct-Loaded SWB	Concrete	0.94667
C.3.3	55-gal Drum Full Compaction w/o Design Spacing	55-gal Drum Full Compaction w/o Design Spacing	Concrete	0.96995[(b)]
C.3.3	55-gal Drum Partial Compaction w/o Design Spacing	55-gal Drum Partial Compaction w/o Design Spacing	Salt	0.96998[(b)]
C.3.3	55-gal Drum Full Compaction with Design Spacing	55-gal Drum Full Compaction with Design Spacing	Concrete	0.96583
A.3.1	55-gal Drum with Particulate beryllium	55-gal Drum with Particulate beryllium	MgO	0.88622
A.3.2	Non-compacted SWB	Non-compacted SWB	MgO	0.96976[(b)]
B.3.1	55-gal Drum with 70% Dense beryllium	55-gal Drum with 70% Dense beryllium	Concrete	0.927072

(a) Per Appendix A, a model of two non-compacted SWBs stacked on top of one another using the same parameters used here exceeded the 0.97 USL (a 60% dense steel wall was modeled to bring the result below the USL.) The cases modeled here use 50% dense wall on the non-compacted SWB.

(b) These cases model the container steel wall as 60% dense.

E.8 References

Elliot J.A., A. Kelly, and A.H. Windle, 2002. “Recursive packing of dense particle mixtures,” J. Mat. Sci. Lett. **21**:1249-1251; 2002.

Torquato, S., T.M. Truskett, and P.G. Debenedetti, 2007. “Is random packing of spheres well defined?” Phys. Rev. Lett. **84**:2064-2067; 2000.

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Appendix F Hazard Evaluation Tables

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Note: Appendix F is unaffected by Revision 8 and no changes were made from the previous revision. Original signatures are on file with WIPP-016 Revision 5.

Analyst NCS Engineer	B. A. Larsen	
Peer Reviewer Senior NCS Engineer	S. L. Larson	Date

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Introduction

The following hazard evaluation tables include potential causes for loss of controlled parameters described in Section 6.0 of this NCSE. The contingent events flow from the hazard evaluation tables and the associated upset condition are evaluated in Section 7.0.

Table F-1. Waste Handling Building Hazard Evaluation by Control Parameter

Waste Handling Building	Loaded shipping cask is stored in Parking Area on over the road transportation trailer. Loaded shipping cask is moved into the CH bay. Shipping cask is opened and unloaded onto facility pallets using an overhead crane. Facility pallet is transferred to the waste hoist via forklift and onto the conveyance loading car.			
Parameter	**Causes**	**Consequences/Analysis Limits**	**Barriers/Factors Contributing to Unlikely Failure**	**Notes**
Mass	Generator site error results in excess mass, onsite overpacking of damaged containers on site results in excess mass.	Fissile mass and beryllium are overbatched beyond the WAC requirements in the contingency analysis. Normal condition and contingency analysis models an optimized fissile mass in terms of moderation and geometry, which is very conservative compared to expected waste configuration. Use of expected configuration would result in higher subcritical mass. Site overpacking of damaged containers creates the potential to exceed container fissile mass limits.	Fissile mass limits established for transportation in HalfPACT, TRUPACT-II or –III shipping casks. Fissile mass and beryllium limits established for CH waste containers in WIPP WAC. One to one container overpacking ensures operations will not exceed container FGE limits. Not placing excess loose material into containers means site overpack will have same materials as shipped to the site per the WIPP WAC Multiple-to-one container overpacking is limited to the larger container fissile mass limits.	Measurements to satisfy the fissile mass limits must include 2 times the measurement uncertainty.
Geometry	Collision, fires, collision followed by fire, dropped facility pallet causes change in geometry	While geometry could be modified from a fire or other breach of a waste container (such as crane failure), a limited number of containers are handled at one time. Contingency analysis evaluates the bounding condition of the 41 ton RH waste forklift impacting the CH waste face and reducing the crushing the containers.	Waste container design, shipping cask in the CH bay and outside area, crane design, fire suppression system in CH bay, limited material in CH bay available to burn, vehicle control program to prevent non waste handling vehicles in the CH	Fissile material conservatively modeled as right cylinders either centralized to the container in the array cases or conservatively placed in two stacked containers such that the fissile material from the two containers is separated only by

Table F-1. Waste Handling Building Hazard Evaluation by Control Parameter

Waste Handling Building	**Loaded shipping cask is stored in Parking Area on over the road transportation trailer. Loaded shipping cask is moved into the CH bay. Shipping cask is opened and unloaded onto facility pallets using an overhead crane. Facility pallet is transferred to the waste hoist via forklift and onto the conveyance loading car.**			
Parameter	**Causes**	**Consequences/Analysis Limits**	**Barriers/Factors Contributing to Unlikely Failure**	**Notes**
			bay during waste handling.	the metal container and any spacing provided by the outer container. The SLB2 contingency model is the exception where the fissile mass is modeled in a prism in the corner of the box, which is noted as the most reactive credible configuration per the criticality analysis in the TRUPACT-III SAR.
Moderation	Excess moderation provided by plastic, graphite, beryllium, or water. Water-in waste from sprinkler activation, from firefighting,	Analysis modeled fissile mass in compact geometry at optimum moderation level by polyethylene / water mixture with no liquid restriction. Beryllium moderation shown to decrease reactivity. Polyethylene density up to 100% by volume evaluated in analysis depending on compaction state.	WIPP WAC imposes fissile and beryllium mass limits. WIPP WAC restricts residual liquid content of waste to less than 1% by volume.	The compaction density of polyethylene is typically not controlled such that compacted waste typically meets the lower fissile limits based on 100% compaction.
Interaction	Waste container compaction resulting from collision in the parking area or CH bay of the WHB	Infinite array of containers is modeled and shown to be subcritical such that spacing between containers is not required for criticality safety.	Waste container design and container handling protocol.	None
		Impact of the 41-ton forklift used for moving RH waste in a shielded cask with a CH waste array was evaluated as the bounding contingency event for loss of interaction control.	Vehicle control program to prevent non waste handling vehicles in the CH bay during waste handling.	None
	Overstacking of containers	Four-tier-high array shown to be subcritical.	Containers stacked two tiers high.	None

Table F-1. Waste Handling Building Hazard Evaluation by Control Parameter

Waste Handling Building	**Loaded shipping cask is stored in Parking Area on over the road transportation trailer. Loaded shipping cask is moved into the CH bay. Shipping cask is opened and unloaded onto facility pallets using an overhead crane. Facility pallet is transferred to the waste hoist via forklift and onto the conveyance loading car.**			
Parameter	**Causes**	**Consequences/Analysis Limits**	**Barriers/Factors Contributing to Unlikely Failure**	**Notes**
Neutron Absorption	Degraded container has rusted steel wall	Analysis models 50%-60% steel density to account for degraded containers.	WAC requires that drums are of good integrity. CH-TRAMPAC also requires that drums are of good integrity prior to shipment to WIPP.	None
Reflection – Internal to Container	Excess reflection provided by excess beryllium, polyethylene, etc., in container	Beryllium mass overbatched beyond the WAC requirements in the contingency analysis. Compacted waste modeled polyethylene at 70%-100% theoretical density to maximize internal reflection. Water filling containers of non-compacted waste also evaluated and system shown to remain subcritical.	WIPP WAC and shipping container SARs impose fissile and special reflector mass limits.	The compaction density of polyethylene is typically not controlled such that compacted waste typically meets the lower fissile limits based on 100% compaction.
Reflection – External to Container	Excess reflection provided by concrete or MgO around the container	Analysis models close fitting, infinite thick, concrete, salt or MgO reflection on all sides of containers in two-container models. Array analysis models MgO supersack plus infinite salt reflection which bounds reflection conditions found above ground.	CH Bay is large such that there is no tight-fitting concrete reflector.	None
Volume	Not controlled	Analysis conservatively models fissile masses as cylinders at the optimum H/D ratio of 1 with the remainder of the waste container filled with beryllium, poly/water mixture, or poly only	None	All containers approved to be shipped to WIPP in the HALF-PACT, TRUPACT-II or –III shipping casks are evaluated. The volume provided by the container is treated as geometry and interaction controls only.

Table F-1. Waste Handling Building Hazard Evaluation by Control Parameter

Waste Handling Building	**Loaded shipping cask is stored in Parking Area on over the road transportation trailer. Loaded shipping cask is moved into the CH bay. Shipping cask is opened and unloaded onto facility pallets using an overhead crane. Facility pallet is transferred to the waste hoist via forklift and onto the conveyance loading car.**			
Parameter	**Causes**	**Consequences/Analysis Limits**	**Barriers/Factors Contributing to Unlikely Failure**	**Notes**
Enrichment	Not controlled	Fissile material is modeled as ^{239}Pu. Uranium-235 and ^{233}U can be shipped under these limits using FGE ^{239}Pu as defined in the CH-TRAMPAC.	None	WAC imposes fissile limits expressed in FGE ^{239}Pu. The FGE value accounts for the difference in minimum critical mass between the isotope and ^{239}Pu. Thus, this evaluation models 100% enrichment of the fissile isotope as related by the FGE to ^{239}Pu.
Concentration	Not controlled	The fissile concentration is unrestricted and optimized by varying the H/Pu ratio in the fissile region.	None	None

Table F-2. Underground Hazard Evaluation by Control Parameter

Underground Storage Operations	**Waste transported onto conveyance; conveyance moved from waste shaft collar to the waste shaft station; waste moved from waste shaft station to active disposal room using forklift. Waste placed in the CH array stacked three tiers high. MgO supersack placed on top of stack.**			
Parameter	**Causes**	**Consequences/Analysis Limits**	**Barriers/Factors Contributing to Unlikely Failure**	**Notes**
Mass	Generator site error results in excess mass, onsite overpacking of damaged containers on site results in excess mass.	Fissile mass and beryllium are overbatched beyond the WAC requirements in the contingency analysis. Normal condition and contingency analysis models an optimized fissile mass in terms of moderation and geometry, which is very conservative compared to expected waste configuration. Use of expected configuration would result in higher subcritical mass. Site overpacking of damaged containers creates the potential to exceed container fissile mass limits.	Fissile mass limits established for transportation in HALF-PACT, TRUPACT-II or -III shipping casks. Fissile mass and beryllium limits established for CH waste containers in WIPP WAC. One to one container overpacking ensures operations will not exceed container FGE limits. Not placing excess loose material into containers means site overpack will have same materials as shipped to the site per the WIPP WAC Multiple-to-one container overpacking is limited to the larger container fissile mass limits.	Measurements to satisfy the fissile mass limits must include 2 times the measurement uncertainty.

Table F-2. Underground Hazard Evaluation by Control Parameter

Underground Storage Operations	**Waste transported onto conveyance; conveyance moved from waste shaft collar to the waste shaft station; waste moved from waste shaft station to active disposal room using forklift. Waste placed in the CH array stacked three tiers high. MgO supersack placed on top of stack.**			
Parameter	**Causes**	**Consequences/Analysis Limits**	**Barriers/Factors Contributing to Unlikely Failure**	**Notes**
Geometry	Collision, fires, collision followed by fire, dropped facility pallet causes change in geometry (roof collapse addressed in interaction parameter), ejection of material from drum, toppling of drum during an earthquake.	While geometry could be modified from a fire or other breach of a waste container (such as crane failure), a limited number of containers are handled at one time. Contingency analysis evaluates the bounding condition of the 41 ton RH waste forklift impacting the CH waste face and crushing the containers.	Waste container design, shipping cask in the CH bay and outside area, crane design, fire suppression system in CH bay, limited material in CH bay available to burn, vehicle control program to prevent non waste handling vehicles in the CH bay during waste handling.	Fissile material conservatively modeled as right cylinders either centralized to the container in the array cases or conservatively placed in two stacked containers such that the fissile material from the two containers is separated only by the metal container and any spacing provided by the outer container. The SLB2 contingency model is the exception where the fissile mass is modeled in a prism in the corner of the box, which is noted as the most reactive credible configuration per the criticality analysis in the TRUPACT-III SAR.
Moderation	Excess moderation provided by plastic, graphite, beryllium, or water. Water-in waste from sprinkler activation, from firefighting, and as a result of hoist failure such that the load falls into the waste shaft sump	Analysis modeled fissile mass in compact geometry at optimum moderation level by polyethylene/water mixture with no liquid restriction. Beryllium moderation shown to decrease reactivity. Polyethylene density up to 100% by volume evaluated in analysis depending on compaction state.	WIPP WAC imposes fissile and beryllium mass limits. WIPP WAC restricts residual liquid content of waste to less than 1% by volume.	The compaction density of polyethylene is typically not controlled such that compacted waste typically meets the lower fissile limits based on 100% compaction.

Table F-2. Underground Hazard Evaluation by Control Parameter

Underground Storage Operations	**Waste transported onto conveyance; conveyance moved from waste shaft collar to the waste shaft station; waste moved from waste shaft station to active disposal room using forklift. Waste placed in the CH array stacked three tiers high. MgO supersack placed on top of stack.**			
Parameter	**Causes**	**Consequences/Analysis Limits**	**Barriers/Factors Contributing to Unlikely Failure**	**Notes**
Interaction	Waste container interaction resulting from waste hoist failure, collision in the underground; roof fall during transport or after disposal	Infinite array of containers is modeled and shown to be subcritical such that spacing between containers is not required for criticality safety. Impact of the 41-ton forklift used for moving RH waste in a shielded cask with a CH waste array was evaluated as the bounding contingency event for loss of interaction control. Four-tier-high array and compacted array resulting from roof fall are shown to be subcritical.	Waste hoist has redundant brakes and ropes. Remote handled waste handling equipment is typically placed between the CH waste face and the approaching 41 ton forklift. Underground array limited to three-tiers high. Mining program limits the mined height such that a four-tier stack is not possible in most areas. Mine engineering provides properly designed roof systems to prevent roof collapse.	None
Neutron Absorption	Degraded container has rusted steel wall	Analysis models 50%-60% steel density to account for degraded containers.	WAC requires that drums are of good integrity. CH-TRAMPAC also requires that drums are of good integrity prior to shipment to WIPP.	None
Reflection – Internal to Container	Excess reflection provided by excess beryllium, polyethylene, etc. in container	Beryllium mass overbatched beyond the WAC requirements in the contingency analysis. Compacted waste modeled polyethylene at 70%-100% theoretical density to maximize internal reflection. Water filling containers of non-compacted waste also evaluated and system shown to remain subcritical.	WIPP WAC and shipping container SARs impose fissile and special reflector mass limits.	The compaction density of polyethylene is typically not controlled such that compacted waste typically meets the lower fissile limits based on 100% compaction.

Table F-2. Underground Hazard Evaluation by Control Parameter

Underground Storage Operations	**Waste transported onto conveyance; conveyance moved from waste shaft collar to the waste shaft station; waste moved from waste shaft station to active disposal room using forklift. Waste placed in the CH array stacked three tiers high. MgO supersack placed on top of stack.**			
Parameter	**Causes**	**Consequences/Analysis Limits**	**Barriers/Factors Contributing to Unlikely Failure**	**Notes**
Reflection – External to Container	Excess reflection provided by salt or MgO around the container	Analysis models close fitting, infinite thick, concrete, salt or MgO reflection on all sides of containers in two-container models. Array analysis models MgO supersack plus infinite salt reflection to represent reflection conditions in underground.	MgO supersack configuration.	None
Volume	Not controlled	Analysis conservatively models fissile masses as cylinders at the optimum H/D ratio of 1 with the remainder of the waste container filled with beryllium, poly/water mixture, or poly only	None	All containers approved to be shipped to WIPP in the HALF-PACT, TRUPACT-II or –III shipping casks are evaluated. The volume provided by the container is treated as geometry and interaction controls only.
Enrichment	Not controlled	Fissile material is modeled as ^{239}Pu. Uranium-235 and ^{233}U can be shipped under these limits using FGE ^{239}Pu as defined in the CH-TRAMPAC.	None	WAC imposes fissile limits expressed in FGE ^{239}Pu. The FGE value accounts for the difference in minimum critical mass between the isotope and ^{239}Pu. Thus, this evaluation models 100% enrichment of the fissile isotope as related by the FGE to ^{239}Pu.
Concentration	Not controlled	The fissile concentration is unrestricted and optimized by varying the H/Pu ratio in the fissile region.	None	None

Appendix G Criticality Control Overpack

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Note: Appendix G is unaffected by Revision 8 and no changes were made from the previous revision. Original signatures are on file with WIPP-016 Revision 6.

Analyst Senior NCS Engineer	S. L. Larson	Date
Peer Reviewer Senior NCS Engineer	E. P. Elliott	Date

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Introduction

In order to allow for increased fissile content in a single shipment of CH waste and to reduce the stringent requirement and associated costs with construction of pipe overpacks evaluated in Appendix D, a criticality control overpack (CCO) configuration for the 55-gallon drum has been approved. The waste is contained within a cylindrical criticality control container (CCC) that is constructed of a 6-inch, 304 stainless steel pipe, placed in the CCO. Sample MCNP5 input file listings for the models contained in this appendix are included in Section G.6.

This appendix was revised in Revision 6 to allow machine-compacted waste in a CCO by adding a limit on the amount of plastic present. That limit is less than the amount of polyethylene present in the MCNP5 models for the CCO with a 25% polyethylene and 75% water (by volume) moderator. No new MCNP calculations were performed in this revision.

G.1 CCO Configuration

The CCO has one configuration in which a CCC is filled with waste and placed inside a 55-gallon drum. The CCC is a standard 6-inch 304 stainless steel pipe with blind flanges that bolt onto each end of the cylinder. The CCC is then placed inside of a standard 55-gallon drum and held in place by plywood dunnage plates that are glued together and stacked in the top and bottom of the drum as shown in Figure G-1. This configuration constitutes the CCO waste container. Dimensions for the CCO are listed in Table G-1. The CCC and dunnage plate dimensions are based on the dimensions given in the TRUPACT-II SAR (DOE-CBFO 2020) and CCO drawings (WTS 2012). The 55-gallon drum radial dimensions are taken from Table 2-1 and the drum internal height is the external height minus the wall thickness.

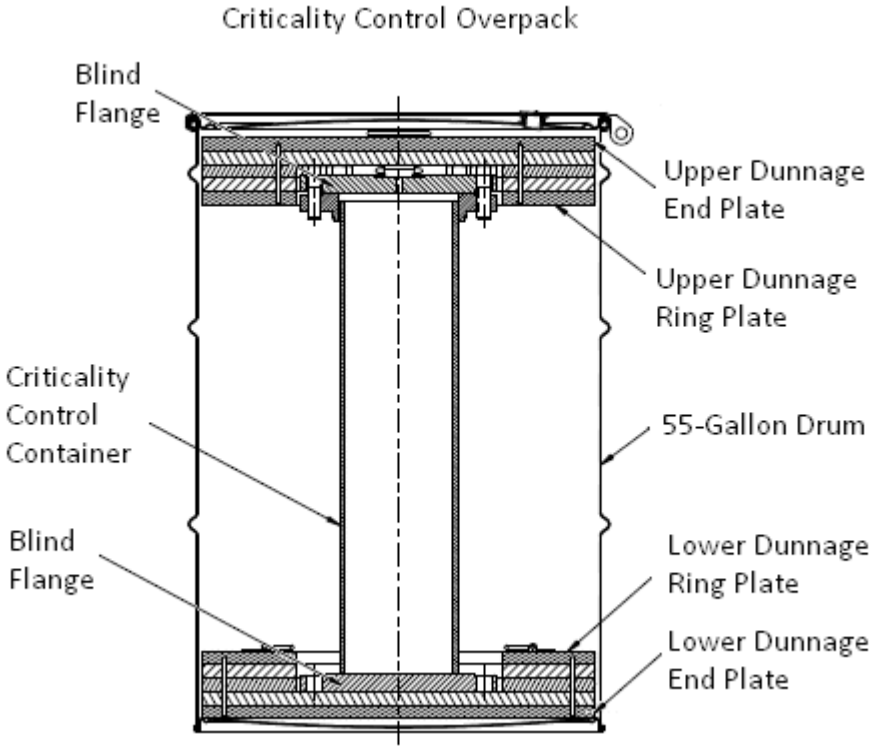

Figure G-1. CCO Assembly

Table G-1. CCO Component Dimensions

CCO Component	Dimension	Measurement (in.)
CCC	Outer Diameter	6.625
	Wall Thickness	0.28
	Inner Height	26.943
	Flange Thickness	1
Dunnage Plates	End Plate	2 Plates
	Ring Plate	3 Plates
	Plate Thickness	0.75
	Ring Plate Inner Diameter	11
55-Gallon Drum	Outer Diameter	22.5956
	Wall Thickness	0.0478
	Overall Height	35

G.2 CCO MCNP5 Models

The CCC wall and endplates are modeled as type 304 stainless steel using the composition in Table G-2. The upper and lower dunnage is 5 plywood sheets that are ¾ inch thick with a cutout in 3 of the sheets to hold the CCC in place. The plywood dunnage around the CCC is modeled as cellulose ($C_6H_{10}O_5$) at a maximum density of 0.387 g/cm^3 from AREVA [2012]. The 55-gallon drum is modeled using the dimensions given in Table G-1 using a carbon steel wall with the composition given in Table G-3 at 50% density, or 3.93 g/cm^3 to account for possible corrosion. The fissile mass is modeled as a cylinder with 380 grams of ^{239}Pu mixed with mixture of 75% water and 25% polyethylene for maximum moderation. The parameters for this mixture are given in Table 5-4. A 1.6 kilogram solid mass of beryllium modeled at 1.848 g/cm^3 was included to represent the addition of up to 1 wt% of special reflectors. This mass of beryllium was determined by taking 1 wt% of the gross weight limit of a loaded CCO container. The compositions of the stainless steel and carbon steel come from the stndrd.n file included in the Visual Editor code package of MCNP5-1.51 from RSICC [2008]. All cross-sections used are from the ENDF-VI library.

Table G-2. Material Composition for type 304 Stainless Steel for the CCC Structure

Element	MCNP Library Specification	Wt. Fraction	Element	MCNP Library Specification	Wt. Fraction
Density - 8 g/cm^3					
C	6000.60c	0.0003	^{54}Fe	26054.60c	0.039996
Si	14000.60c	0.005	^{56}Fe	26056.60c	0.644764
P	15031.60c	0.000225	^{57}Fe	26057.60c	0.015026
S	16000.60c	0.00015	^{58}Fe	26058.60c	0.002039
Mn	25055.60c	0.01	^{58}Ni	28058.60c	0.06234
^{50}Cr	24050.60c	0.00793	^{60}Ni	28060.60c	0.024654
^{52}Cr	24052.60c	0.159031	^{61}Ni	28061.60c	0.001085
^{53}Cr	24053.60c	0.018378	^{62}Ni	28062.60c	0.003504
^{54}Cr	24054.60c	0.004661	^{64}Ni	28064.60c	0.000917

Table G-3. Material Composition for Carbon Steel for the CCO Structure

Element	MCNP Library Specification	Wt. Fraction	Element	MCNP Library Specification	Wt. Fraction
Density - 3.93 g/cm^3					
C	6000.60c	0.0006	^{56}Fe	26056.60c	0.91493
Mn	25055.60c	0.0035	^{57}Fe	26057.60c	0.021323
^{54}Fe	26054.60c	0.056755	^{58}Fe	26058.60c	0.002893

G.2.1 Array Model

The CCOs were modeled as an array of 21 CCOs arranged in 3 tiers of 7 packs stacked on top of each other and then infinitely reflected to represent their emplacement in the underground. The array model for the CCOs is similar to that of the direct loaded drums described in Appendix A and the pipe overpacks described in Appendix D. The main difference is that the fissile material for the CCO is contained within the CCC and the plywood dunnage at the top and bottom of the CCC provides stability and support to align the CCC in the drum. The CCO differs from the pipe overpack in that there is only one configuration for the CCC compared to multiple different types of pipe components for the pipe overpack. Another difference is that the area in the drum outside the CCC is not filled with cellulose or shielding material as in the pipe overpacks. Figure G-2 is an MCNP5 generated diagram of the array model with cylindrical source geometry located in the center of the CCC.

MCNP5 calculations support an FGE limit of 380 grams of ^{239}Pu. The fuel mixture used in this calculation is a mixture of plutonium, 25% polyethylene and 75% water. The beryllium was modeled as a 1.6 kilogram solid mass to account for any special reflectors that may be present in the waste. This weight was chosen because it corresponds to 1 wt% of the gross weight of a loaded CCO. The MgO sacks are no longer required to be placed on top of each waste stack in the underground, however modeling the array with the MgO present proved to be the more conservative configuration. All cases of the array model containing this mixture remained below the USL of 0.96 as show in Table G-4 and Figure G-3.

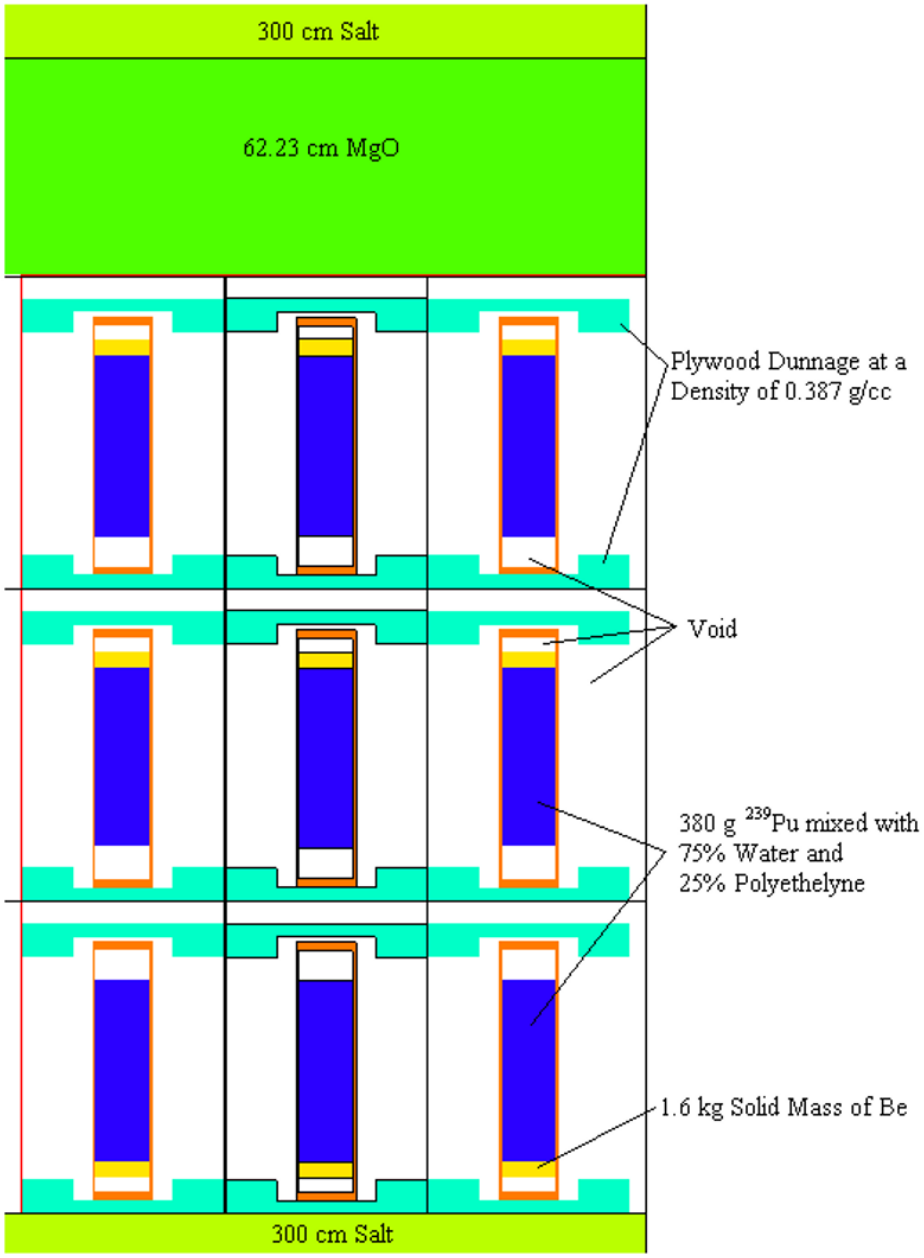

Figure G-2. Array Geometry for CCOs in the Underground

Table G-4. MCNP5 Results for Array Model

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
500	0.92541	0.00065	0.92671	hx500mgo380fge
600	0.93922	0.00063	0.94048	hx600mgo380fge
700	0.94400	0.00060	0.94520	hx700mgo380fge
800	0.94421	0.00062	0.94545	hx800mgo380fge
900	0.94063	0.00056	0.94175	hx900mgo380fge

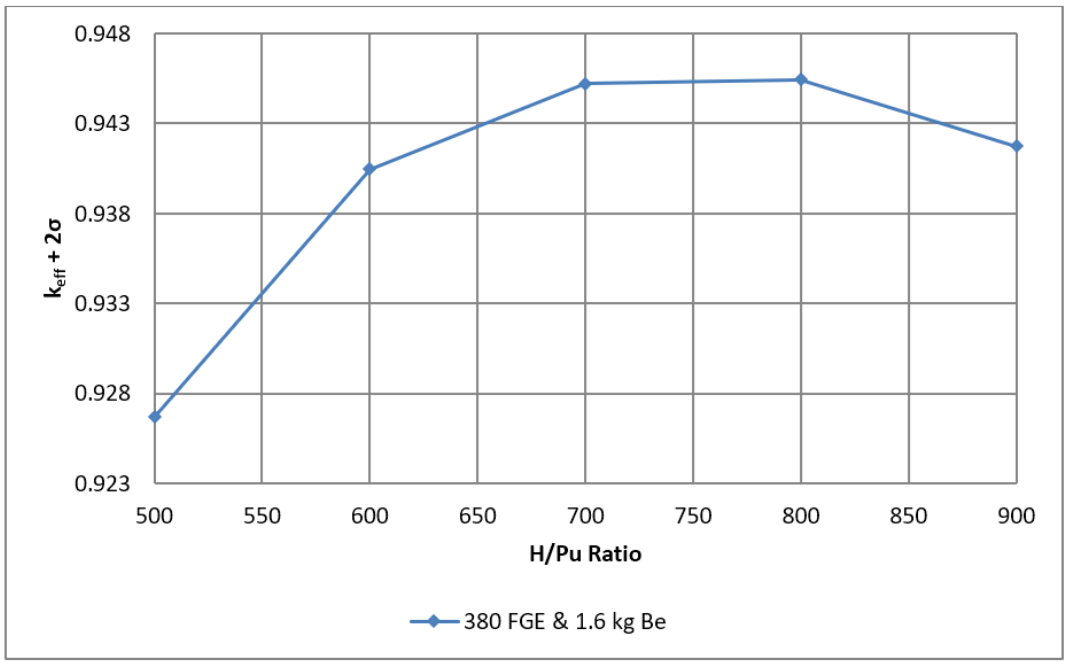

Figure G-3. CCO Array Reactivity

G.2.2 Two-Container Model

A two-container model is developed to evaluate the reactivity of the CCO in the event the fissile material in two adjacent containers was as close as possible to one another. The geometry stacks two CCOs on top of each other surrounded by a large reflector made of concrete, salt, or MgO. The fissile material is modeled in a cylindrical source mixed with 75% water and 25% polyethylene. The fissile material is placed as close together as possible with the material in the bottom CCO placed at the top of the CCC and the material of the top CCO placed at the bottom the CCC. A 1.6 kilogram solid mass of Be is placed under the lower fissile material region and on top of the upper fissile material region. Figure G-4 shows the two-container model surrounded by the MgO reflector. Table G-5 and Figure G-5 show the results of the two-container model configurations with MgO as the reflector because the MgO case was the most reactive. However, k_{eff} in the two-container configuration is lower than in the array configuration and all results are less than the USL.

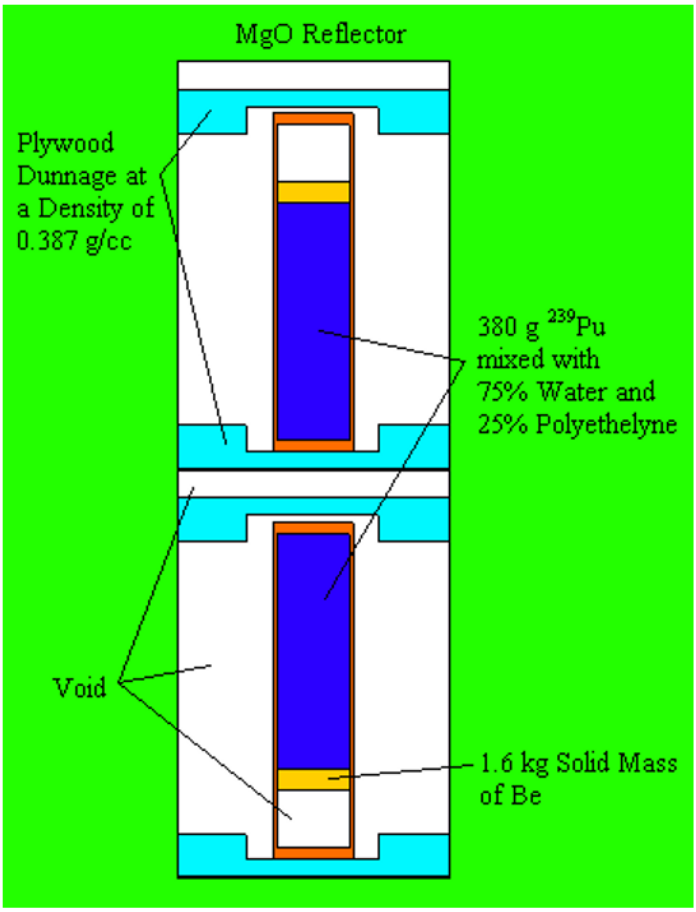

Figure G-4. Two-Container Model with MgO Reflector

Table G-5. MCNP5 Results for Two-Container Model

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
300	0.70407	0.00088	0.70583	d2mgo300hx
400	0.72058	0.00094	0.72246	d2mgo400hx
500	0.72368	0.00091	0.72550	d2mgo500hx
600	0.72072	0.00089	0.72250	d2mgo600hx
700	0.71297	0.00081	0.71459	d2mgo700hx
800	0.70157	0.00081	0.70319	d2mgo800hx
900	0.68854	0.00076	0.69006	d2mgo900hx

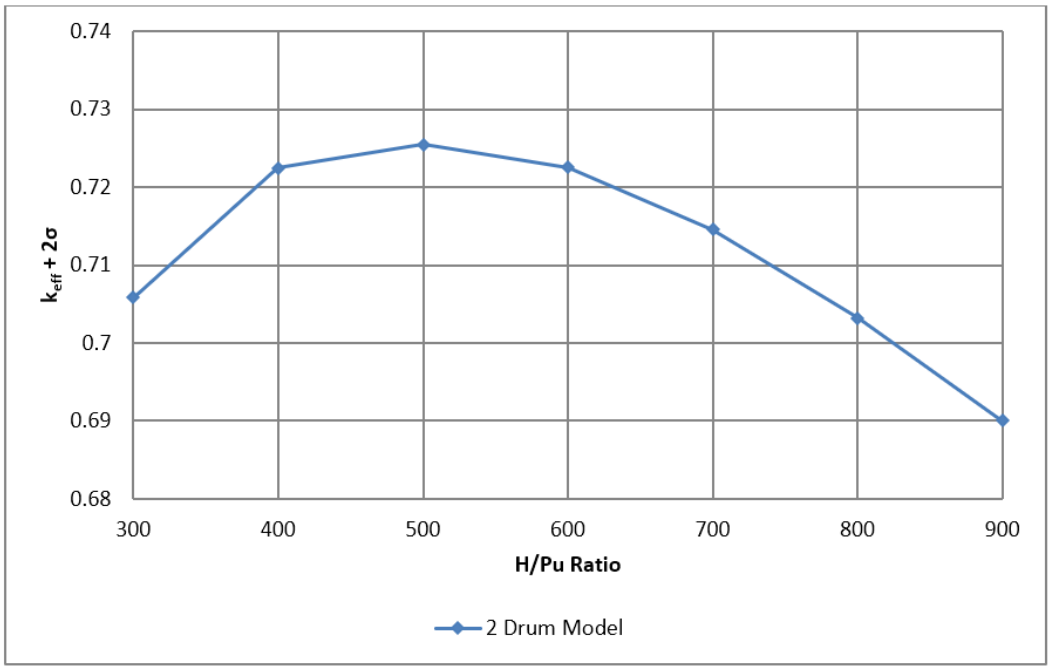

Figure G-5. Two-Container Reactivity

G.3 MCNP5 Contingency Models

To ensure a conservative bound on the analysis, different contingency conditions were evaluated for the underground array configuration of the CCO. Specifically, an overstacking event, an overbatch event, a roof fall event, a collision event, and water intrusion into the drums were considered. All contingency models were considered with MgO stacked on top of the waste containers.

G.3.1 CCO Array Overstack Model

In considering overstacking events, it is important to note that although WIPP panel heights were designed to accommodate three layers of waste containers, ground control safety constraints have resulted in areas of the disposal rooms being mined to a height greater than 13 feet. As a result, it is possible to stack greater than three tiers high. This contingency model uses the waste configuration from the normal array model with a 4th tier added to the stack and MgO placed on top of the array. All models for this contingency were below the USL of 0.96 and the results are shown in Table G-6 and Figure G-6.

Table G-6. MCNP5 Results for Overstacking Contingency

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
600	0.94924	0.00067	0.95058	u4ts600hx380fge
700	0.95648	0.00066	0.95780	u4ts700hx380fge
750	0.95782	0.00058	0.95898	u4ts750hx380fge
800	0.95771	0.00061	0.95893	u4ts800hx380fge
900	0.95385	0.00063	0.95511	u4ts900hx380fge

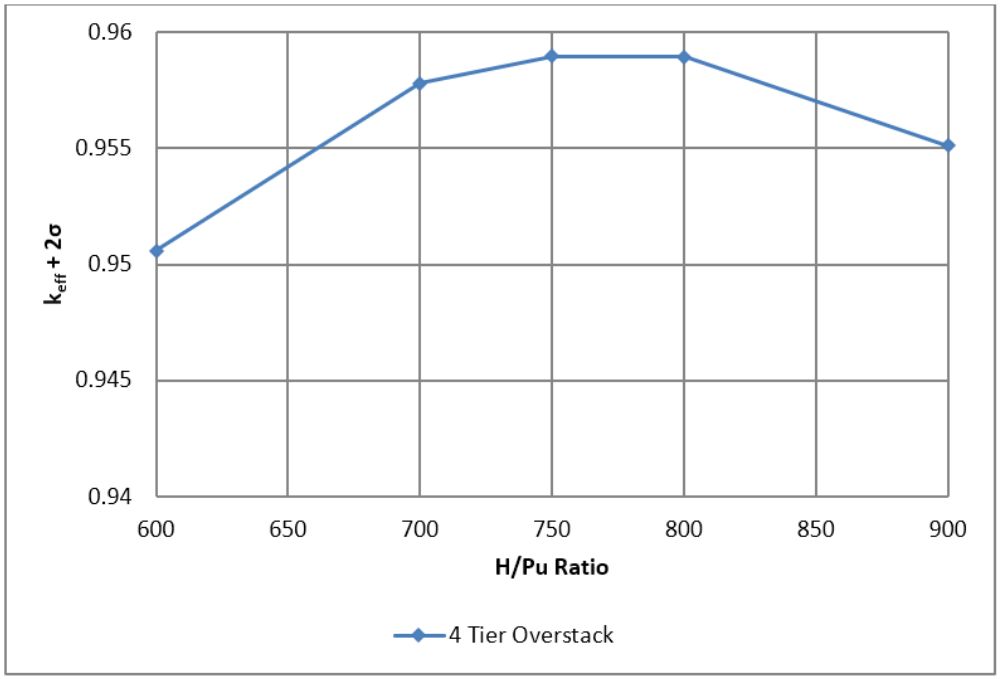

Figure G-6. Four-Tier Overstack CCO Array Reactivity

G.3.2 CCO Array Overbatch Model

Overbatch scenarios in the CCOs were evaluated with 1.5 and 1.25 times the maximum FGE loading for the CCC in the center drum of the center tier of every 7-pack stack. Two overbatch scenarios were considered because the lower mass allows for a higher H/Pu ratio in the fissile mixture in the drum. The normal drums in this scenario are loaded with 380 FGE at an H/Pu ratio of 800 as this was found to be the most reactive moderation level in Section G.2.1. To model the maximum H/Pu ratio possible in an overbatch scenario, the 475 FGE 700 H/Pu case and the 570 FGE 600 H/Pu case have less Be in the CCC than normal. Because the 475 FGE 700 H/Pu case continued to trend upwards, as shown in Figure G-7, two extra cases were performed to ensure the configuration remained subcritical. The 475 FGE 690 H/Pu ratio represents the maximum H/Pu ratio possible while maintaining 1.6 kilograms of beryllium in the CCC. The 475 FGE 745 H/Pu ratio represents the maximum H/Pu ratio possible without any Be in the CCC. The results for all these models stay below the USL of 0.96 as shown in Table G-7 and Figure G-7.

Table G-7. MCNP5 Results for Overbatch CCO Contingency

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Be Mass/CCO [kg]	Filename
475 FGE Overbatch					
400	0.94566	0.00061	0.94688	1.600	uob800hx475fge400hx
500	0.94649	0.00064	0.94777	1.600	uob800hx475fge500hx
600	0.94799	0.00068	0.94935	1.600	uob800hx475fge600hx
690	0.94958	0.00060	0.95078	1.600	uob800kx475fge690hx
700	0.94838	0.00064	0.94966	1.465	uob800hx475fge700hx
745	0.94785	0.00061	0.94907	0.000	uob800hx475fge745hx
570 FGE Overbatch					
300	0.94709	0.00065	0.94839	1.600	uob800hx570fge300hx
400	0.94821	0.00066	0.94953	1.600	uob800hx570fge400hx
500	0.95180	0.00060	0.95300	1.600	uob800hx570fge500hx
600	0.95089	0.00062	0.95213	0.826	uob800hx570fge600hx

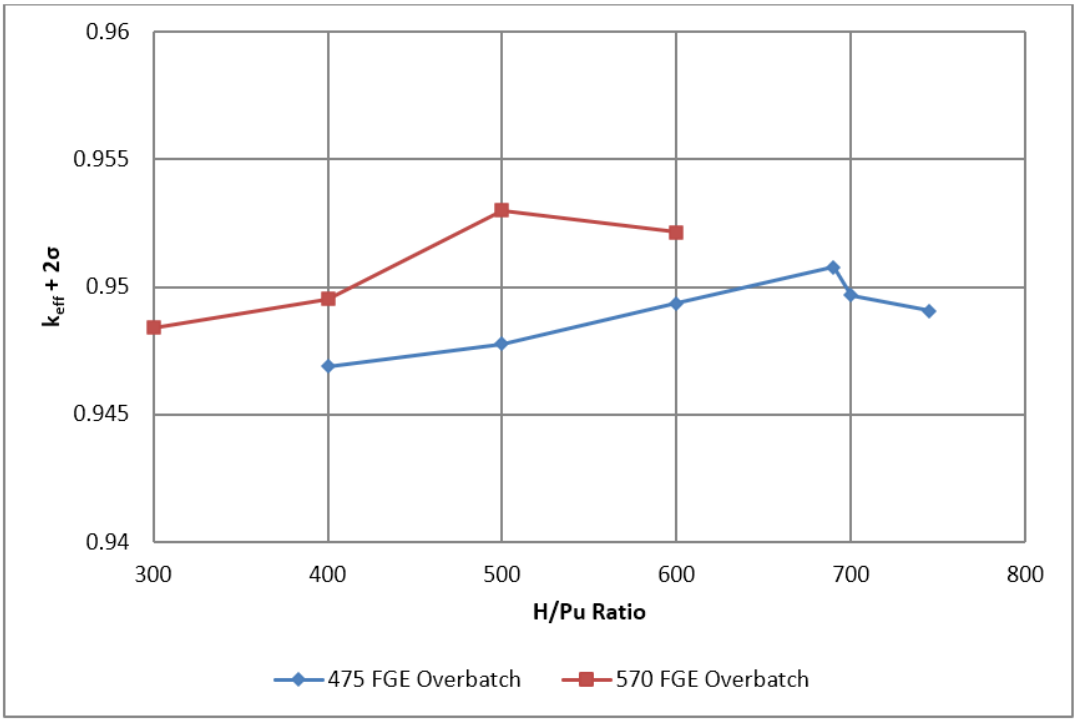

Figure G-7. Overbatch Array Reactivity

G.3.3 CCO Array Flooded Drum Model

This contingent condition simulates an abnormal state where the CCOs contain an excess of liquid in the void dunnage as a result of generator site error or water intrusion into the container. The array is modeled

as three tiers of 7-packs with the void outside of the CCC flooded with water as shown in Figure G-8. To show the reactivity change due to gradual water intrusion over time, the worst-case H/Pu ratio from Table G-4 was used in simulations where the drums where partially filled to different heights with water. Table G-8 and Figure G-9 show the reactivity of the array as the void outside of the CCC is filled with water to 25, 50, 75 and 100 percent of the volume. This simulates the intrusion of water into the containers and shows that reactivity decreases as water levels increase in the drums keeping all values below the USL of 0.96.

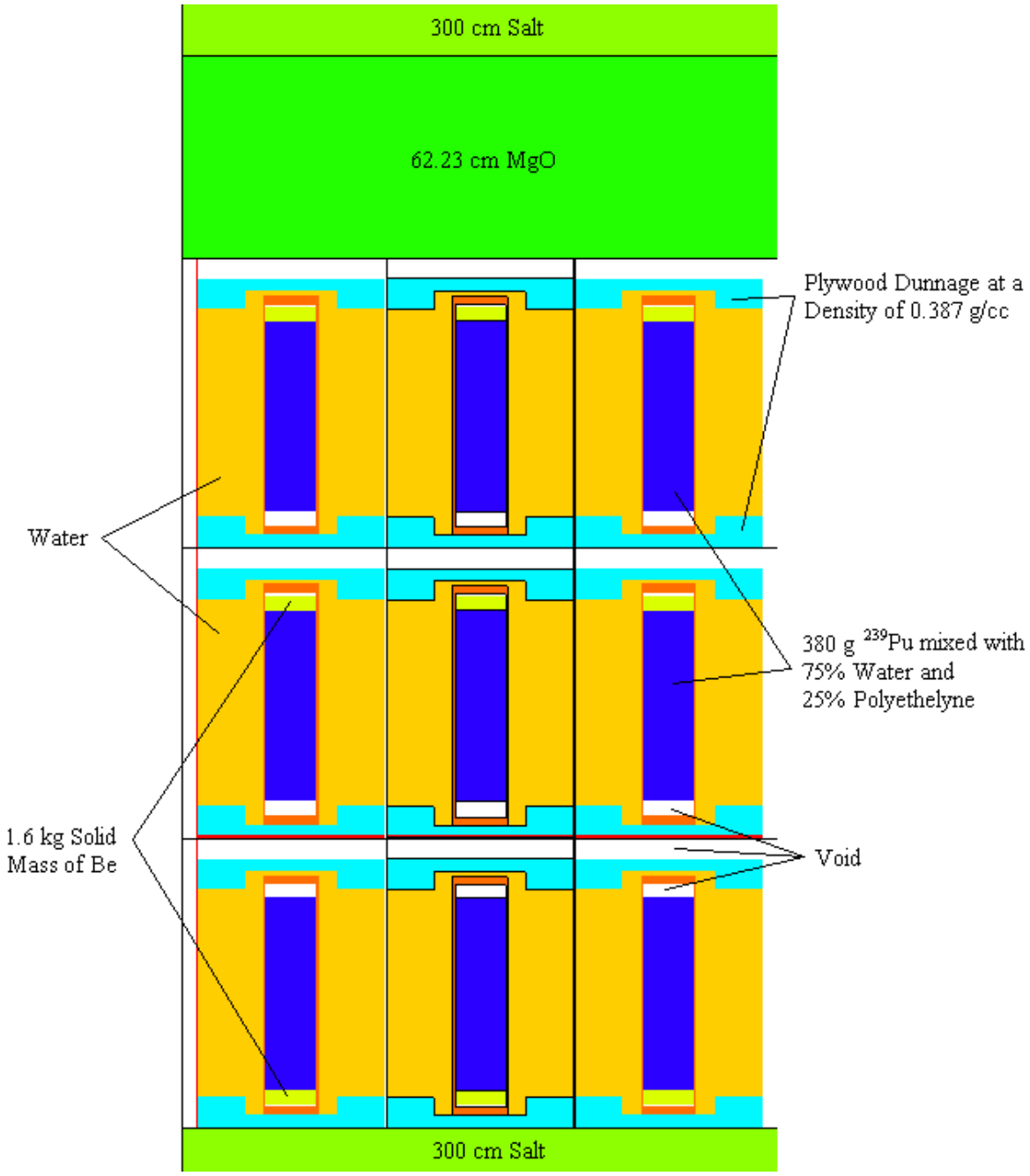

Figure G-8. Flooding Contingency Configuration for the CCO Container

Table G-8. MCNP5 Results of Flood Fill Levels in CCO

H/Pu Ratio	Flood %	k_{eff}	σ	k_{eff} + 2σ	Filename
800	0	0.94421	0.00062	0.94545	hx800mgo380fge
800	25	0.82624	0.00075	0.82774	u25fl800hx380fge
800	50	0.76963	0.00087	0.77137	u50fl800hx380fge
800	75	0.74746	0.00069	0.74884	u75fl800hx380fge
800	100	0.74894	0.00083	0.75060	ufl800hx380fge

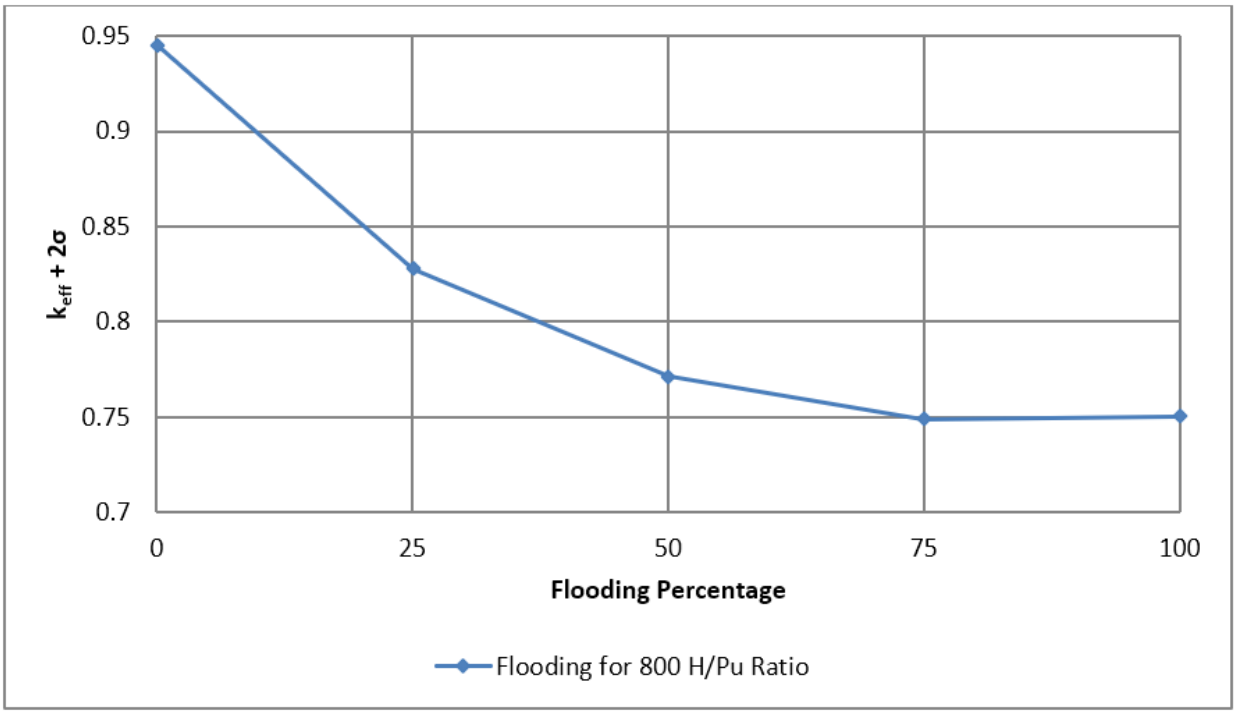

Figure G-9. Reactivity of Flooding Barrels

G.3.4 Impact of 41-ton Forklift into Waste Face Model

This contingency simulates an accident condition where the 41-ton waste handling forklift loaded with the facility cask impacts an array of CCOs in the underground. To simulate the effects of a collision with the waste face, some of the air volume within the CCO is expelled deforming the drums to 90% of their initial volume. This value is based on the damage ratio given in DOE-STD-5506-2007 for a vehicle collision impact. The scenario is modeled with three of the reduced size 7-packs stacked on top of each other and infinitely reflected on five sides. The sixth side has a slab of lead 200 cm thick in front of it to simulate the facility cask as shown in Figure G-10. The lead composition is taken from Table 5-6.

The results of this contingency remained under the USL of 0.96 and can be seen in Table G-9 and Figure G-11. Thus, a criticality accident from a loss of interaction control caused by the impact of a large object, such as a 41-ton forklift, with an array of CCOs is not credible.

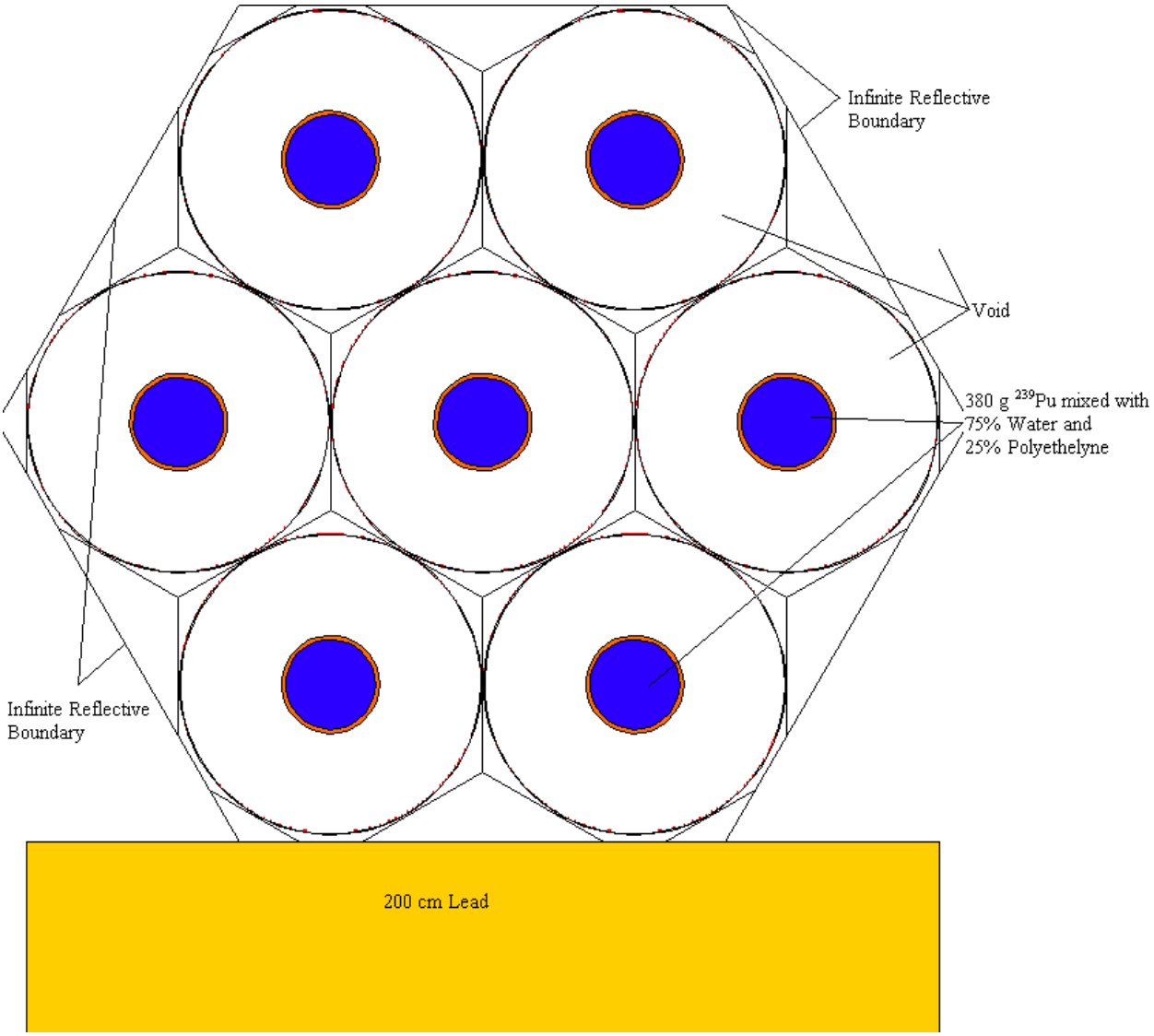

Figure G-10. Top View Model of the Impact Contingency of the 41-Ton Forklift Impacting an Array of CCOs

Table G-9. MCNP5 Results for 41-Ton Forklift Impact Contingency

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
500	0.93414	0.00085	0.93584	urhfl500hx380fge
600	0.94765	0.00082	0.94929	urhfl600hx380fge
700	0.95212	0.00076	0.95364	urhfl700hx380fge
800	0.95153	0.00071	0.95295	urhfl800hx380fge
900	0.94609	0.00077	0.94763	urhfl900hx380fge

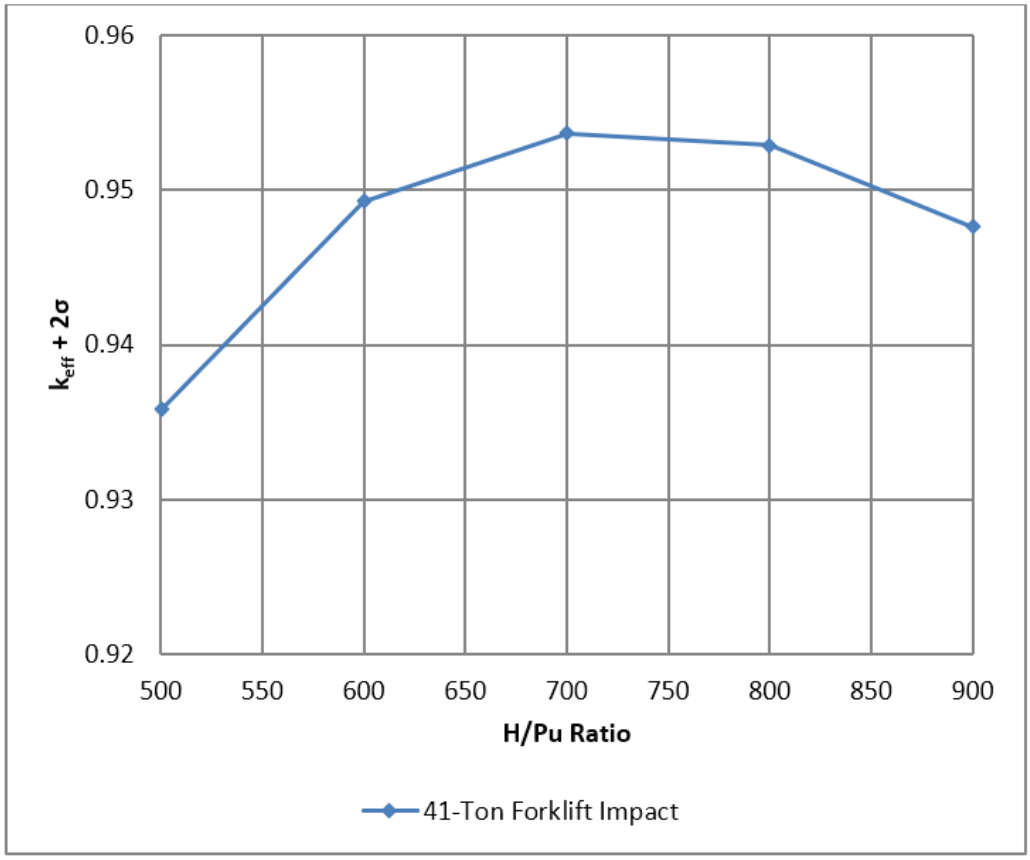

Figure G-11. 41-Ton Forklift Impact Reactivity

G.3.5 Roof Fall Model

This contingency simulates a collapse of the salt roof in the underground onto an infinite array of waste. The waste is postulated to be crushed such that the plywood at the bottom of the bottom tier drum will be sheared off, the voids between the drums are flattened and the top plywood dunnage plates will be sheared off and crushed as shown in Figure G-12. The roof fall is also considered to have ruptured the MgO, therefore the 62.23 cm that would normally be MgO has been replaced with salt. Crushing the voids and the top plywood dunnage plates results in a 4.46 inches compaction in the middle and top row and crushing the void, the top and bottom plywood dunnage in a 5.96 in compaction in the bottom row resulting in a total compaction of 14.88 inches. The plywood dunnage at the top is in the model, however the top 2 plates are now modeled as rings and begin at the top of the CCC. The results for this contingency remain under the USL as shown in Table G-10 and Figure G-13. Thus, a criticality accident from a loss of interaction control caused by a roof fall is not credible.

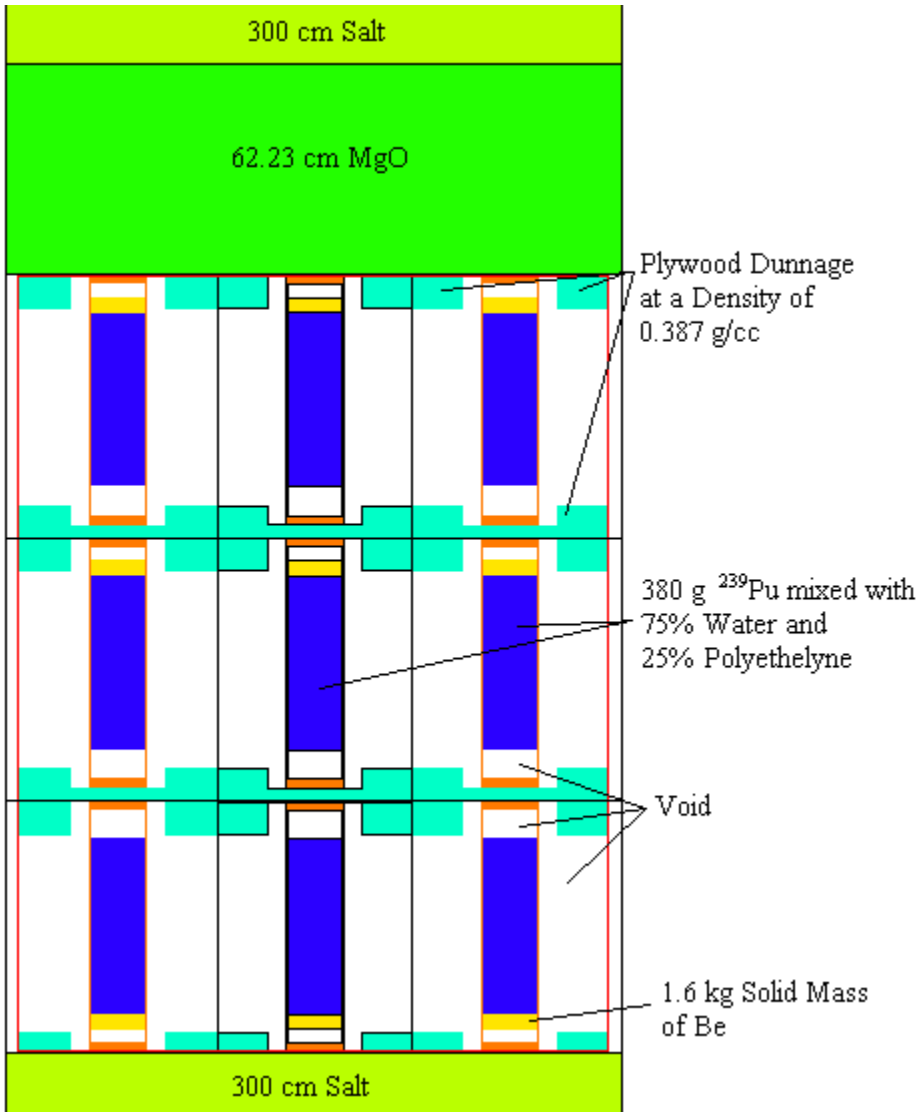

Figure G-12. Roof Fall Array Configuration

Table G-10. MCNP5 Results for Roof Fall Contingency

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
600	0.95250	0.00084	0.95418	uugrf600hx380fge
700	0.95729	0.00062	0.95853	uugrf700hx380fge
750	0.95760	0.00048	0.95856	uugrf750hx380fge
800	0.95610	0.00080	0.95770	uugrf800hx380fge
900	0.95234	0.00075	0.95384	uugrf900hx380fge

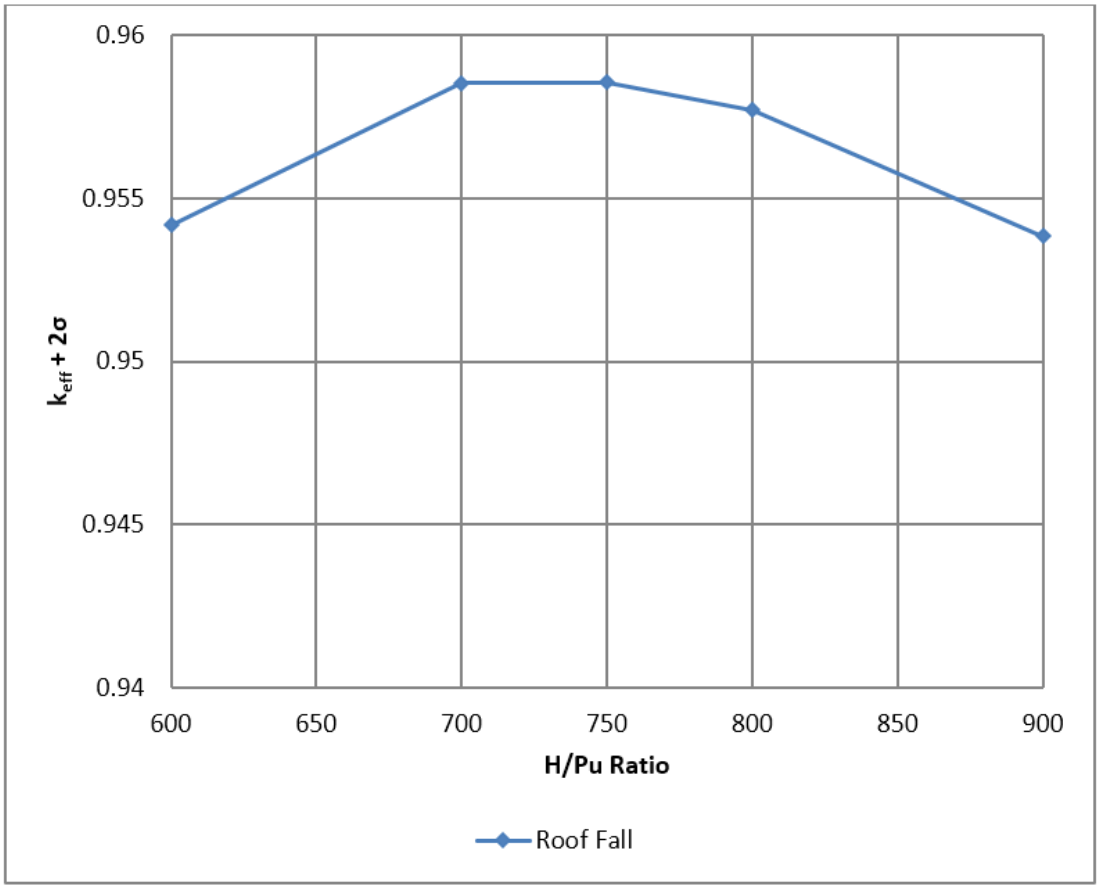

Figure G-13. Roof Fall Reactivity

G.4 Machine-Compacted Waste in CCOs

In the calculations performed above, the fissile material is moderated by a mixture of 25% polyethylene and 75% water (by volume) representative of direct loaded waste. As discussed in Section 6.2.1 of the *TRUPACT-II Safety Analysis Report* (DOE-CBFO 2020), a 25% volumetric packing fraction for polyethylene is used as a conservative value as it bounds the 13.6% packing fraction of polyethylene in manually compacted CH-TRU waste determined from physical testing. If the contents of the CCO are machine-compacted, the polyethylene packing fraction could exceed 25%. At the maximum packing fraction of 100% possible for machine-compacted waste, polyethylene would be the only moderator for the fissile material. Thus, if the polyethylene mass in machine-compacted waste is limited to the amount present in the non-compacted waste as analyzed above, the machine-compacted waste would have a significantly smaller H/Pu ratio from ignoring the water in the non-compacted fissile mixture. This would result in a lower reactivity because the fissile material is undermoderated while accounting for the fact that polyethylene is a more effective moderator than water. Thus, limiting the mass of plastic in machine-compacted waste in a CCO to less than what was evaluated for non-compacted waste will ensure the analysis of subcriticality in Sections G.2 and G.3 is bounding for machine-compacted waste.

The array cases and associated contingency models had the highest k_{eff} values and thus were used to calculate the amount of polyethylene modeled. The calculations in Table G-11 show that each of these cases contained more than 2,000 grams of polyethylene in each CCO. To align with the limit in the

TRUPACT-II SAR (DOE-CBFO 2020), each CCO of machine-compacted waste is limited to a maximum of 2000 grams of plastic.

Table G-11. Calculation of Polyethylene in Non-Compacted Waste Models

Case	FGE per CCO	Optimum H/Pu Ratio	^{239}Pu Concentration (g/L) [(a)]	Fissile Mix Volume (cm^3) [(b)]	^{239}Pu Volume (cm^3) [(c)]	Poly Volume (cm^3) [(d)]	Poly Mass (g) [(e)]
Normal Array Case	380	800	34.751	10934.9	19.1	2728.9	2518.8
Overstacking	380	750	37.229	10207.2	19.1	2547.0	2350.9
Overbatch	570	500	55.543	10262.3	28.7	2558.4	2361.4
Forklift Upset	380	700	39.706	9570.3	19.1	2387.8	2203.9
Roof Fall	380	750	37.229	10207.2	19.1	2547.0	2350.9

(a) From Table 5-4 directly or interpolated.

(b) FGE / ^{239}Pu Concentration × 1000 cm^3/L.

(c) FGE / 19.848 g ^{239}Pu/cm^3 from Section 5.2.1.

(d) (Fissile Mix Volume - ^{239}Pu Volume) × 25 volume % Poly in Moderator.

(e) Poly volume × 0.923 g Poly/cm^3 from Section 5.2.1.

G.5 Conclusions

This appendix demonstrates that the CCO waste containers will remain subcritical in the two-container configuration as well as in the underground repository array with the following limits:

- Maximum 380 FGE/CCO in non-compacted waste.
- Maximum 380 FGE/CCO in machine-compacted waste provided each CCO contains ≤ 2,000 grams of plastic.
- Less than or equal to 1 wt% special reflectors/CCO with non-compacted or machine-compacted waste.

G.6 References

DOE-CBFO, 2020. *TRUPACT-II Safety Analysis Report*, Revision 24, August 2020, U.S. Department of Energy, Carlsbad Field Office, Carlsbad, NM

WTS, 2012. Criticality Control Overpack, CCO-DWG-0001, Revision 1, September 2012, Washington TRU Solutions LLC, Carlsbad, NM.

AREVA, 2012. *Criticality Control Overpack Criticality Analysis for TRUPACT-II and HalfPACT*, 01937.01.M009-01, Revision 0, February 2012, AREVA Federal Services LLC.

RSICC, 2008. *Standard Materials for VisedX_22S*, MCNP5-1.51, stndrd.n.

DOE-STD-5506-2007, 2007. *Preparation of Safety Basis Documents for Transuranic (TRU) Waste Facilities*, April 2007, U.S. Department of Energy, Washington, D.C.

G.7 Sample MCNP5 Input File listings for Appendix G

G.7.1 MCNP5 Input File Listing for Infinite Array Case with MgO (Filename hx800mgo380fge)

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MCNPX Visual Editor Version 740X_23z
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c   CELL CARDS FOR 380 FGE CCO DRUMS
c
    1     1 -1.01303 -30 33 -34  u=1 $PU
    2     0          (-30 34 -32 ):(-30 -40 31 ) u=1
    3   264       -8 (-36 37 -38 )(30 :-31 :32 ) u=1 $CCC WALLS
    4     3  -0.387 (-17 8 -2 16 ):(-37 -16 8 ):(-10 15 -2 16 ):
            (-10 -16 14 ) u=1
    5    10  -1.848 -30 -33 40  u=1 $BE
    6     0          -14 -2 37 #1 #2 #3 #4 #5  u=1
    7   224   -3.93 (2 :18 :-8 )-4 6 -12  u=1
    8     0          (-2 -18 10 ) u=1
    9     0          4 :-6 :12  u=1
c
c   CELL CARDS FOR 380 FGE CCO DRUMS
c
   21     1 -1.01303 -30 33 -34  u=2 $PU
   22     0          (-30 -32 41 ):(-30 -33 31 ) u=2
   23   264       -8 (-36 37 -38 )(30 :-31 :32 ) u=2 $CCC WALLS
   24     3  -0.387 (-17 8 -2 16 ):(-37 -16 8 ):(-10 15 -2 16 ):
            (-10 -16 14 ) u=2
   25    10  -1.848 -30 -41 34  u=2 $BE
   26     0          -14 -2 37 #21 #22 #23 #24 #25  u=2
   27   224   -3.93 (2 :18 :-8 )-4 6 -12  u=2
   28     0          (-2 -18 10 ) u=2
   29     0          4 :-6 :12  u=2
c
c  CELL CARDS FOR HEXAGONAL 7 PACK
c
  112     0          -21 20 -22 25 -23 24 -27 26  u=4 lat=2 $ROW 1
            fill=-3:3 -3:3 0:2
       4 4 4 4 4 4 4  $ROW 1
        4 4 4 4 4 4 4  $ROW 2
         4 4 4 1 1 4 4  $ROW 3
          4 4 1 1 1 4 4  $ROW 4
           4 4 1 1 4 4 4  $ROW 5
            4 4 4 4 4 4 4  $ROW 6
             4 4 4 4 4 4 4  $ROW 7
       4 4 4 4 4 4 4  $ROW 1
        4 4 4 4 4 4 4  $ROW 2
         4 4 4 2 2 4 4  $ROW 3
          4 4 2 2 2 4 4  $ROW 4
           4 4 2 2 4 4 4  $ROW 5
            4 4 4 4 4 4 4  $ROW 6
             4 4 4 4 4 4 4  $ROW 7
```

```
      4 4 4 4 4 4 4  $ROW 1
       4 4 4 4 4 4 4  $ROW 2
        4 4 4 2 2 4 4  $ROW 3
         4 4 2 2 2 4 4  $ROW 4
          4 4 2 2 4 4 4  $ROW 5
           4 4 4 4 4 4 4  $ROW 6
            4 4 4 4 4 4 4  $ROW 7
  113     0         -61 60 -62 65 -63 64 -67 66  fill=4
c
c  CELL CARDS FOR MGO AND SALT LAYERS (MGO REMOVED BECAUSE WE NO LONGER
c  TAKE CREDIT FOR STACKING MGO ON TOP OF EVERY COLUM OF WASTE)
c
  114     8  -2.165 (53 :-66 )-61 60 -62 65 -63 64 50 -52
  115     7   -1.45 -61 60 -62 65 -63 64 67 -53
c
c  CELL CARDS FOR THE REST OF THE UNIVERSE
c
  116     0         -50 :52 :61 :-60 :62 :-65 :63 :-64

c
c  SURFACE CARDS FOR ALL DRUM SURFACES
c
    2        cz 28.575
    4        cz 28.696
    6        pz 0
    8        pz 0.121
   10        pz 82.671
   12        pz 88.9  $Top Outer Wall of Drum
   14        pz 78.861
   15        pz 73.146
   16        cz 14
   17        pz 9.646
   18        pz 88.779
c
c  SURFACE CARDS FOR THE CCO 280 FGE DRUMS
c
   30        cz 7.7026
   31        pz 6.471
   32        pz 74.9062
   33        pz 11.3553  $Bottom tier lowewr fuel line H/X Variable
   34        pz 70.0219  $Bottom tier upper fuel line H/X Variable
   36        cz 8.4138
   37        pz 3.931
   38        pz 77.44622
   39        cz 6.5408  $Cylinder for H/D = 1
   40        pz 6.7102  $BE under fuel
   41        pz 74.667  $BE on top of fuel/upper fuel line
c   42        pz 25.0742  $Upper tier lower fuel line
c
c  SURFACE CARDS FOR THE HEX 7-PACK
c
   20        px -28.75
   21        px 28.75
   22         p 1 1.7321 0 57.5
   23         p -1 1.7321 0 57.5
   24         p -1 1.7321 0 -57.5
```

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   25         p 1 1.7321 0 -57.5
   26        pz 0
   27        pz 88.9
c
c  SURFACE CARDS FOR MGO AND SALT
c
   50        pz -300
   52        pz 628.93
   53        pz 328.93
c
c  SURFACE CARDS FOR 7-PACK INFINITE ARRAY
c
  *60        py -78.5
  *61        py 78.5
  *62         p 1.7321 1 0 157
  *63         p 1.7321 -1 0 157
  *64         p 1.7321 -1 0 -157
  *65         p 1.7321 1 0 -157
   66        pz 0
   67        pz 266.7

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kcode 5000 1.000000 250 550
ksrc  -58.000000 0.000000 41.000000
      -30.000000 -50.000000 41.000000
      -30.000000 50.000000 41.000000
      0.000000   0.000000 41.000000
      58.000000 0.000000 41.000000
      30.000000 -50.000000 41.000000
      30.000000  50.000000 41.000000
     -58.000000 0.000000 124.000000
      -30.000000 -50.000000 124.000000
      -30.000000 50.000000 124.000000
      0.000000   0.000000 124.000000
      58.000000 0.000000 124.000000
      30.000000 -50.000000 124.000000
      30.000000  50.000000 124.000000
     -58.000000 0.000000 206.000000
      -30.000000 -50.000000 206.000000
      -30.000000 50.000000 206.000000
      0.000000   0.000000 206.000000
      58.000000 0.000000 206.000000
      30.000000 -50.000000 206.000000
      30.000000  50.000000 206.000000
c
c MATERIAL CARDS
c
c
c PU-H2O-POLY FOR THE FISSILE MASS CONTAINING 380 GRAMS OF PU
c
m1    94239.60c     -0.034304
      1001.60c      -0.115272 6000.60c       -0.19407 8016.60c      -0.656354
c
```

```
c  74% H2O - 25% POLY MODERATOR MIXTURE
c
m2    1001.60c              4
      6000.60c              1 8016.60c             1
c
c  CANE FIBERBOARD DUNNAGE
c
m3    6000.60c              6
      1001.60c             10 8016.60c             5
c
c  MGO LAYER
c
m7    12000.60c           0.5
      8016.60c            0.5
c
c  SALT REFLECTOR
c
m8    11023.60c           0.5
      17000.60c           0.5
c
c  BE REFLECTOR
c
m10   4009.60c             -1
c
c  SS-304 FOR MAKING THE CCC
c
m264  6000.60c        -0.0003  $SS-304,SS-304L
      14000.60c        -0.005 15031.60c     -0.000225 16000.60c      -0.00015
      24050.60c      -0.00793 24052.60c     -0.159031 24053.60c     -0.018378
      24054.60c     -0.004661 25055.60c         -0.01 26054.60c     -0.039996
      26056.60c     -0.644764 26057.60c     -0.015026 26058.60c     -0.002039
      28058.60c      -0.06234 28060.60c     -0.024654 28061.60c     -0.001085
      28062.60c     -0.003504 28064.60c     -0.000917
c
c  CARBON STEEL 55 GALLON DRUM WALLS
c
m224  6000.60c        -0.0006  $carbon steel
      25055.60c       -0.0035 26054.60c     -0.056755 26056.60c      -0.91493
      26057.60c     -0.021323 26058.60c     -0.002893
imp:n   1 21r        0             $ 1, 116
mt1       LWTR.01T  POLY.01T
mt2       LWTR.01T  POLY.01T
mt10      BE.01T
print
c
c  PRINT TO MCTAL FILE
c
prdmp 2J 1
```

G.7.2 MCNP5 Input File Listing for Overbatch Array Case (Filename uob800hx570fge500hx)

```
MCNPX Visual Editor Version 740X_23z
```

```
c
c   CELL CARDS FOR 380 FGE CCO DRUMS
c
    1     1 -1.01303 -30 33 -34  u=1 $PU
    2     0          (-30 34 -32 ):(-30 -40 31 ) u=1
    3   264       -8 (-36 37 -38 )(30 :-31 :32 ) u=1 $CCC WALLS
    4     3  -0.387 (-17 8 -2 16 ):(-37 -16 8 ):(-10 15 -2 16 ):
          (-10 -16 14 ) u=1
    5    10  -1.848 -30 -33 40  u=1 $BE
    6     0         -14 -2 37 #1 #2 #3 #4 #5  u=1
    7   224   -3.93 (2 :18 :-8 )-4 6 -12  u=1
    8     0         (-2 -18 10 ) u=1
    9     0         4 :-6 :12  u=1
c
c   CELL CARDS FOR 380 FGE CCO DRUMS
c
   21     1 -1.01303 -30 33 -34  u=2 $PU
   22     0          (-30 -32 41 ):(-30 -33 31 ) u=2
   23   264       -8 (-36 37 -38 )(30 :-31 :32 ) u=2 $CCC WALLS
   24     3  -0.387 (-17 8 -2 16 ):(-37 -16 8 ):(-10 15 -2 16 ):
          (-10 -16 14 ) u=2
   25    10  -1.848 -30 -41 34  u=2 $BE
   26     0         -14 -2 37 #21 #22 #23 #24 #25  u=2
   27   224   -3.93 (2 :18 :-8 )-4 6 -12  u=2
   28     0         (-2 -18 10 ) u=2
   29     0         4 :-6 :12  u=2
c
c   CELL CARDS FOR DOUBLEBATCHED CCO DRUMS
c
   11    11 -1.0328 -30 83 -84  u=3 $PU
   12     0         (-30 85 -32 ):(-30 -83 31 ) u=3
   13   264       -8 (-36 37 -38 )(30 :-31 :32 ) u=3 $CCC WALLS
   14     3 -0.387 (-17 8 -2 16 ):(-37 -16 8 ):(-10 15 -2 16 ):
          (-10 -16 14 ) u=3
   15    10  -1.848 -30 84 -85  u=3 $BE
   16     0         -14 -2 37 #11 #12 #13 #14 #15  u=3
   17   224   -3.93 (2 :18 :-8 )-4 6 -12  u=3
   18     0         (-2 -18 10 ) u=3
   19     0         4 :-6 :12  u=3
c
c  CELL CARDS FOR HEXAGONAL 7 PACK
c
  112     0         -21 20 -22 25 -23 24 -27 26  u=4 lat=2 $ROW 1
            fill=-3:3 -3:3 0:2
       4 4 4 4 4 4 4  $ROW 1
        4 4 4 4 4 4 4  $ROW 2
         4 4 4 1 1 4 4  $ROW 3
          4 4 1 1 1 4 4  $ROW 4
           4 4 1 1 4 4 4  $ROW 5
            4 4 4 4 4 4 4  $ROW 6
             4 4 4 4 4 4 4  $ROW 7
       4 4 4 4 4 4 4  $ROW 1
        4 4 4 4 4 4 4  $ROW 2
         4 4 4 2 2 4 4  $ROW 3
          4 4 2 3 2 4 4  $ROW 4
           4 4 2 2 4 4 4  $ROW 5
```

```
           4 4 4 4 4 4 4  $ROW 6
            4 4 4 4 4 4 4  $ROW 7
      4 4 4 4 4 4 4  $ROW 1
       4 4 4 4 4 4 4  $ROW 2
        4 4 4 2 2 4 4  $ROW 3
         4 4 2 2 2 4 4  $ROW 4
          4 4 2 2 4 4 4  $ROW 5
           4 4 4 4 4 4 4  $ROW 6
            4 4 4 4 4 4 4  $ROW 7
  113     0         -61 60 -62 65 -63 64 -67 66  fill=4
c
c  CELL CARDS FOR MGO AND SALT LAYERS (MGO REMOVED BECAUSE WE NO LONGER
c  TAKE CREDIT FOR STACKING MGO ON TOP OF EVERY COLUM OF WASTE)
c
  114     8  -2.165 (53 :-66 )-61 60 -62 65 -63 64 50 -52
  115     7   -1.45 -61 60 -62 65 -63 64 67 -53
c
c  CELL CARDS FOR THE REST OF THE UNIVERSE
c
  116     0         -50 :52 :61 :-60 :62 :-65 :63 :-64

c
c  SURFACE CARDS FOR ALL DRUM SURFACES
c
    2        cz 28.575
    4        cz 28.696
    6        pz 0
    8        pz 0.121
   10        pz 82.671
   12        pz 88.9  $Top Outer Wall of Drum
   14        pz 78.861
   15        pz 73.146
   16        cz 14
   17        pz 9.646
   18        pz 88.779
c
c  SURFACE CARDS FOR THE CCO 280 FGE DRUMS
c
   30        cz 7.7026
   31        pz 6.471
   32        pz 74.9062
   33        pz 11.3553  $Bottom tier lowewr fuel line H/X Variable
   34        pz 70.0219  $Bottom tier upper fuel line H/X Variable
   36        cz 8.4138
   37        pz 3.931
   38        pz 77.44622
   39        cz 6.5408  $Cylinder for H/D = 1
   40        pz 6.7102  $BE under fuel
   41        pz 74.667  $BE on top of fuel/upper fuel line
c   42        pz 25.0742  $Upper tier lower fuel line
c
c  UPSET CONDITION FISSILE MATERIAL BOUNDARYS
c
   83        pz 13.1597  $Bottom H/X Upset Variable
   84        pz 68.2175  $Top H/X Upset Variable
   85        pz 72.8626  $BE for upset Variable
```

```
c
c  SURFACE CARDS FOR THE HEX 7-PACK
c
   20        px -28.75
   21        px 28.75
   22         p 1 1.7321 0 57.5
   23         p -1 1.7321 0 57.5
   24         p -1 1.7321 0 -57.5
   25         p 1 1.7321 0 -57.5
   26        pz 0
   27        pz 88.9
c
c  SURFACE CARDS FOR MGO AND SALT
c
   50        pz -300
   52        pz 628.93
   53        pz 328.93
c
c  SURFACE CARDS FOR 7-PACK INFINITE ARRAY
c
  *60        py -78.5
  *61        py 78.5
  *62         p 1.7321 1 0 157
  *63         p 1.7321 -1 0 157
  *64         p 1.7321 -1 0 -157
  *65         p 1.7321 1 0 -157
   66        pz 0
   67        pz 266.7

c
c    DATA CARDS
c
mode  n
kcode 5000 1.000000 250 550
ksrc  -58.000000 0.000000 41.000000
      -30.000000 -50.000000 41.000000
      -30.000000 50.000000 41.000000
      0.000000   0.000000 41.000000
      58.000000 0.000000 41.000000
      30.000000 -50.000000 41.000000
      30.000000  50.000000 41.000000
     -58.000000 0.000000 124.000000
      -30.000000 -50.000000 124.000000
      -30.000000 50.000000 124.000000
      0.000000   0.000000 124.000000
      58.000000 0.000000 124.000000
      30.000000 -50.000000 124.000000
      30.000000  50.000000 124.000000
     -58.000000 0.000000 206.000000
      -30.000000 -50.000000 206.000000
      -30.000000 50.000000 206.000000
      0.000000   0.000000 206.000000
      58.000000 0.000000 206.000000
      30.000000 -50.000000 206.000000
      30.000000  50.000000 206.000000
c
```

```
c MATERIAL CARDS
c
c
c PU-H2O-POLY FOR THE FISSILE MASS CONTAINING 380 GRAMS OF PU
c
m1    94239.60c     -0.034304
      1001.60c      -0.115272 6000.60c       -0.19407 8016.60c      -0.656354
c
c  74% H2O - 25% POLY MODERATOR MIXTURE
c
m2    1001.60c              4
      6000.60c              1 8016.60c             1
c
c  PLYWOOD DUNNAGE
c
m3    6000.60c              6
      1001.60c             10 8016.60c             5
c
c  MGO LAYER
c
m7    12000.60c           0.5
      8016.60c            0.5
c
c  SALT REFLECTOR
c
m8    11023.60c           0.5
      17000.60c           0.5
c
c  BE REFLECTOR
c
m10   4009.60c             -1
c
c PU-H2O-POLY FOR THE OVERBATCH DRUM
c
m11   94239.60c     -0.053779
      1001.60c      -0.112947 6000.60c      -0.190156 8016.60c      -0.643117
c
c  SS-304 FOR MAKING THE CCC
c
m264  6000.60c        -0.0003  $SS-304,SS-304L
      14000.60c        -0.005 15031.60c     -0.000225 16000.60c      -0.00015
      24050.60c      -0.00793 24052.60c     -0.159031 24053.60c     -0.018378
      24054.60c     -0.004661 25055.60c         -0.01 26054.60c     -0.039996
      26056.60c     -0.644764 26057.60c     -0.015026 26058.60c     -0.002039
      28058.60c      -0.06234 28060.60c     -0.024654 28061.60c     -0.001085
      28062.60c     -0.003504 28064.60c     -0.000917
c
c  CARBON STEEL 55 GALLON DRUM WALLS
c
m224  6000.60c        -0.0006  $carbon steel
      25055.60c       -0.0035 26054.60c     -0.056755 26056.60c      -0.91493
      26057.60c     -0.021323 26058.60c     -0.002893
imp:n   1 30r        0             $ 1, 116
mt1       LWTR.01T  POLY.01T
mt2       LWTR.01T  POLY.01T
mt10      BE.01T
```

```
mt11      LWTR.01T  POLY.01T
print
c
c  PRINT TO MCTAL FILE
c
prdmp 2J 1
```

Appendix H Shielded Containers

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Note: Appendix H is unaffected by Revision 8 and no changes were made from the previous revision. Original signatures are on file with WIPP-016 Revision 7.

Note: An extent of condition was performed to Revision 7 of this NCSE to review all established limits, assumptions, and judgements. It was identified that the excess liquid in waste containers contingency models were inadvertently omitted from the NCSE in Revision 7 when the analysis for the Shielded Containers were moved from Appendix A to Appendix H. This analysis will be reincorporated into a future revision of this NCSE.

Analyst in Training NCS Engineer	N. Dickes	Date
Analyst Senior NCS Engineer	S. L. Larson	Date
Peer Reviewer Senior NCS Engineer	W. D. Newmyer	Date

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Introduction

There are five shielded container configurations that can be used as an alternative to RH canisters. These containers are considered in this NCSE since the shielding will reduce the dose rate to levels appropriate for contact-handling such that these containers will be emplaced in the CH array. Shielded containers are emplaced in the interstitial spaces among the CH waste in the disposal room and are not expected to be stacked more to two high. Shielded containers are approved for both machine and non-machine compacted waste forms that contain less than or equal to 1 wt% special reflectors. Calculations in this appendix were performed with MCNP 6.2, and thus the applicable USL is 0.9659 as discussed in Section 4.2.2.

H.1 Shielded Container Configurations

The shielded container configurations evaluated in this analysis consist of the SC-30G1, SC-30G2, SC-30G3, SC-55G1, and the SC-55G2. The shielded containers are shipped to WIPP in assemblies of three, two, or single container(s), depending on the shielded container type, in the HalfPACT shipping container (*HALFPACT Safety Analysis Report,* Rev. 8, February 2022). The five shielded container designs are described below. Additional details can be found in Sections 2.9.10 through 2.9.15 of the *Contact-Handled Transuranic Waste Authorized Methods for Payload Control (CH-TRAMPAC*, Rev. 6, February 2022).

Without the lead shielding, a Shielded Container would be bounded by a 55-gallon drum. Both containers have a 200 FGE limit and as shown in the subsections below, all five shielded container designs have a larger outer radius than the 11.2978-inch outer radius given in Table 2-1. However, the Shielded Containers are explicitly analyzed in this Appendix because lead is a very good reflector. Thus, the lead wall thickness is maximized in the MCNP6.2 models as discussed below. The lead is poured between two thin sheets of steel to construct the shielded container body. The steel sheets are modeled at their nominal thickness. The SC-55G2 wall does not contain lead but is constructed of thick steel, which is also a very good reflector at that thickness, and its thickness is also maximized.

H.1.1 Shielded Container SC-30G1

The SC-30G1 has a cylindrical sidewall with nominal 1-inch-thick lead shielding between double-walled steel shells as shown in Figure H-1. The external wall is 11-guage steel and the internal wall is 7-guage steel, with the thicknesses given on Drawing SCA-DWG-0001. The upper and lower lid of the container is carbon steel approximately 3 inches thick. The SC-30G1 modeled dimensions, as summarized in Table H-1, are taken from SAR Drawing 163-008 Revision 4. Tolerances are applied in a manner that maximizes the lead shielding thickness per the discussion in Section H.1. Nominal values were also evaluated for this container type for comparison.

Table H-1. Modeled SC-30G1 Shielded Container Dimensions

Dimension	Nominal Drawing Value (in.)[a]	Drawing MAX/MIN Value (in.)	Modeled Value (in.)	Modeled Value (cm)
Outer Height	35.750	N/A	35.750	90.8050
Inner Height	29.750	N/A	29.750	75.5650
Outer Diameter	23.000	23.180	23.180	58.8772
Inner Diameter	20.375	20.250	20.250	51.4350
Lead Thickness	1.000	N/A	1.166	2.9616
Outer Lead Diameter	22.760	N/A	22.940	58.2422
Inner Lead Diameter	20.733	N/A	20.608	52.3443
Bottom Lid Thickness	3.000	N/A	3.000	7.620
Upper Lid Thickness	3.000	N/A	3.000	7.620
Lead Wall Height	0.179	0.179	0.179	0.45466
Inner steel wall thickness	0.120	0.120	0.120	0.3048
Outer steel wall thickness	35.750	N/A	35.750	90.8050

[a] Values used in “Nominal” Model

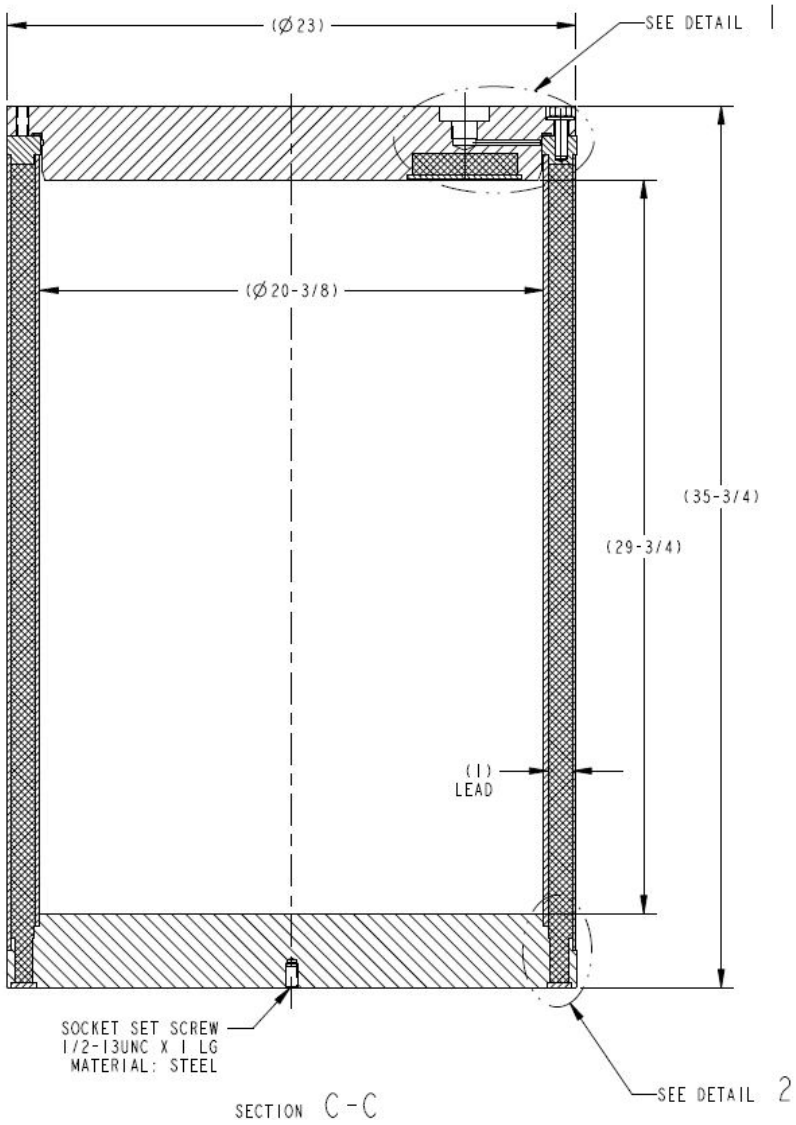

Figure H-1. SC-30G1 Shielded Container

H.1.2 Shielded Container SC-30G2

The SC-30G2 has a cylindrical sidewall with a nominal 1.5-inch-thick lead shielding between double-walled steel shells as shown in Figure H-2. The internal and external steel walls are nominally 0.3 inches thick. The upper lid of the container has an external carbon steel shell that is approximately 3.89 inches thick total with 1 inch of lead shielding internally. The lower lid is similar with 3 inches total thickness with the external shell comprised of carbon steel encasing 1.21 inches of internal lead shielding. The SC-30G2 modeled dimensions, as summarized in Table H-2, are taken from SAR Drawing 163-010 Revision 0. Tolerances are applied in a manner that maximizes the lead shielding thickness per the discussion in Section H.1.

Table H-2. Modeled SC-30G2 Shielded Container Dimensions

Dimension	Nominal Drawing Value (in.)	Nominal MAX/MIN Value (in.)	Modeled Value (in.)	Modeled Value (cm)
Outer Height	36.625	36.625	36.625	93.0275
Inner Height	29.750	29.750	29.750	75.5650
Outer Diameter	24.500	24.590	24.590	62.4586
Inner Diameter	20.375	20.230	20.230	51.3842
Total Wall Thickness	2.100	2.180	2.180	5.5372
Inner or Outer Steel Wall Thickness	0.300	0.300	0.300	0.7620
Inner Lead Thickness	1.500	1.580	1.580	4.0132
Upper Lid Total Thickness	3.890	3.890	3.890	9.8806
Bottom Total Thickness	3.000	3.000	3.000	7.6200
Bottom Inner Lead Thickness	1.210	1.215	1.215	3.0861
Bottom Steel Thickness Above Lead	0.910	0.910	0.910	2.3114
Bottom Steel Thickness Below Lead	0.880	0.875	0.875	2.2225
Upper Lid Lead Thickness	0.750	0.75	0.75	1.905
Upper Lid Lower Steel Thickness Below Lead	0.750	0.75	0.75	1.905
Upper Lid Upper Steel Thickness Above Lead	2.140	2.390	2.390	6.0706

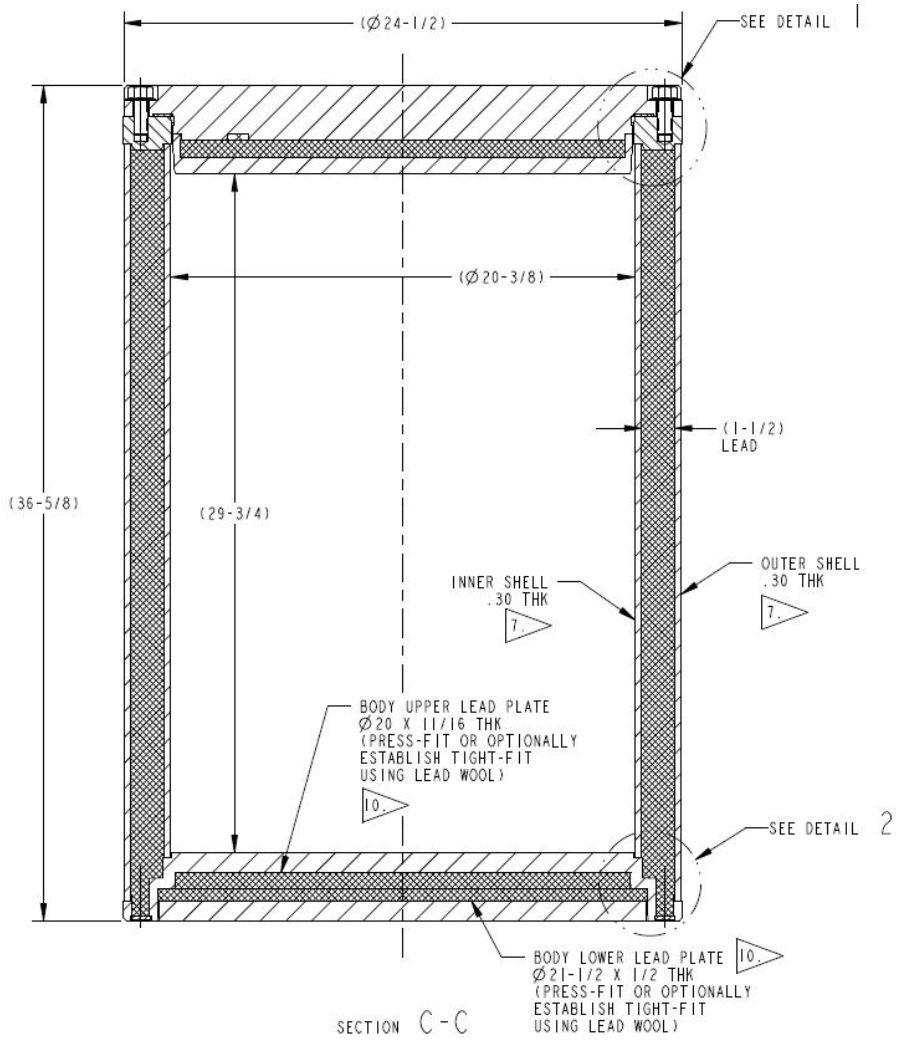

Figure H-2. SC-30G2 Shielded Container

H.1.3 Shielded Container SC-30G3

The SC-30G3 has a cylindrical sidewall with a nominal 2.75-inch-thick lead shielding between two steel shells as shown in Figure H-3. The internal and external steel walls are nominally 0.5 inches thick. The upper lid of the container has an external carbon steel shell that is approximately 6.79 inches thick total with 2.25 inches of lead shielding internally. The lower lid is similar with 5.75 inches total thickness with the external shell comprised of carbon steel and 2.25 inches of internal lead shielding. The SC-30G3 modeled dimensions, as summarized in Table H-3, are taken from SAR Drawing 163-011 Revision 0. Tolerances are applied in a manner that maximizes the lead shielding thickness per the discussion in Section H.1.

Table H-3. Modeled SC-30G3 Shielded Container Dimensions

Dimension	Nominal Drawing Value (in.)	Drawing MAX/MIN Value (in.)	Modeled Value (in.)	Modeled Value (cm)
Outer Height	42.250	42.250	42.250	107.315
Inner Height	29.750	29.750	29.750	75.565
Outer Diameter	28.000	28.130	28.130	71.450
Inner Diameter	20.375	20.230	20.230	51.384
Total Wall Thickness	3.750	3.950	3.950	10.033
Upper Lid Thickness	6.790	N/A	6.790	17.247
Top Lid Lead Thickness	2.250	N/A	2.250	5.715
Top Lid Steel Thickness Above Lead	2.750	N/A	2.750	6.985
Top Lid Steel Thickness Below Lead	1.790	N/A	1.790	4.547
Inner Steel Wall Thickness	0.500	N/A	0.500	1.270
Outer Steel Wall Thickness	0.500	N/A	0.500	1.270
Lead Sidewall Thickness	2.750	2.950	2.950	7.493
Bottom Lid Thickness	5.750	5.750	5.750	14.605
Bottom Lid Lead Thickness	2.500	2.510	2.510	6.375
Bottom Lid Steel Thickness Above Lead	1.740	N/A	1.740	4.420
Bottom Lid Steel Thickness Below Lead	1.500	N/A	1.500	3.810
Lead Ring in Top Lid Thickness	0.76	N/A	0.76	1.930
Steel Thickness above Lead Ring in Top Lid	0.19	N/A	0.19	0.483
Lead Ring in Top Lid Inner Diameter	17.75	N/A	17.75	45.085
Lead Ring in Top Lid Outer Diameter	23.50	N/A	23.50	59.690

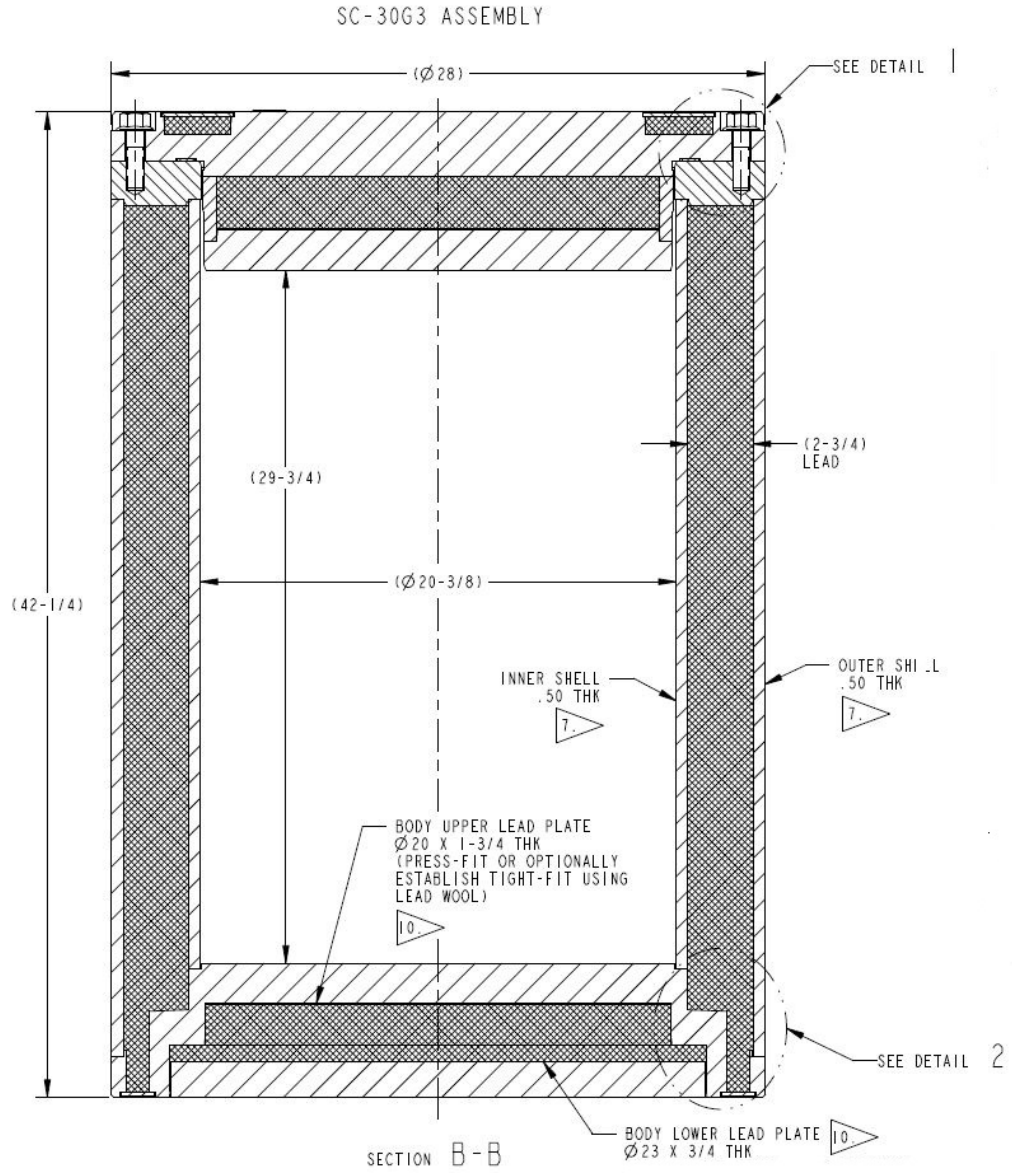

Figure H-3. SC-30G3 Shielded Container

H.1.4 Shielded Container SC-55G1

The SC-55G1 consists of a monolithic carbon steel cylindrical structure and lid. Nominally, the sidewall is comprised of 2.20 inches of steel shielding. The sidewall is connected to a 2.35-inch-thick steel bottom and the top lid is 2.40-inch thick as shown in Figure H-4. The SC-55G1 modeled dimensions, as summarized in Table H-4, are taken from SAR Drawing 163-012 Revision 0. Tolerances are applied in a manner that maximizes the steel wall thickness per the discussion in Section H.1.

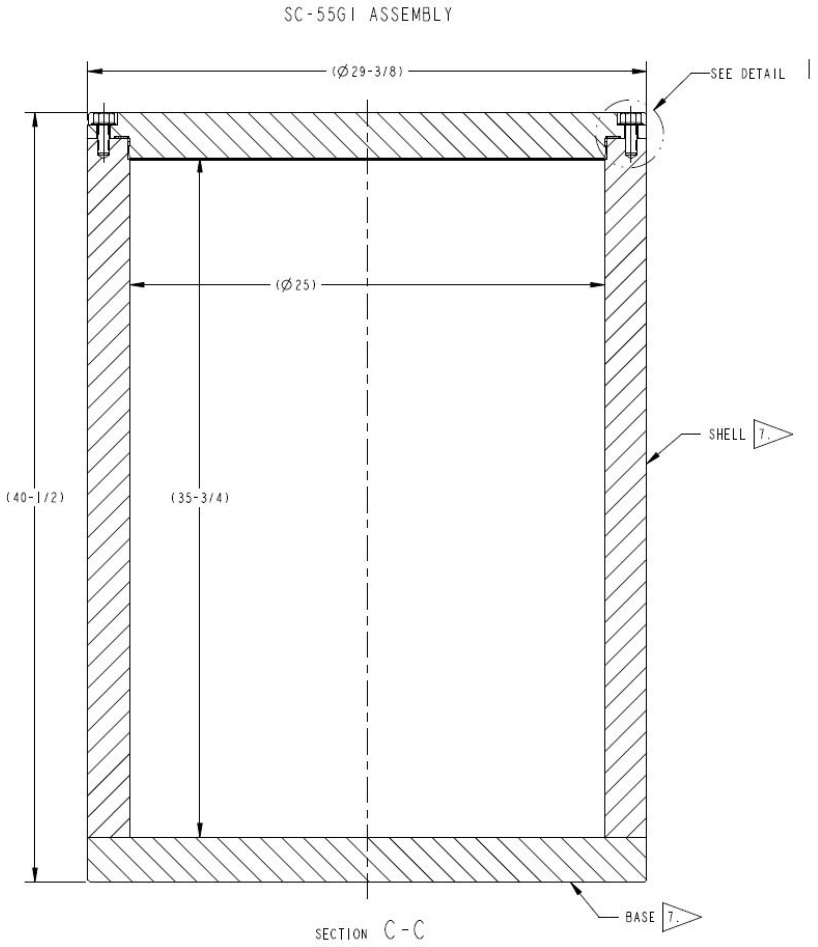

Figure H-4. SC-55G1 Shielded Container

Table H-4. Modeled SC-55G1 Shielded Container Dimensions

Dimension	Nominal Drawing Value (in.)	Drawing MAX/MIN Value (in.)	Modeled Value (in.)	Modeled Value (cm)
Outer Height	40.500	40.500	40.500	102.8700
Inner Height	35.750	35.750	35.750	90.8050
Outer Diameter	29.400	29.500	29.500	74.9300
Inner Diameter	25.000	24.900	24.900	63.2460
Total Wall Thickness	2.200	2.300	2.300	5.8420
Upper Lid Thickness	2.400	2.400	2.400	6.0960
Bottom Lid Thickness	2.350	2.350	2.350	5.9690

H.1.5 Shielded Container SC-55G2

The SC-55G2 consists of a twin-shelled, carbon steel cylindrical structure and a lid. Nominally, 2 inches of lead shielding is contained between the 0.50-inch-thick inner and outer shells. The shells are connected to an upper flange and a 4.25-inch-thick laminated lead lower lid with 1.75 inches lead internally as shown in Figure H-5. The top lid is similar being 5.75-inch thick with 1.50 inches lead internally. The SC-55G2 modeled dimensions, as summarized in Table H-5, are taken from SAR Drawing 163-013 Revision 0. Tolerances are applied in a manner that maximizes the lead shielding thickness per the discussion in Section H.1.

Table H-5. Modeled SC-55G2 Shielded Container Dimensions

Dimension	Nominal Drawing Value (in.)	Drawing MAX/MIN Value (in.)	Modeled Value (in.)	Modeled Value (cm)
Outer Height	45.750	45.750	45.750	116.2050
Inner Height	35.740	35.750	35.750	90.8050
Outer Diameter	31.000	31.130	31.130	79.0702
Inner Diameter	24.960	24.780	24.780	62.9412
Total Wall Thickness	3.020	3.175	3.175	8.0645
Inner Steel Thickness	0.500	0.500	0.500	1.2700
Body Lead Thickness	2.020	2.175	2.175	5.5245
Outer Steel Thickness	0.500	0.500	0.500	1.2700
Top Lid Thickness	5.750	5.760	5.760	14.6304
Top Lid Upper Steel Thickness	3.000	3.000	3.000	7.6200
Top Lid Lead Thickness	1.500	1.510	1.510	3.8354
Top Lid Lower Steel Lid Thickness	1.250	1.250	1.250	3.1750
Bottom Lid Thickness	4.250	4.250	4.250	10.7950
Bottom Lid Upper Steel Thickness	1.240	1.240	1.240	3.1496
Bottom Lid Upper Lead Thickness	1.000	1.010	1.010	2.5654
Bottom Lid Lower Lead Thickness	0.750	0.750	0.750	1.9050
Bottom Lid Lower Steel Base	1.250	1.250	1.250	3.1750
Lead Ring in Top Lid Thickness	0.51	0.51	0.51	1.295
Steel Thickness above Lead Ring in Top Lid	0.19	0.19	0.19	0.483
Lead Ring in Top Lid Inner Diameter	21.625	21.625	21.625	54.928
Lead Ring in Top Lid Outer Diameter	26.625	26.625	26.625	67.628

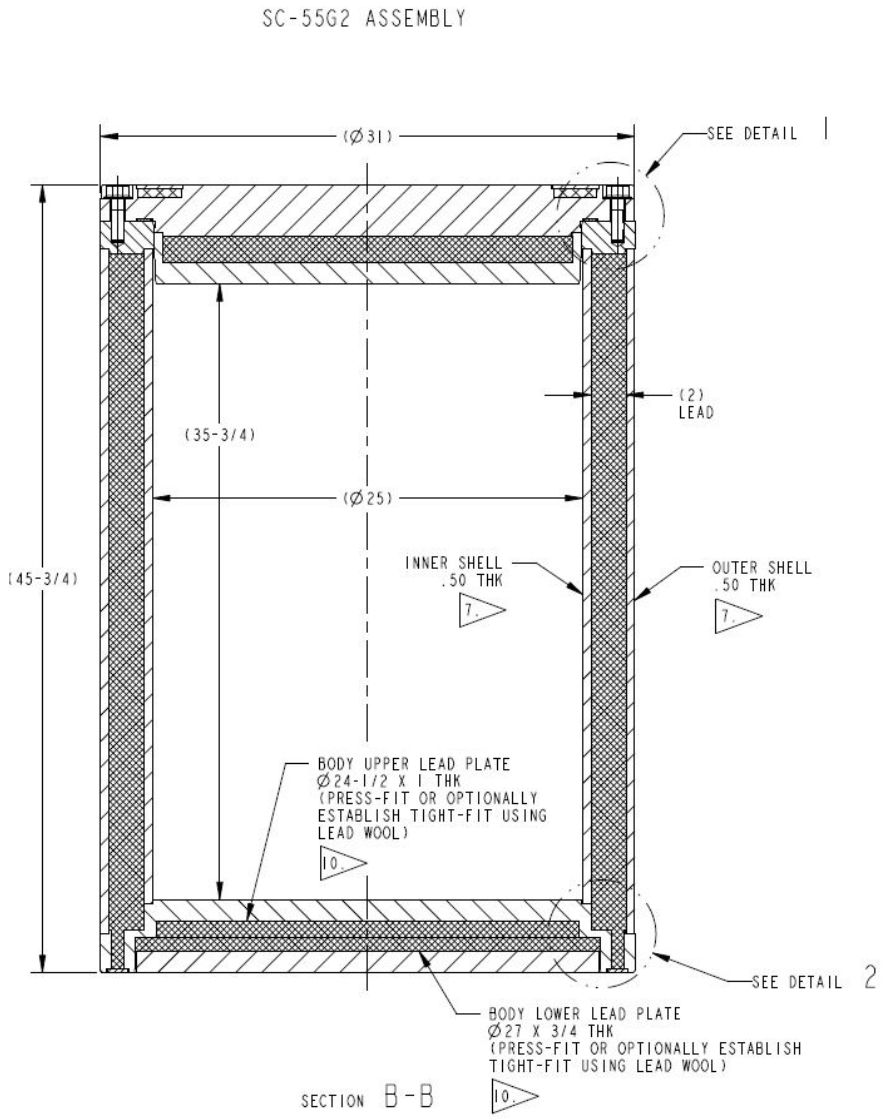

Figure H-5. SC-55G2 Shielded Container

H.2 Shielded Container Normal Condition MCNP6.2 Models

Both non-compacted and machine-compacted waste containing up to 1 wt% special reflector materials are allowed to be shipped to WIPP in shielded containers, and thus both loadings are evaluated. The FGE limit for both types of waste is 200 FGE per shielded container. The shielded containers of non-compacted (also referred to as direct loaded) waste are modeled with 200 grams of ^{239}Pu mixed with a polyethylene-water moderator, which is 25% by volume polyethylene and 75% by volume water. A mixture of beryllium and polyethylene fills the remainder of the shielded container interior reflecting the fissile mass. The ^{239}Pu density used in determining source mixtures is 19.84 g/cm^3 (*Nuclides and Isotopes Chart of the Nuclides 16th Edition*) and the theoretical densities for polyethylene, water and beryllium are 0.92 g/cm^3, 0.9982 g/cm^3 and 1.85 g/cm^3, respectively (*SCALE Code System*). The maximum polyethylene packing fraction modeled is 25% as determined to bound the packing fraction of

direct-loaded (non-machine compacted) waste in the *TRUPACT-II Safety Analysis Report* (Rev. 25 February 2022). The fissile mixture parameters for non-compacted waste are tabulated in Table H-6. Outside of the fissile mixture, the maximum polyethylene density in the reflector is 0.92 g/cm^3 × 0.25 = 0.23 g/cm^3. The amount of beryllium is based on 1 wt% of the net container loading limit of 600 pounds per the *Contact-Handled Transuranic Waste Authorized Methods for Payload Control* or 2.72 kilograms, which is rounded up to 3 kilograms beryllium per shielded container. The beryllium is modeled as homogeneously mixed throughout the polyethylene reflector. Note that beryllium is slightly more reactive modeled in the reflector than in the moderator as discussed in Section 6.4.3.2.2 of the *TRUPACT-II Safety Analysis Report*.

Table H-6. Mixture Parameters for Non-Compacted Waste Versus Hydrogen/Plutonium Ratio in MCNP6.2

H/Pu Ratio	^{239}Pu Conc. (g/l)	Mix density (g/cm^3)	Wt.% H	Wt.% O	Wt.% C-12	Wt.% C-13	Wt.% Pu	200 FGE Cylinder Radius (cm)[1]
	^{239}Pu Mixed with 75% By Volume Polyethylene and 25% By Volume H_2O							
600	46.0729	1.0225	11.3993	64.877	19.0118	0.2056	4.5061	8.84032
700	39.5042	1.0162	11.4732	65.297	19.1350	0.2070	3.8874	9.30541
800	34.5748	1.0115	11.5292	65.616	19.2284	0.2080	3.4181	9.72815
900	30.7391	1.0079	11.5732	65.866	19.3017	0.2088	3.0499	10.11703
1000	27.6695	1.0050	11.6086	66.068	19.3608	0.2094	2.7533	10.47811
1100	25.1573	1.0026	11.6377	66.234	19.4093	0.2099	2.5093	10.81589
1200	23.0633	1.0006	11.6621	66.373	19.4500	0.2104	2.3050	11.13379
1300	21.2911	0.9989	11.6828	66.490	19.4846	0.2107	2.1315	11.43451
1400	19.7718	0.9974	11.7006	66.592	19.5143	0.2111	1.9822	11.72019
1500	18.4549	0.9962	11.7161	66.680	19.5401	0.2113	1.8525	11.99259

Machine compacted waste is moderated and reflected by polyethylene at its theoretical density of 0.92 g/cm^3 as a bounding configuration for machine-compacted waste. Thus, polyethylene is modeled both intermixed within the 200 FGE in the fissile waste region and surrounding the fissile region filling the container. The fissile mixture parameters are given in Table H-7. Again, in the reflector region, 3 kilograms of beryllium is dispersed through the polyethylene to account for the up to 1 wt% special reflector material allowed in this waste form.

Table H-7. Mixture Parameters for Machine Compacted Waste Versus Hydrogen/Plutonium Ratio in MCNP6.2

H/Pu Ratio	^{239}Pu Conc. (g/l)	Mix density (g/cm^3)	Wt.% H	Wt.% C-12	Wt.% C-13	Wt. %Pu	200 FGE Cylinder Radius (cm)[1]
	^{239}Pu Mixed with 100% By Volume Polyethylene						
600	52.1276	0.9697	13.5988	80.1586	0.86697	5.3756	8.4839
700	44.6975	0.9626	13.7041	80.7790	0.87368	4.6433	8.9301
800	39.1214	0.9573	13.7841	81.2505	0.87878	4.0866	9.3357
900	34.7822	0.9532	13.8469	81.6212	0.88279	3.6491	9.7088
1000	31.3094	0.9499	13.8977	81.9201	0.88603	3.2962	10.0552
1100	28.4672	0.9471	13.9394	82.1663	0.88869	3.0056	10.3793

Table H-7. Mixture Parameters for Machine Compacted Waste Versus Hydrogen/Plutonium Ratio in MCNP6.2

H/Pu Ratio	^{239}Pu Conc. (g/l)	Mix density (g/cm^3)	Wt.% H	Wt.% C-12	Wt.% C-13	Wt. %Pu	200 FGE Cylinder Radius (cm)[1]
1200	26.0981	0.9449	13.9744	82.3726	0.89092	2.7620	10.6843
1300	24.0930	0.9430	14.0042	82.5480	0.89282	2.5550	10.9729
1400	22.3740	0.9413	14.0298	82.6989	0.89445	2.3768	11.2470
1500	20.8839	0.9399	14.0521	82.8302	0.89587	2.2219	11.5083

H.2.1 Array Model

The shielded containers are shipped with one to three assemblies in a HalfPACT and will likely be emplaced in groups of one to three in the interstitial space between 7-packs and the room wall as shown in Figure 2-6 in Section 2.1. However, the shielded container array model conservatively evaluates them in a three-high, 7-pack arrangement, similar to the array model for 55-gallon drums described in Appendix A. The limits determined for this configuration, shown in Figure H-6, will bound other array configurations of shielded containers as this configuration minimizes spacing and increases interaction between the containers.

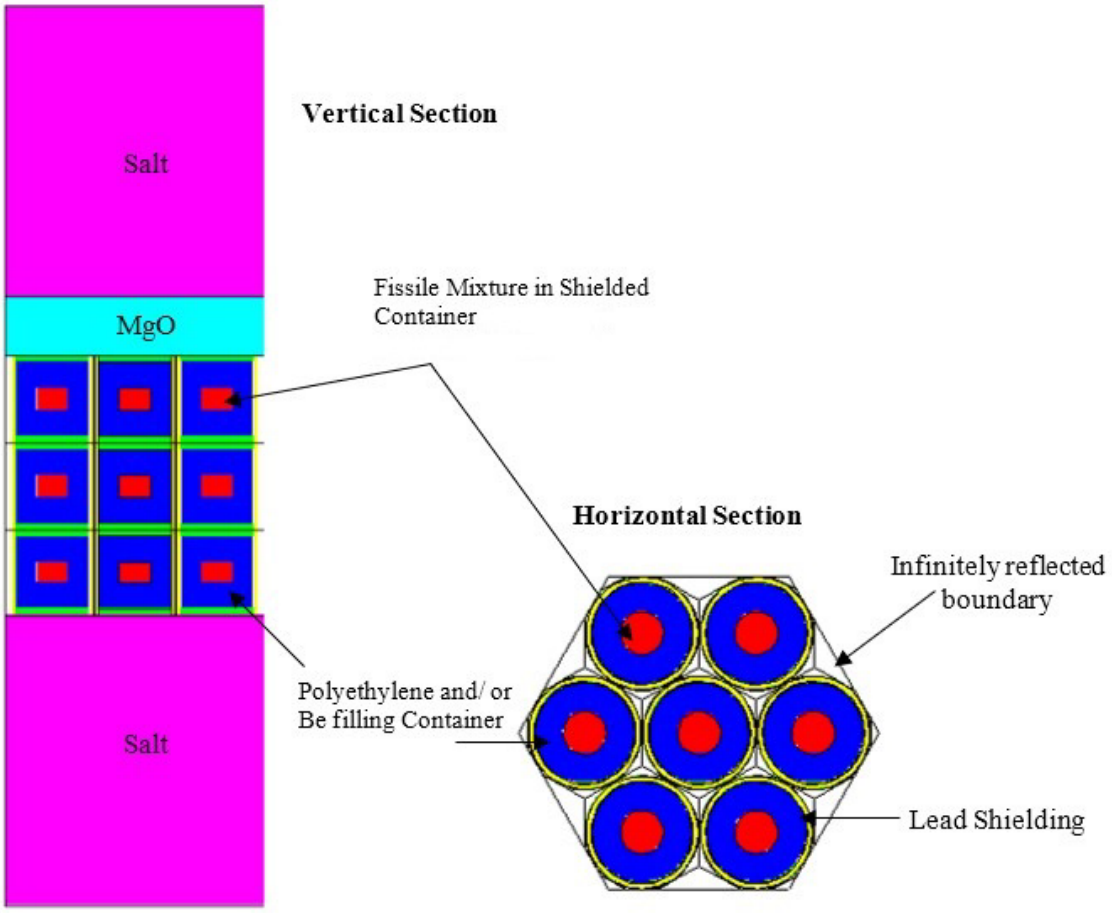

Figure H-6. Base Array Geometry for Shielded Containers Containing Less Than or Equal to 1 Weight Percent Beryllium

Table H-8 and Figure H-7 give the results of a parametric study versus H/Pu ratio for non-compacted waste and Table H-9 and Figure H-8 give the results for the machine-compacted waste in each of the shielded container models. The SC-30G1 model clearly yields the highest k_{eff} for non-compacted loadings. The SC-30G1 has the least amount of shielding of the smaller diameter SC-30 models, indicating that the interaction between the contents in the shielded containers has a larger impact on k_{eff} than the reflection from the shielding. This conclusion is further supported by the fact that the results with machine-compacted waste loadings show less variation between the shielded container designs as the polyethylene filling the container provides internal reflection that lessens the impact of the lead or steel shielding. The SC-30G1 array was also modeled with the nominal lead thickness vs. the maximum lead thickness. As expected, the nominal dimensions resulted in a slightly higher k_{eff} with non-compacted waste but had little impact when loaded with machine compacted waste. The minimum lead thickness is not given in the Shielded Container drawings cited in Section H.1.1 through H.1.5. However, as discussed in Section H.1, Shielded Containers without lead are bounded by the 55-gallon drum analyses in Appendix A for non-compacted waste and Appendix B for compacted waste. The 55-gallon drums are smaller in diameter and the Shielded Containers are emplaced in smaller packs of one to three containers, even though they are conservatively modeled in seven-packs.

The non-compacted waste containers have no polyethylene around the fissile sphere and the containers of compacted waste are filled with full density polyethylene. The peak k-effective is 0.90 for the non-compacted case compared to the peak k-effective 0.86 for machine-compacted waste. The density of the polyethylene fill was further varied from 0 to 100% TD. The results in Table H-10 confirm that ignoring the polyethylene fill is the most reactive case for non-compacted waste configurations. All results remain below the MCNP6.2 USL of 0.9659 indicating that arrays of shielded containers will remain subcritical under normal conditions.

Table H-8. Shielded Container Array Model Results with 200 FGE in Non-Compacted Waste

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
SC-30G1 with nominal dimensions				
800	0.89807	0.00024	0.89855	SC30G1a08NPRn
900	0.90383	0.00025	0.90433	SC30G1a09NPRn
1000	0.90631	0.00023	0.90677	SC30G1a10NPRn
1100	0.90615	0.00021	0.90657	SC30G1a11NPRn
1200	0.90338	0.00023	0.90384	SC30G1a12NPRn
1300	0.89927	0.00021	0.89969	SC30G1a13NPRn
1400	0.89395	0.00021	0.89437	SC30G1a14NPRn
1500	0.88756	0.00020	0.88796	SC30G1a15NPRn
SC-30G1				
800	0.89611	0.00024	0.89659	SC30G1a08npr
900	0.90268	0.00023	0.90314	SC30G1a09npr
1000	0.90493	0.00023	0.90539	SC30G1a10npr
1100	0.90448	0.00022	0.90492	SC30G1a11npr
1200	0.90198	0.00022	0.90242	SC30G1a12npr
1300	0.89795	0.00021	0.89837	SC30G1a13npr
1400	0.89223	0.00022	0.89267	SC30G1a14npr
1500	0.88588	0.00022	0.88632	SC30G1a15npr
SC-30G2				
800	0.85539	0.00025	0.85589	SC30G2a08nprc
900	0.86377	0.00023	0.86423	SC30G2a09nprc
1000	0.86763	0.00023	0.86809	SC30G2a10nprc
1100	0.86922	0.00023	0.86968	SC30G2a11nprc
1200	0.86845	0.00022	0.86889	SC30G2a12nprc
1300	0.86552	0.00021	0.86594	SC30G2a13nprc
1400	0.85648	0.00021	0.85690	SC30G2a14nprc
1500	0.85648	0.00021	0.85690	SC30G2a15nprc
SC-30G3				
800	0.78613	0.00025	0.78663	SC30G3a08npr
900	0.79762	0.00024	0.79810	SC30G3a09npr
1000	0.80437	0.00023	0.80483	SC30G3a10npr
1100	0.80875	0.00024	0.80923	SC30G3a11npr
1200	0.81078	0.00022	0.81122	SC30G3a12npr
1300	0.81082	0.00023	0.81128	SC30G3a13npr
1400	0.80912	0.00021	0.80954	SC30G3a14npr
1500	0.80637	0.00022	0.80681	SC30G3a15npr

Table H-8. Shielded Container Array Model Results with 200 FGE in Non-Compacted Waste

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
SC-55G1				
800	0.73376	0.00025	0.73426	SC55G1a08npr
900	0.74689	0.00024	0.74737	SC55G1a09npr
1000	0.75631	0.00024	0.75679	SC55G1a10npr
1100	0.76236	0.00024	0.76284	SC55G1a11npr
1200	0.76541	0.00022	0.76585	SC55G1a12npr
1300	0.76648	0.00022	0.76692	SC55G1a13npr
1400	0.76613	0.00022	0.76657	SC55G1a14npr
1500	0.76554	0.00021	0.76596	SC55G1a15npr
SC-55G2				
800	0.75182	0.00024	0.75230	SC55G2a08npr
900	0.76441	0.00025	0.76491	SC55G2a09npr
1000	0.77289	0.00025	0.77339	SC55G2a10npr
1100	0.77802	0.00023	0.77848	SC55G2a11npr
1200	0.78088	0.00023	0.78134	SC55G2a12npr
1300	0.78196	0.00022	0.78240	SC55G2a13npr
1400	0.78099	0.00021	0.78141	SC55G2a14npr
1500	0.77954	0.00022	0.77998	SC55G2a15npr

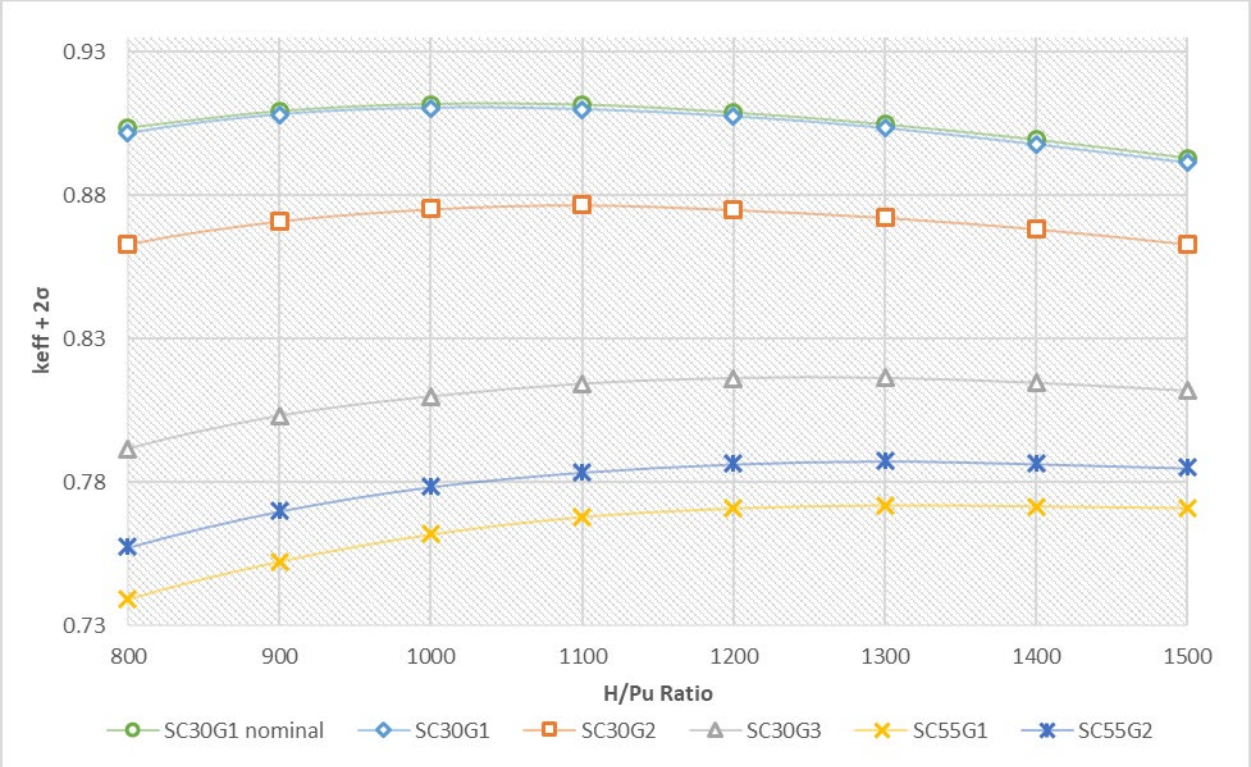

Figure H-7. Shielded Container Array with 200 FGE in Non-Compacted Waste Results

Table H-9. Shielded Container Array Model Results with 200 FGE in Machine Compacted Waste

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
SC-30G1 with nominal dimensions				
700	0.85388	0.00026	0.85440	SC30G1a07MCn
800	0.85915	0.00026	0.85967	SC30G1a08MCn
900	0.86164	0.00024	0.86212	SC30G1a09MCn
1000	0.86136	0.00026	0.86188	SC30G1a10MCn
1100	0.85925	0.00024	0.85973	SC30G1a11MCn
1200	0.85654	0.00024	0.85702	SC30G1a12MCn
SC-30G1				
700	0.85391	0.00025	0.85441	SC30G1a07MC
800	0.85935	0.00026	0.85987	SC30G1a08MC
900	0.86163	0.00026	0.86215	SC30G1a09MC
1000	0.86185	0.00025	0.86235	SC30G1a10MC
1100	0.85921	0.00025	0.85971	SC30G1a11MC
1200	0.85623	0.00023	0.85669	SC30G1a12MC
SC-30G2				
700	0.85322	0.00027	0.85376	SC30G2a07MC
800	0.85912	0.00026	0.85964	SC30G2a08MC
900	0.86175	0.00025	0.86225	SC30G2a09MC
1000	0.86166	0.00025	0.86216	SC30G2a10MC
1100	0.85947	0.00024	0.85995	SC30G2a11MC
1200	0.85610	0.00023	0.85656	SC30G2a12MC
SC-30G3				
700	0.85331	0.00025	0.85381	SC30G3a07MC
800	0.85920	0.00025	0.85970	SC30G3a08MC
900	0.86146	0.00026	0.86198	SC30G3a09MC
1000	0.86176	0.00025	0.86226	SC30G3a10MC
1100	0.85977	0.00025	0.86027	SC30G3a11MC
1200	0.85620	0.00023	0.85666	SC30G3a12MC
SC-55G1				
700	0.85306	0.00026	0.85358	SC55G1a07MC
800	0.85875	0.00025	0.85925	SC55G1a08MC
900	0.86121	0.00026	0.86173	SC55G1a09MC
1000	0.86088	0.00024	0.86136	SC55G1a10MC
1100	0.85894	0.00024	0.85942	SC55G1a11MC
1200	0.85540	0.00023	0.85586	SC55G1a12MC
SC-55G2				
700	0.85301	0.00026	0.85353	SC55G2a07MC
800	0.85859	0.00026	0.85911	SC55G2a08MC
900	0.86088	0.00025	0.86138	SC55G2a09MC
1000	0.86118	0.00025	0.86168	SC55G2a10MC
1100	0.85878	0.00023	0.85924	SC55G2a11MC
1200	0.85520	0.00024	0.85568	SC55G2a12MC

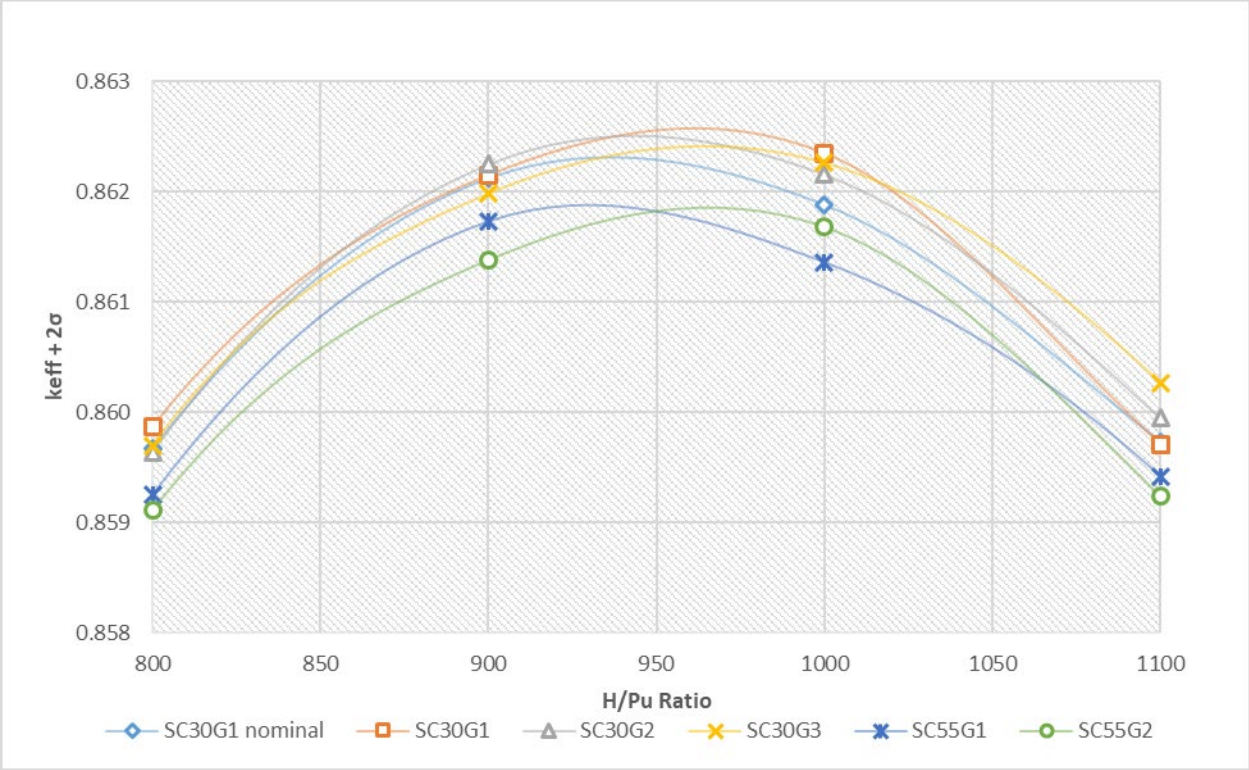

Figure H-8. Standard Array Model 200 FGE with 100% Poly mix Surrounded by 3 kg Be and 100 Poly Results

Table H-10. SC-30G1 Array Model Results vs. Polyethylene Fill Density at Optimum H/Pu Ratio

H/Pu Ratio	Polyethylene Density (% of TD)	k_{eff} + 2σ	Filename
200 FGE moderated with 25% poly/75% water with varied density polyethylene fill			
1000	0.00	0.90539	SC30G1a10npr
1500	0.10	0.74132	SC30G1e1510p
1400	0.25	0.73446	SC30G1e1425p
1200	0.50	0.76125	SC30G1e1250p
1000	0.75	0.78670	SC30G1e1075p
900	1.00	0.80511	SC30G1e0999p

H.2.2 Impact of Reflection from Shielded Container Wall on 55-gallon Drum Array

Shielded containers will be placed adjacent to other types of waste containers. A model was created with shielded containers around the seven-pack of 55-gallon drums as shown in Figure H-9 to investigate the effect of lead reflection on adjacent non-shielded containers. The outer hexagonal surface around the shielded containers is reflected to model an infinite array. The fissile mass is modeled as a cylinder located in the center of each container and the containers are stacked three tiers high with MgO and salt reflection. For this case the SC-30G1 container is evaluated as its geometry most closely mimics that of a 55-gallon drum and they can be tightly placed around the 55-gallon drum 7-pack. The SCA container types with the larger diameters were unable to be placed tightly around the array, as shown in

Figure H-10, allowing for significant neutron loss thereby resulting a significantly lower reactivity. Non-machine compacted and machine compacted configurations were modeled. For the 55-gallon drums in the 7-pack, the non-machine compacted waste configuration consists of three 200 FGE ^{239}Pu mixed and one at 50 FGE with 25% polyethylene and 75% water moderator surrounded by 5 kg of dispersed beryllium, as evaluated in Section A.2.1 of Appendix A. The 7-pack in the machine compacted configuration consists of three drums at 170 FGE ^{239}Pu and one at 90 FGE, per the requirements in Table 9-1, mixed with 100% dense polyethylene surrounded by 100% dense polyethylene mixed with 5 kg of beryllium. The empty 55-gallon drums contain 5 kg beryllium. The results are given in Table H-11 and Figure H-11. Both configurations remain below 0.89, which is less than the results for the shielded container and 55-gallon drum arrays evaluated separately and well below the USL of 0.9659. Thus, the shielded containers will reduce k_{eff} when intermixed into an array of non-shielded containers.

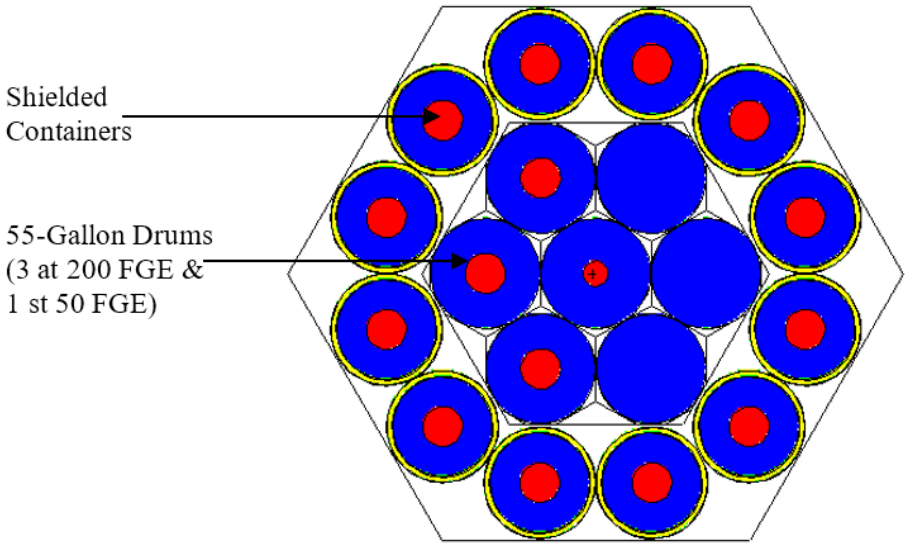

Figure H-9. Shielded Container SC-30G1 Reflection Model, X-Y Plane

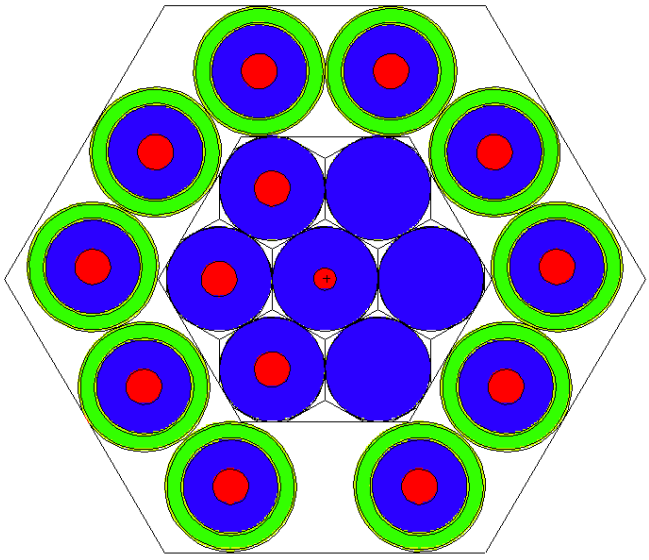

Figure H-10. Example of Other Shielded Container Physical Packing Constraints

Table H-11. Three-Tier Shielded Container SC-30G1 Reflection Model, X-Y Plane Results

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
SC-30G1 Nominal Reflection Model with Non-Compacted Waste				
800	0.86581	0.00024	0.86629	SC30G1r08n
900	0.87378	0.00023	0.87424	SC30G1r09n
1000	0.87835	0.00022	0.87879	SC30G1r10n
1100	0.87943	0.00023	0.87989	SC30G1r11n
1200	0.87880	0.00022	0.87924	SC30G1r12n
1300	0.87602	0.00022	0.87646	SC30G1r13n
1400	0.87145	0.00022	0.87189	SC30G1r14n
1500	0.86640	0.00020	0.86680	SC30G1r15n
SC-30G1 Reflection Model with Non-Compacted Waste				
800	0.87438	0.00025	0.87488	SC30G1r08
900	0.88267	0.00023	0.88313	SC30G1r09
1000	0.88626	0.00023	0.88672	SC30G1r10
1100	0.88721	0.00023	0.88767	SC30G1r11
1200	0.88620	0.00023	0.88666	SC30G1r12
1300	0.88304	0.00022	0.88348	SC30G1r13
1400	0.87922	0.00021	0.87964	SC30G1r14
1500	0.87327	0.00021	0.87369	SC30G1r15
SC-30G1 Nominal Reflection Model with Machine Compacted Waste				
800	0.85978	0.00018	0.86014	SC30G1r08MCn
900	0.86138	0.00018	0.86174	SC30G1r09MCn
1000	0.86152	0.00018	0.86188	SC30G1r10MCn
1100	0.85972	0.00017	0.86006	SC30G1r11MCn
1200	0.85611	0.00017	0.85645	SC30G1r12MCn
1300	0.85169	0.00016	0.85201	SC30G1r13MCn
1400	0.84633	0.00016	0.84665	SC30G1r14MCn
1500	0.84027	0.00017	0.84061	SC30G1r15MCn
SC-30G1 Reflection Model with Machine Compacted Waste				
800	0.85915	0.00018	0.85951	SC30G1r08MC
900	0.86146	0.00017	0.86180	SC30G1r09MC
1000	0.86183	0.00017	0.86217	SC30G1r10MC
1100	0.85946	0.00017	0.85980	SC30G1r11MC
1200	0.85608	0.00017	0.85642	SC30G1r12MC
1300	0.85159	0.00017	0.85193	SC30G1r13MC
1400	0.84652	0.00017	0.84686	SC30G1r14MC
1500	0.84011	0.00016	0.84043	SC30G1r15MC

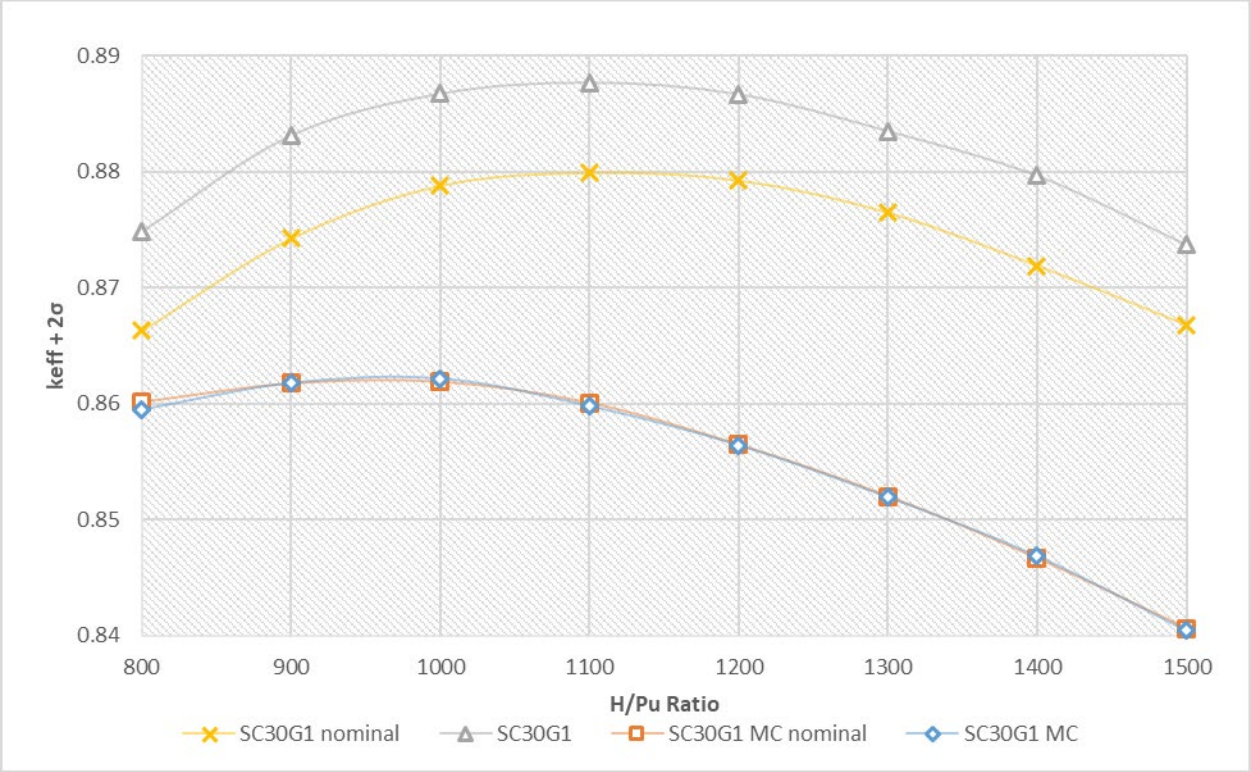

Figure H-11. Three-Tier Shielded Container Reflection Model, X-Y Plane Results

H.2.3 Two-Container Model

A two-container model is developed to evaluate the reactivity of the shielded containers with maximum interaction between the fissile material in the two containers and maximum reflection. Whereas the fissile material is centered in each container in the array model, the two-container model considers a localized, well-reflected, worst-case fissile placement. The fissile source is modeled in a cylindrical geometry with an H/D ratio of one. The fissile material in the lower shielded container is modeled at the top of the container while the fissile material in the upper shielded container is modeled at the bottom of the shielded container. To maximize reflection, the volume surrounding the fissile region is filled with either 25% dense polyethylene and 1 wt. % dispersed beryllium for non-machine compacted models or 100% dense polyethylene and 1 wt. % dispersed beryllium for machine compacted models, and the two containers are reflected by 300 cm of MgO. The two-container results in Appendix A indicate that MgO and salt reflectors yield a similar eigenvalue to a concrete reflector. In addition, scoping calculations were performed and found the MgO to be slightly more reactive. Figure H-12 shows the MCNP two-container model.

The results as a function of H/Pu ratio are tabulated in Table H-12 and Table H-13 and shown in Figure H-13 and Figure H-14, and are all well below the USL with the highest $k_{eff} + 2\sigma$ value being less than 0.874.

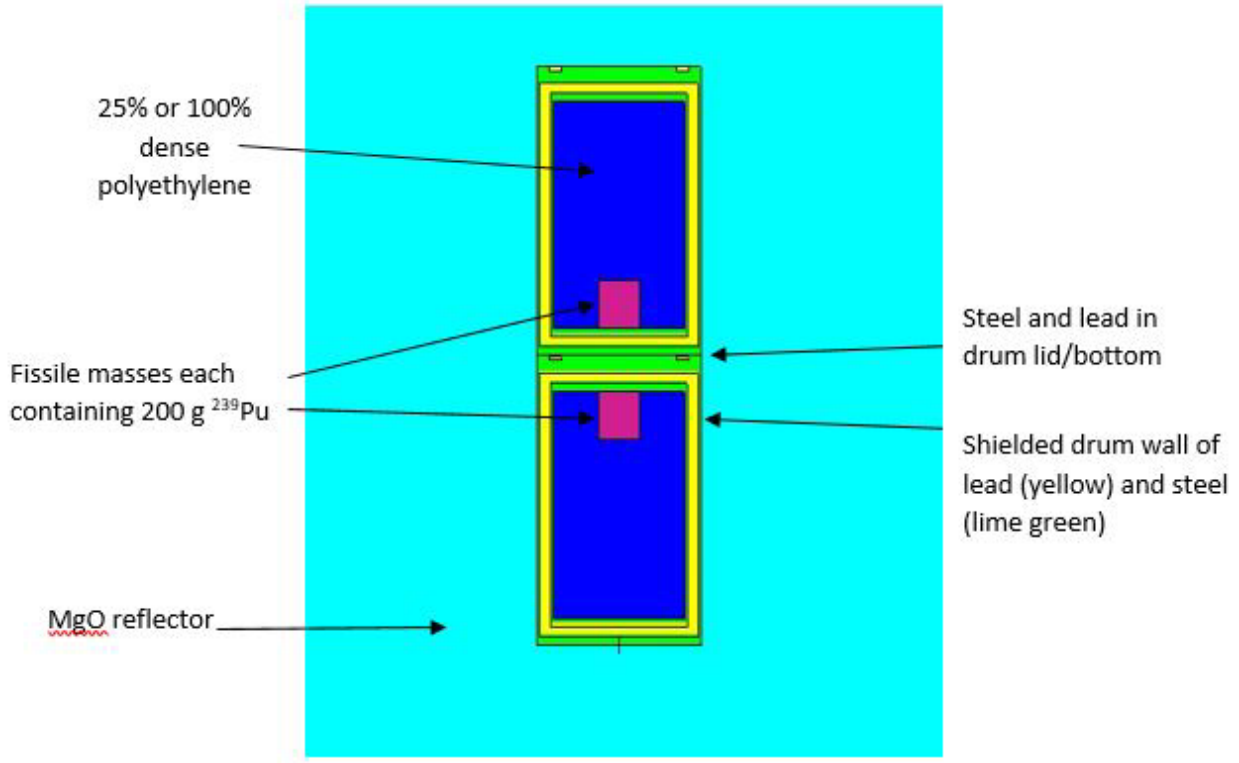

Figure H-12. MCNP Plot of 2-Drum Shielded Container Model (SC-30G2 shown)

Table H-12. Two-Container Model Results for Shielded Containers with 200 FGE in Non-Compacted Waste

H/Pu Ratio	k_{eff}	σ	k_{eff} + 2σ	Filename
SC-30G1 nominal dimensions				
1000	0.75695	0.00026	0.75747	SC30G1b10BePn
1100	0.75940	0.00024	0.75988	SC30G1b11BePn
1200	0.76133	0.00024	0.76181	SC30G1b12BePn
1300	0.76077	0.00023	0.76123	SC30G1b13BePn
1400	0.75925	0.00024	0.75973	SC30G1b14BePn
1500	0.75713	0.00024	0.75761	SC30G1b15BePn
SC-30G1				
1000	0.75722	0.00025	0.75772	SC30G1b10PBe
1100	0.75990	0.00025	0.76040	SC30G1b11PBe
1200	0.76152	0.00024	0.76200	SC30G1b12PBe
1300	0.76123	0.00024	0.76171	SC30G1b13PBe
1400	0.75960	0.00023	0.76006	SC30G1b14PBe
1500	0.75703	0.00023	0.75749	SC30G1b15PBe
SC-30G2				
1000	0.75673	0.00026	0.75725	SC30G2b10PBe
1100	0.75994	0.00026	0.76046	SC30G2b11PBe
1200	0.76144	0.00024	0.76192	SC30G2b12PBe
1300	0.76107	0.00024	0.76155	SC30G2b13PBe
1400	0.75935	0.00022	0.75979	SC30G2b14PBe
1500	0.75702	0.00022	0.75746	SC30G2b15PBe

Table H-12. Two-Container Model Results for Shielded Containers with 200 FGE in Non-Compacted Waste

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
SC-30G3				
1000	0.75065	0.00025	0.75115	SC30G3b10PBe
1100	0.75455	0.00025	0.75505	SC30G3b11PBe
1200	0.75542	0.00025	0.75592	SC30G3b12PBe
1300	0.75555	0.00024	0.75603	SC30G3b13PBe
1400	0.75474	0.00025	0.75524	SC30G3b14PBe
1500	0.75261	0.00022	0.75305	SC30G3b15PBe
SC-55G1				
1000	0.75082	0.00025	0.75132	SC55G1b10PBe
1100	0.75438	0.00025	0.75488	SC55G1b11PBe
1200	0.75525	0.00023	0.75571	SC55G1b12PBe
1300	0.75471	0.00024	0.75519	SC55G1b13PBe
1400	0.75343	0.00023	0.75389	SC55G1b14PBe
1500	0.75079	0.00023	0.75125	SC55G1b15PBe
SC-55G2				
1000	0.74312	0.00026	0.74364	SC55G2b10PBe
1100	0.74682	0.00025	0.74732	SC55G2b11PBe
1200	0.74802	0.00024	0.74850	SC55G2b12PBe
1300	0.74807	0.00023	0.74853	SC55G2b13PBe
1400	0.74685	0.00023	0.74731	SC55G2b14PBe
1500	0.74485	0.00022	0.74529	SC55G2b15PBe

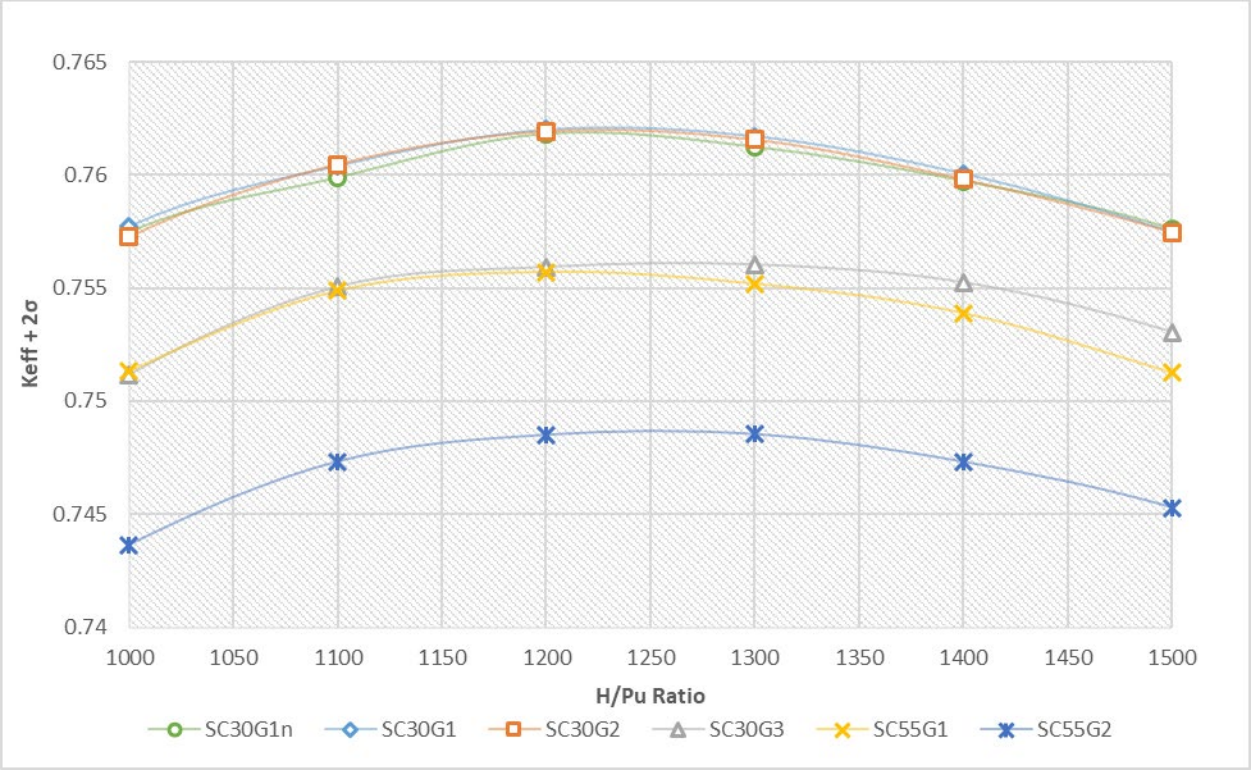

Figure H-13. Two-Container Model Results Comparison for Shielded Containers of Non-Compacted Waste

Table H-13. Two-Container Model Results for Shielded Containers with 200 FGE in Machine Compacted Waste

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
SC-30G1 with nominal dimensions				
700	0.86225	0.00026	0.86277	SC30G1b07MCn
800	0.86812	0.00026	0.86864	SC30G1b08MCn
900	0.86956	0.00025	0.87006	SC30G1b09MCn
1000	0.86984	0.00025	0.87034	SC30G1b10MCn
1100	0.86754	0.00025	0.86804	SC30G1b11MCn
1200	0.86393	0.00023	0.86439	SC30G1b12MCn
SC-30G1				
700	0.86215	0.00027	0.86269	SC30G1b07MC
800	0.86774	0.00027	0.86828	SC30G1b08MC
900	0.87035	0.00026	0.87087	SC30G1b09MC
1000	0.86991	0.00025	0.87041	SC30G1b10MC
1100	0.86801	0.00026	0.86853	SC30G1b11MC
1200	0.86422	0.00024	0.86470	SC30G1b12MC
SC-30G2				
700	0.86043	0.00027	0.86097	SC30G2b07MC
800	0.86628	0.00025	0.86678	SC30G2b08MC
900	0.86905	0.00025	0.86955	SC30G2b09MC
1000	0.86851	0.00025	0.86901	SC30G2b10MC
1100	0.86673	0.00024	0.86721	SC30G2b11MC
1200	0.86275	0.00023	0.86321	SC30G2b12MC
SC-30G3				
700	0.85622	0.00026	0.85674	SC30G3b07MC
800	0.86215	0.00025	0.86265	SC30G3b08MC
900	0.86423	0.00024	0.86471	SC30G3b09MC
1000	0.86449	0.00024	0.86497	SC30G3b10MC
1100	0.86249	0.00024	0.86297	SC30G3b11MC
1200	0.85901	0.00022	0.85945	SC30G3b12MC
SC-55G1				
700	0.86511	0.00026	0.86563	SC55G1b07MC
800	0.87046	0.00025	0.87096	SC55G1b08MC
900	0.87283	0.00026	0.87335	SC55G1b09MC
1000	0.87264	0.00026	0.87316	SC55G1b10MC
1100	0.86972	0.00024	0.87020	SC55G1b11MC
1200	0.86639	0.00023	0.86685	SC55G1b12MC
SC-55G2				
700	0.85617	0.00027	0.85671	SC55G2b07MC
800	0.86196	0.00025	0.86246	SC55G2b08MC
900	0.86489	0.00026	0.86541	SC55G2b09MC
1000	0.86469	0.00025	0.86519	SC55G2b10MC
1100	0.86284	0.00024	0.86332	SC55G2b11MC
1200	0.85971	0.00024	0.86019	SC55G2b12MC

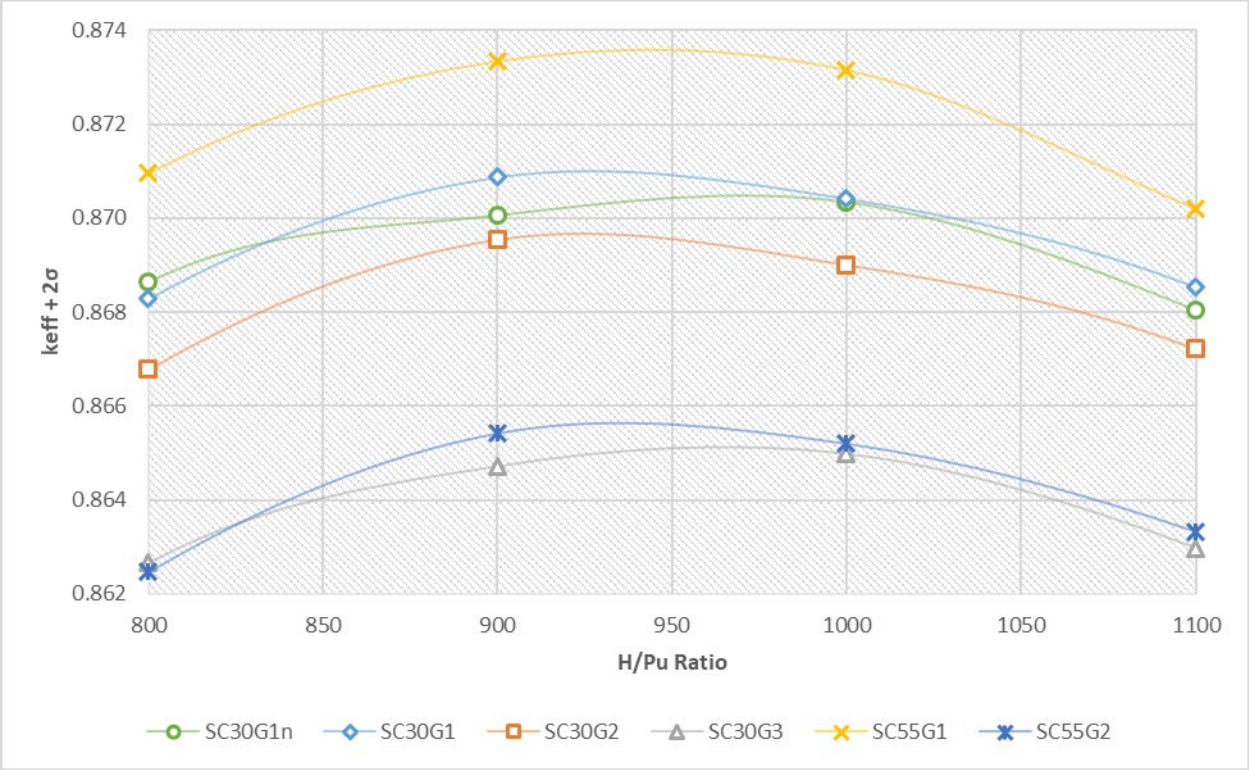

Figure H-14. Two-Container Model Results Comparison for Shielded Containers of Machine Compacted Waste

H.3 Shielded Container Contingency Models

Upset conditions, including an FGE overbatching event, a Be/BeO overbatching event, and an overstacking event, are evaluated for the underground storage array of shielded containers. Since the two-container model is sufficiently conservative to bound any contingency of realistic or expected conditions related to the interaction between small numbers of containers, only array configurations with centrally located fissile material will be considered. These upset condition models are based on the most reactive array models from Section H.2.1, namely the non-machine compacted and machine compacted configurations of the SC-30G1. The SC-30G1 is the most reactive container in the array model with both non-machine compacted and machine compacted cases with a peak $k_{eff} + 2\sigma$ values of 0.907 and 0.862 for each waste type, respectively (Table H-8 and Table H-9).

H.3.1 Shielded Container Array Overstack Model

In the underground repository, shielded containers are typically placed in the interstitial spaces along the wall between the rib and the waste array. While it is not common practice to stack shielded containers, from an NCS perspective, they are approved to be stacked three high. Thus, a four tier stack of SC-30G1 seven-packs is evaluated as the upset condition for both machine compacted and non-machine compacted waste configurations. The results for the four-tier overstack configuration are given in Table H-14 and Figure H-15. There is an increase in k_{eff} of 0.02 for the non-compacted waste loading but the compacted waste results are essentially unchanged as the polyethylene fill isolates the tiers in the stack. All results remain below the MCNP6.2 USL and thus, this upset remains subcritical.

Table H-14. SC-30G1 Four-Tier Array Model Results for Non-Compacted and Machine Compacted Waste

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
SC-30G1 with nominal dimensions and non-compacted waste				
800	0.91960	0.00024	0.92008	SC30G1f08n
900	0.92420	0.00023	0.92466	SC30G1f09n
1000	0.92563	0.00023	0.92609	SC30G1f10n
1100	0.92415	0.00022	0.92459	SC30G1f11n
1200	0.92045	0.00021	0.92087	SC30G1f12n
1300	0.91512	0.00021	0.91554	SC30G1f13n
1400	0.90879	0.00020	0.90919	SC30G1f14n
1500	0.90143	0.00020	0.90183	SC30G1f15n
SC-30G1 and non-compacted waste				
800	0.91804	0.00024	0.91852	SC30G1f08
900	0.92286	0.00024	0.92334	SC30G1f09
1000	0.92418	0.00023	0.92464	SC30G1f10
1100	0.92248	0.00022	0.92292	SC30G1f11
1200	0.91885	0.00021	0.91927	SC30G1f12
1300	0.91364	0.00021	0.91406	SC30G1f13
1400	0.90746	0.00020	0.90786	SC30G1f14
1500	0.90005	0.00020	0.90045	SC30G1f15
SC-30G1 with nominal dimensions and machine-compacted waste				
800	0.85942	0.00026	0.85994	SC30G1f08MCn
900	0.86165	0.00026	0.86217	SC30G1f09MCn
1000	0.86164	0.00024	0.86212	SC30G1f10MCn
1100	0.85970	0.00025	0.86020	SC30G1f11MCn
1200	0.85630	0.00024	0.85678	SC30G1f12MCn
1300	0.85162	0.00023	0.85208	SC30G1f13MCn
1400	0.84609	0.00023	0.84655	SC30G1f14MCn
1500	0.84018	0.00022	0.84062	SC30G1f15MCn
SC-30G1 with machine-compacted waste				
800	0.85916	0.00026	0.85968	SC30G1f08MC
900	0.86119	0.00024	0.86167	SC30G1f09MC
1000	0.86147	0.00024	0.86195	SC30G1f10MC
1100	0.85962	0.00023	0.86008	SC30G1f11MC
1200	0.85597	0.00024	0.85645	SC30G1f12MC
1300	0.85145	0.00023	0.85191	SC30G1f13MC
1400	0.84607	0.00023	0.84653	SC30G1f14MC
1500	0.83994	0.00022	0.84038	SC30G1f15MC

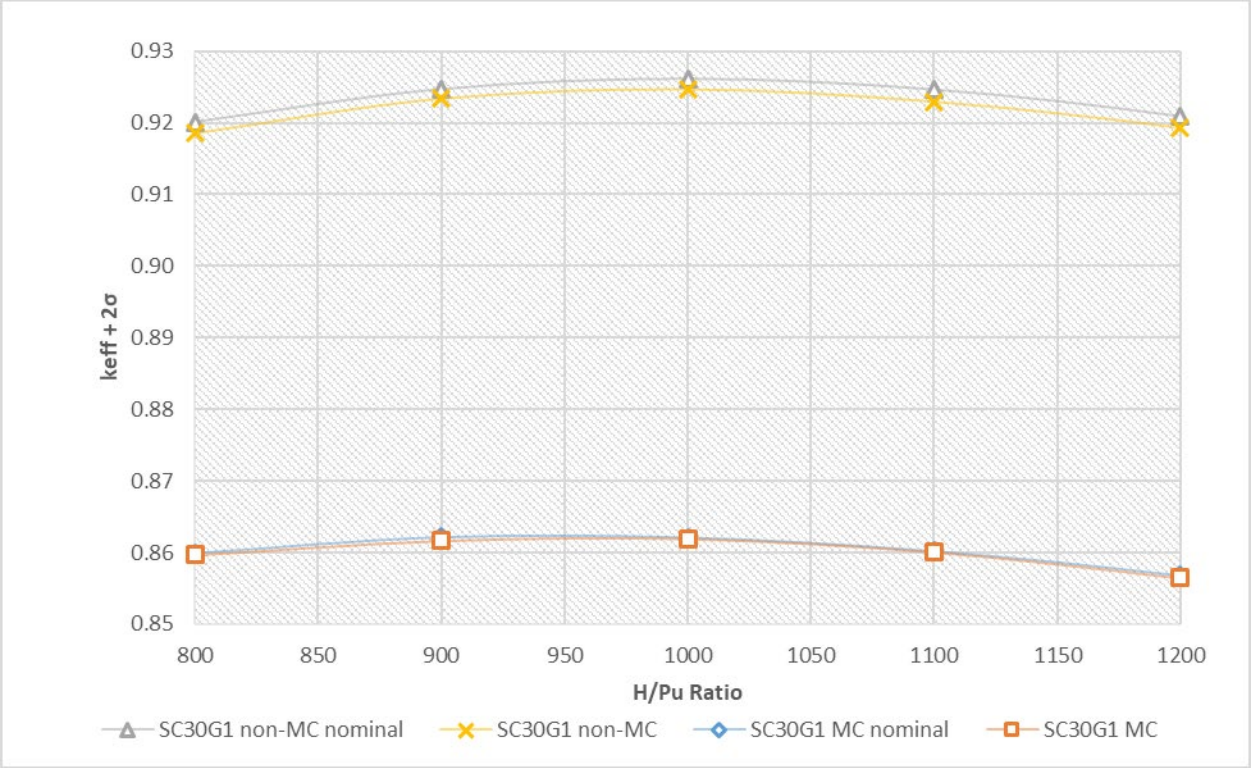

Figure H-15. SC-30G1 Four-Tier Array Model for Non-Compacted and Machine Compacted Waste

H.3.2 Shielded Container Array FGE Overbatch Model

An FGE overbatch scenario is modeled in the SC-30G1 array model. The overbatch model consists of a three-tier stack of seven SC-30G1 containers with a single container on the center outside edge overbatched by 50% to 300 FGE. Because the sides of this model are mirrored, this is equivalent to an overbatch in one out of every 21 shielded containers in the underground array with two overbatched containers in contact. As shown in the MCNP results in Table H-15 and Figure H-16, the non-compacted waste loading has a peak $k_{eff} + 2\sigma$ value of 0.92055 and the machine compacted configuration has a peak $k_{eff} + 2\sigma$ value of 0.94985. With the higher 300 FGE container, the moderation and reflection by the full density polyethylene drives k_{eff} higher than the non-compacted waste result. However, the result is lower than the result for the FGE overbatch in a 55-gallon drum array with machine compacted waste given in Section C.6.2 and all results are subcritical as they remain below the USL of 0.9659.

Table H-15. SC30-G1 Array with 300 FGE Overbatch Container Results

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
SC-30G1 nominal model with 200 FGE in Non-Compacted Waste with One Container at 300 FGE Located on the Center Tier Edge				
800	0.91202	0.00025	0.91252	SC30G1c08NPRn
900	0.91779	0.00024	0.91827	SC30G1c09NPRn
1000	0.92009	0.00023	0.92055	SC30G1c10NPRn
1100	0.91979	0.00022	0.92023	SC30G1c11NPRn
1200	0.91599	0.00022	0.91643	SC30G1c12NPRn
1300	0.91183	0.00021	0.91225	SC30G1c13NPRn
1400	0.90584	0.00021	0.90626	SC30G1c14NPRn
1500	0.89934	0.00020	0.89974	SC30G1c15NPRn
SC-30G1 model with 200 FGE in Non-Compacted Waste with One Container at 300 FGE Located on the Center Tier Edge				
800	0.91016	0.00024	0.91064	SC30G1c08ob_oco
900	0.91568	0.00024	0.91616	SC30G1c09ob_oco
1000	0.91864	0.00024	0.91912	SC30G1c10ob_oco
1100	0.91711	0.00023	0.91757	SC30G1c11ob_oco
1200	0.91477	0.00021	0.91519	SC30G1c12ob_oco
1300	0.91060	0.00022	0.91104	SC30G1c13ob_oco
1400	0.90441	0.00021	0.90483	SC30G1c14ob_oco
1500	0.89798	0.00021	0.89840	SC30G1c15ob_oco
SC-30G1 nominal model with 200 FGE in Machine Compacted Waste with One Container at 300 FGE Located on the Center Tier Edge				
700	0.94485	0.00027	0.94539	SC30G1c07MCCn
800	0.94903	0.00026	0.94955	SC30G1c08MCCn
900	0.94921	0.00025	0.94971	SC30G1c09MCCn
1000	0.94715	0.00025	0.94765	SC30G1c10MCCn
1100	0.94314	0.00023	0.94360	SC30G1c11MCCn
1200	0.93803	0.00024	0.93851	SC30G1c12MCCn
SC-30G1 model with 200 FGE in Machine Compacted Waste with One Container at 300 FGE Located on the Center Tier Edge				
700	0.94533	0.00027	0.94587	SC30G1c07MCC
800	0.94901	0.00026	0.94953	SC30G1c08MCC
900	0.94927	0.00026	0.94979	SC30G1c09MCC
1000	0.94805	0.00025	0.94855	SC30G1c10MCC
1100	0.94304	0.00024	0.94352	SC30G1c11MCC
1200	0.93847	0.00024	0.93895	SC30G1c12MCC

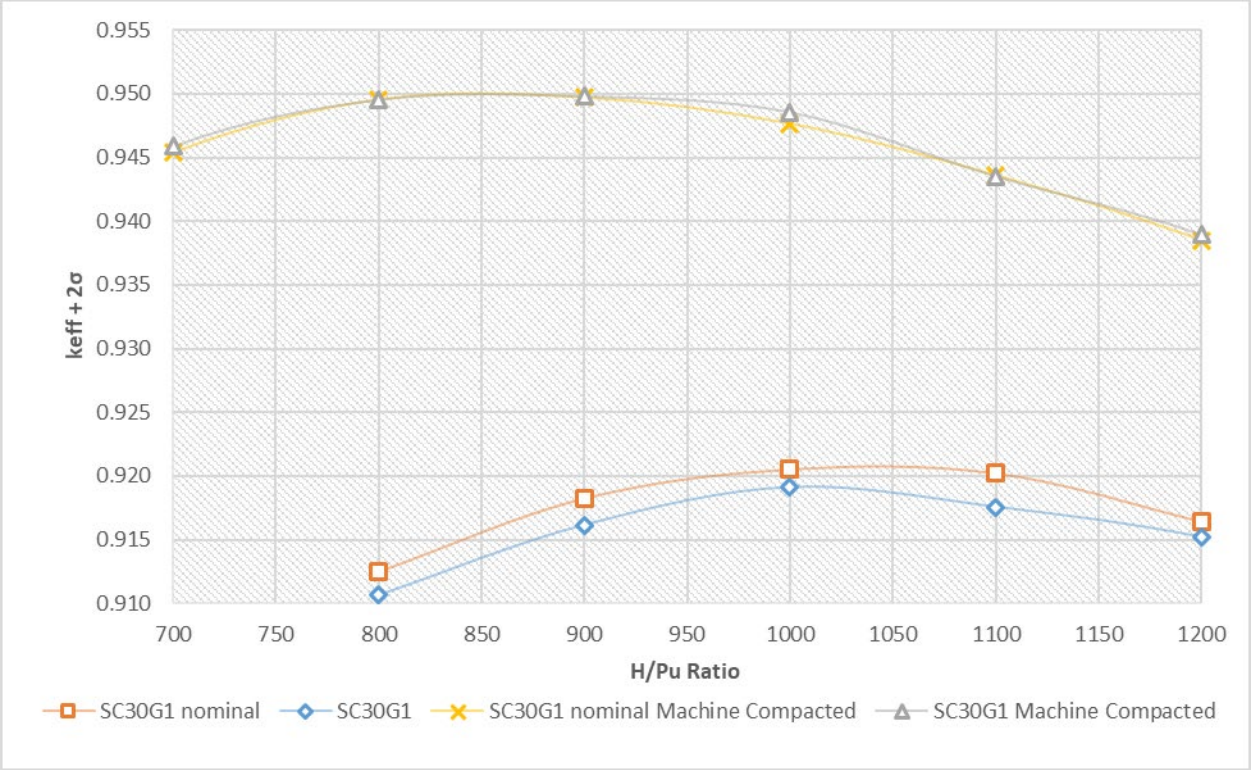

Figure H-16. Shielded Container Array with 300 FGE Overbatch Container Results

H.3.3 Shielded Container Array Be Overbatch Model

Since waste with greater than one percent by weight beryllium is prohibited in shielded containers per the CH-TRAMPAC, a waste loading with unlimited beryllium is not considered. However, a doubling of the beryllium to 2 wt% or 6 kg in all containers is evaluated for both non-compacted and machine compacted waste. As shown in the MCNP results in Table H-16 and Figure H-17, the non-compacted configuration has a peak k-effective of 0.90472 and the machine compacted configuration has a peak k-effective of 0.86359. These results are slightly lower than the results with 1 wt% beryllium and well below the USL of 0.9659.

Table H-16. SC-30G1 Array with 6 kg Be Overbatch in all Containers

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
SC-30G1 nominal model with 200 FGE in Non-compacted Waste				
800	0.89412	0.00024	0.89460	SC30G1d08BeOBn
900	0.90086	0.00024	0.90134	SC30G1d09BeOBn
1000	0.90424	0.00024	0.90472	SC30G1d10BeOBn
1100	0.90385	0.00022	0.90429	SC30G1d11BeOBn
1200	0.90168	0.00022	0.90212	SC30G1d12BeOBn
1300	0.89753	0.00020	0.89793	SC30G1d13BeOBn
1400	0.89189	0.00020	0.89229	SC30G1d14BeOBn
1500	0.88614	0.00021	0.88656	SC30G1d15BeOBn
SC-30G1 model with 200 FGE in Non-compacted Waste				
800	0.89259	0.00024	0.89307	SC30G1d08Be

Table H-16. SC-30G1 Array with 6 kg Be Overbatch in all Containers

H/Pu Ratio	k_{eff}	σ	$k_{eff} + 2\sigma$	Filename
900	0.89982	0.00023	0.90028	SC30G1d09Be
1000	0.90205	0.00023	0.90251	SC30G1d10Be
1100	0.90216	0.00022	0.90260	SC30G1d11Be
1200	0.90005	0.00022	0.90049	SC30G1d12Be
1300	0.89588	0.00022	0.89632	SC30G1d13Be
1400	0.89118	0.00020	0.89158	SC30G1d14Be
1500	0.88435	0.00020	0.88475	SC30G1d15Be
SC-30G1 nominal model with 200 FGE in Machine Compacted Waste				
700	0.85465	0.00026	0.85517	SC30G1d07MCn
800	0.86077	0.00027	0.86131	SC30G1d08MCn
900	0.86304	0.00025	0.86354	SC30G1d09MCn
1000	0.86311	0.00024	0.86359	SC30G1d10MCn
1100	0.86101	0.00024	0.86149	SC30G1d11MCn
1200	0.85700	0.00023	0.85746	SC30G1d12MCn
SC-30G1 model in 200 FGE in Machine Compacted Waste				
700	0.85485	0.00026	0.85537	SC30G1d07MC
800	0.86092	0.00026	0.86144	SC30G1d08MC
900	0.86300	0.00025	0.86350	SC30G1d09MC
1000	0.86216	0.00024	0.86264	SC30G1d10MC
1100	0.86088	0.00025	0.86138	SC30G1d11MC
1200	0.85704	0.00023	0.85750	SC30G1d12MC

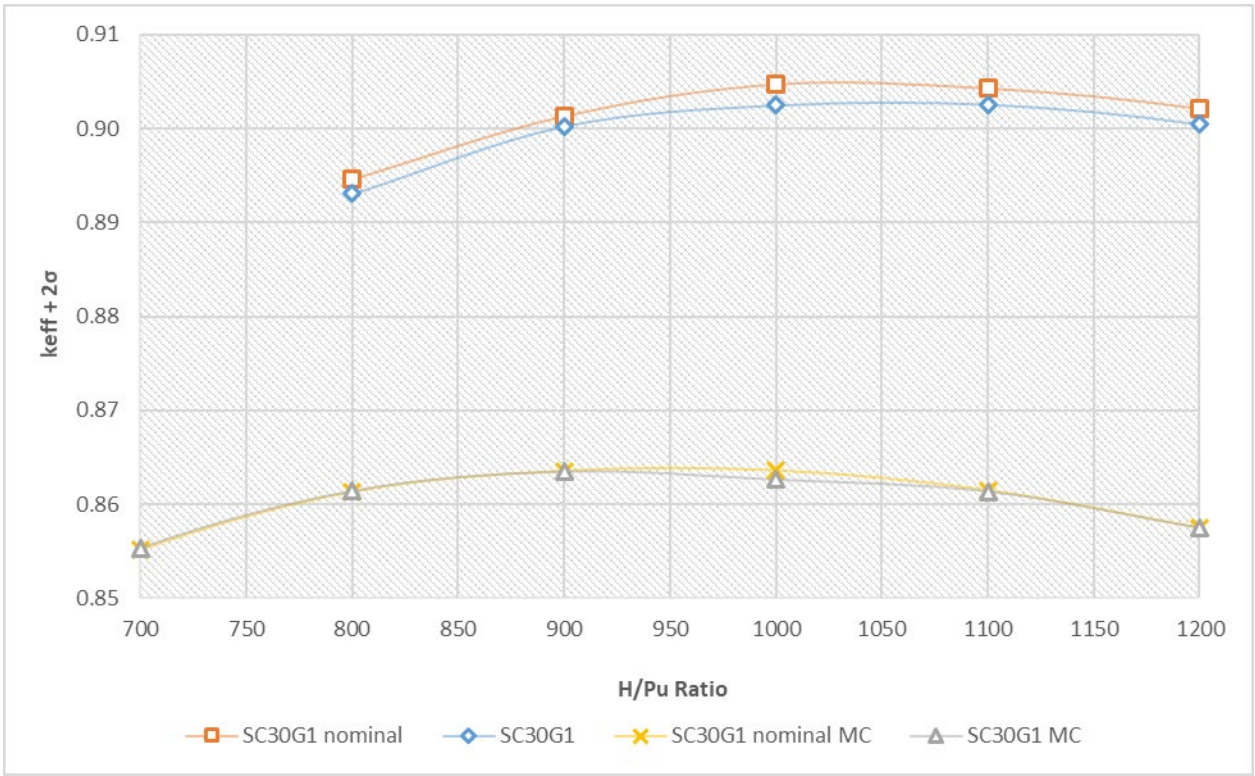

Figure H-17. SC-30G1 Array Model with 6 kg Be Overbatch in all Containers

H.4 Conclusions

This appendix demonstrates that all identified shielded container designs, SC-30G1, SC-30G2, SC-30G3, SC-55G1 and SC-55G2, will remain subcritical in the two-container configuration as well in the underground repository array with the following limits:

- Maximum 200 FGE per shielded container in non-compacted (direct loaded) waste
- Maximum 200 FGE per shielded container in machine-compacted waste
- Less than or equal to 1 wt% special reflectors (3 kilograms) per shielded container with non-compacted or machine-compacted waste.

Note: waste with > 1 wt.% beryllium is not allowed in a shielded container.

H.5 References

30G1 Shielded Container SAR Drawing, 163-008, Rev. 4.

30G2 Shielded Container SAR Drawing, 163-010, Rev. 0.

30G3 Shielded Container SAR Drawing, 163-011, Rev. 0.

55G1 Shielded Container SAR Drawing, 163-012, Rev. 0.

55G2 Shielded Container SAR Drawing, 163-013, Rev. 0.

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DOE-CBFO, 2022. *TRUPACT-II Safety Analysis Report*, Revision 25, February 2022, U.S. Department of Energy, Carlsbad Field Office, Carlsbad, NM

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Nuclides and Isotopes Chart of the Nuclides 16th Edition, Knolls Atomic Power Laboratory, Inc.; 16th edition (January 1, 2002).

Shielded Container Assembly, SCA-DWG-0001, Rev. 2.

W. A. Wieselquist, R. A. Lefebvre, and M. A. Jessee, Eds., *SCALE Code System*, ORNL/TM-2005/39, Version 6.2.4, Oak Ridge National Laboratory, Oak Ridge, TN (2020).

H.6 Sample MCNP6.2 Input File Listings for Appendix H

H.6.1 MCNP Input File (SC30G1c10MCC) SC-30G1 Overbatch Model, Standard Three Tier Array with Machine Compacted Waste, 200 FGE with 100% Poly mix Surrounded by 100% Poly with 3 kg Be Dispersed with One Container at 300 FGE:

```
     Array of  SC30G1 Shielded Containers, 200 FGE and 3kg Be per, H/Pu=      900
C    INFINITE ARRAY 7-PACK MODEL OF SHIELDED CONTAINERS WITH 200 GRAMS PU
C    EACH WITH ONE OVERBATCHED AT 300 FGE . ALL FISSILE BEARING CONTAINERS CONTAIN
C    A 100% POLY MODERATOR WHICH IS MIXED WITH THE PU. THE FISSILE
C    MASSES ARE CENTRALLY LOCATED IN THE FISSILE BEARING DRUMS AND
C    ARE CYLINDRICAL IN SHAPE WITH A H/D RATIO OF 1.0.  THE FISSILE MASSES
C    ARE REFLECTED BY THE 3 KG's of DISPERSED BERYLLIUM AND 100% POLY
C     IN THE REMAINING VOLUME.  THE STEEL WALL DENSITY IS 100%. THE 7-PACKS
C    ARE STACKED 3-HIGH WITH A MGO LAYER ON TOP.  THE UPPER AND LOWER VERTICAL
C    MIRRORED TO SIMULATE INFINITE REFLECTION IN THE LATERAL PLANE.
C CCCC
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C
C    CELL CARDS FOR THE REST OF THE UNIVERSE.
C
16    0          -50:52:61:-60:62:-65:63:-64          IMP:N=0

C
C    SURFACE CARDS FOR ALL CONTAINER SUFFACES
C
1     PZ        90.8050              $ SCA Top Outer Steel Surface
2     PZ         0.0000              $ SCA Bottom Outer Steel Surface
7     PZ        83.1850              $ SCA Top Inside Steel Surface
8     PZ         7.6200              $ Bottom Inside Steel Surface
9     CZ        29.4386              $ SCA Outer Steel Radius
10    CZ        29.1338              $ Outside Lead Radius
11    CZ        26.1722              $ Inside Lead Radius
12    CZ        25.7175              $ Inside Steel Radius
C
C    CELL CARDS FOR THE 200 FGE FISSILE MASS.
C
14    CZ         9.7088             $ Radius of fuel
16    PZ        55.1113              $ Top surface fuel
18    PZ        35.6937              $ Bottom surface fuel
C
C
C    CELL CARDS FOR THE 300 FGE FISSILE MASS.
C
15    CZ        11.1138              $ Radius of fuel
17    PZ        56.5163              $ Top surface fuel
19    PZ        34.2887              $ Bottom surface fuel
C
C    SURFACE CARDS FOR HEXAGON AROUND AN SCA
C
20    PX -29.4386                    $ Outer Radius of SCA
21    PX  29.4386                    $ Outer Radius of SCA
22    P   1   1.7321   0   58.8772   $ 2 times SCA Outer Radius
23    P  -1   1.7321   0   58.8772   $ 2 times SCA Outer Radius
24    P  -1   1.7321   0  -58.8772   $ 2 times SCA Outer Radius
25    P   1   1.7321   0  -58.8772   $ 2 times SCA Outer Radius
26    PZ  0.0000                     $ Base of SCA = 0
27    PZ  90.8050                   $ External Top of SCA
C
C    SURFACE CARDS FOR THE MGO AND SALT LAYERS.
C
50    PZ -300.00                     $ Salt thickness below SCA cm
52    PZ  634.6450                   $ SCA Stack Height + MGO + 300 cm salt
53    PZ  334.6450                   $ Stack + MGO Height of 62.3 cm
C
C    SURFACE CARDS FOR THE 3-STACK INFINITE ARRAY.
C
*60    PY -80.4263                   $ -2.732*r
*61    PY  80.4263                   $  2.732*r
*62    P   1.7321   1   0   160.8525  $ 1.7321   1   0   2*(2.732*r)
*63    P   1.7321  -1   0   160.8525  $ 1.7321  -1   0   2*(2.732*r)
*64    P   1.7321  -1   0  -160.8525  $ 1.7321  -1   0  -2*(2.732*r)
*65    P   1.7321   1   0  -160.8525  $ 1.7321   1   0  -2*(2.732*r)
66    PZ   0.0                       $ 0 Base Height
67    PZ  272.4150                   $ H*3   Stack Height

C  DATA CARDS.
MODE N
C
```

```
C  SOURCE CARDS.
KCODE 10000 1.0 100 1100
KSRC       0.00      0.00    45.40        $ First Row Center Bottom
          -58.88      0.00    45.40        $ First Row Left of Center Bottom
           58.88      0.00    45.40        $ First Row Right of Center Bottom
          -29.44     50.99    45.40        $ First Row Upper Left of Center Bottom
           29.44     50.99    45.40        $ First Row Upper Right of Center Bottom
          -29.44    -50.99    45.40        $ First Row Lower Left of Center Bottom
           29.44    -50.99    45.40        $ First Row Lower Right of Center Bottom
            0.00      0.00   136.21        $ Second Row Center Bottom
          -58.88      0.00   136.21        $ Second Row Left of Center Bottom
           58.88      0.00   136.21        $ Second Row Right of Center Bottom
          -29.44     50.99   136.21        $ Second Row Upper Left of Center Bottom
           29.44     50.99   136.21        $ Second Row Upper Right of Center Bottom
          -29.44    -50.99   136.21        $ Second Row Lower Left of Center Bottom
           29.44    -50.99   136.21        $ Second Row Lower Right of Center Bottom
            0.00      0.00   227.01        $ Third Row Center Bottom
          -58.88      0.00   227.01        $ Third Row Left of Center Bottom
           58.88      0.00   227.01        $ Third Row Right of Center Bottom
          -29.44     50.99   227.01        $ Third Row Upper Left of Center Bottom
           29.44     50.99   227.01        $ Third Row Upper Right of Center Bottom
          -29.44    -50.99   227.01        $ Third Row Lower Left of Center Bottom
           29.44    -50.99   227.01        $ Third Row Lower Right of Center Bottom
C
C  MATERIAL CARDS
C
C  PU-POLY FOR THE FISSILE MASS.
M1       94239.00C  -0.036491
         1001.00C  -0.138469
         6012.00C  -0.816212
         6013.00C  -0.008828
MT1      h-poly.40t
C
C  3 KG BE & 100% POLY AROUND THE 200 FGE FISSILE MASS.
M2        4009.00C  -0.021327
         1001.00C  -0.140649
         6012.00C  -0.829058
         6013.00C  -0.008967
MT2    be-met.40t    h-poly.40t
C
C    LEAD
M3       82204.00C    0.014
        82206.00C    0.241
        82207.00C    0.221
        82208.00C    0.524
C
C      SCA A569 STEEL WALLS.
M4        6012.00C -1.4830E-03
          6013.00C -1.7000E-05
         15031.00C -3.5000E-04
         16032.00C -3.7861E-04
         16033.00C -3.1258E-06
         16034.00C -1.8178E-05
         16036.00C -8.9732E-08
         25055.00C -6.0000E-03
         26054.00C -5.5990E-02
         26056.00C -9.1143E-01
         26057.00C -2.1425E-02
         26058.00C -2.9013E-03
C
C  MGO LAYER.
```

```
M5       8016.00C     0.5
        12024.00C   0.39495
        12025.00C     0.05
        12026.00C   0.05505
C
C  SALT REFLECTOR.
M6       11023.00C     0.5
        17035.00C    0.3789
        17037.00C    0.1211
C
C  3 KG BE & 100% POLY AROUND THE 300 FGE FISSILE MASS.
M7       4009.00C  -0.021736
         1001.00C  -0.140590
         6012.00C  -0.828711
         6013.00C  -0.008963
MT7    be-met.40t    h-poly.40t
C
C     PRINT TABLE 40 FOR MASS FRACTIONS
PRINT
```

H.6.2 MCNP Input File (SC-55G2a10MC) SC-55G2 Array with Machine Compacted Waste, 200 FGE Moderated with 100% Poly Surrounded by 100% Poly and 3 kg Be Dispersed:

```
Normal Array SC-55G2 Shielded Containers, 200 FGE and 3kg Be per, H/Pu=    1000
C     INFINITE ARRAY 7-PACK MODEL OF SHIELDED CONTAINERS WITH 200 GRAMS PU
C     EACH. ALL FISSILE BEARING CONTAINERS CONTAIN A 100% POLY
C     MODERATOR WHICH IS MIXED WITH THE PU. THE FISSILE
C     MASSES ARE CENTRALLY LOCATED IN THE FISSILE BEARING DRUMS AND
C     ARE CYLINDRICAL IN SHAPE WITH A H/D RATIO OF 1.0.  THE FISSILE MASSES
C     ARE REFLECTED BY THE 3 KG's of DISPERSED BERYLLIUM AND 100% POLY IN THE REMAINING
C     VOLUME.  THE STEEL WALL DENSITY IS 100%. THE 7-PACKS
C     ARE STACKED 3-HIGH WITH A MGO LAYER ON TOP.  THE UPPER AND LOWER VERTICAL
C     MIRRORED TO SIMULATE INFINITE REFLECTION IN THE LATERAL PLANE.
C
CCCC
```

```
                1 1 1  4 4 4 4
                 1 1   4 16R
13    0           -61 60 -62 65 -63 64 -67 66 FILL=4      IMP:N=1
C
C    CELL CARDS FOR THE MGO AND SALT LAYERS.
C
14    6   -2.165    (53:-66) -61 60 -62 65 -63 64 50 -52    IMP:N=1
15    5   -1.45     -61 60 -62 65 -63 64 67 -53             IMP:N=1
C
C    CELL CARDS FOR THE REST OF THE UNIVERSE.
C
16    0           -50:52:61:-60:62:-65:63:-64            IMP:N=0

C
C    SURFACE CARDS FOR ALL CONTAINER SUFFACES
C
1     PZ         116.2050              $ SCA Top Outer Steel Surface
2     PZ          0.0000               $ SCA Bottom Outer Steel Surface
3     PZ         109.1946              $ Lead Top Upper Surface
4     PZ         105.3592              $ Lead Top Lower Surface
5     PZ          7.6454               $ Lead Bottom Top Surface
6     PZ          3.1750               $ Lead Bottom Lower Surface
7     PZ         101.6000              $ SCA Top Inside Steel Surface
8     PZ         10.7950               $ Bottom Inside Steel Surface
9     CZ         39.5351               $ SCA Outer Steel Radius
10    CZ          38.2651              $ Outside Lead Radius
11    CZ          32.7406              $ Inside Lead Radius
12    CZ          31.4706              $ Inside Steel Radius
13    CZ          33.8138              $ Lead Ring O.R.
14    CZ          27.4638              $ Lead Ring I.R.
15    PZ          115.7224             $ Lead Ring Top Surface
16    PZ          114.1095             $ Lead Ring Bottom Surface
C
C    SURFACE CARDS FOR HEXAGON AROUND AN SCA
C
20    PX -39.5351                      $ Outer Radius of SCA
21    PX  39.5351                      $ Outer Radius of SCA
22    P   1    1.7321    0    79.0702      $ 2 times SCA Outer Radius
23    P  -1    1.7321    0    79.0702      $ 2 times SCA Outer Radius
24    P  -1    1.7321    0   -79.0702      $ 2 times SCA Outer Radius
25    P   1    1.7321    0   -79.0702      $ 2 times SCA Outer Radius
26    PZ  0.0000                      $ Base of SCA = 0
27    PZ  116.2050                     $ External Top of SCA
C    CELL CARDS FOR THE FISSILE MASS.
C
34    CZ          10.0552              $ Radius of fuel
36    PZ          66.2527              $ Top surface fuel
38    PZ          46.1423              $ Bottom surface fuel
C
C    SURFACE CARDS FOR THE MGO AND SALT LAYERS.
C
50    PZ -300.00                       $ Salt thickness below SCA cm
52    PZ  710.8450                     $ SCA Stack Height + MGO + 300 cm salt
53    PZ  410.8450                     $ Stack + MGO Height of 62.3 cm
C
C    SURFACE CARDS FOR THE 3-STACK INFINITE ARRAY.
C
*60    PY -108.0099                    $ -2.732*r
*61    PY  108.0099                    $  2.732*r
*62    P   1.7321   1    0   216.0198      $ 1.7321   1    0   2*(2.732*r)
*63    P   1.7321  -1    0   216.0198      $ 1.7321  -1    0   2*(2.732*r)
```

```
*64     P   1.7321  -1    0  -216.0198      $ 1.7321  -1    0  -2*(2.732*r)
*65     P   1.7321   1    0  -216.0198      $ 1.7321   1    0  -2*(2.732*r)
66     PZ   0.0                      $ 0 Base Height
67     PZ  348.6150                    $ H*3   Stack Height

C  DATA CARDS.
MODE N
C
C  SOURCE CARDS.
KCODE 10000 1.0 100 1100
KSRC        0.00      0.00    56.20          $ First Row Center Bottom
           -79.07     0.00    56.20          $ First Row Left of Center Bottom
            79.07     0.00    56.20          $ First Row Right of Center Bottom
           -39.54    68.48    56.20          $ First Row Upper Left of Center Bottom
            39.54    68.48    56.20          $ First Row Upper Right of Center Bottom
           -39.54    -68.48   56.20          $ First Row Lower Left of Center Bottom
            39.54    -68.48   56.20          $ First Row Lower Right of Center Bottom
             0.00      0.00   172.40          $ Second Row Center Bottom
           -79.07      0.00   172.40          $ Second Row Left of Center Bottom
            79.07      0.00   172.40          $ Second Row Right of Center Bottom
           -39.54     68.48   172.40          $ Second Row Upper Left of Center Bottom
            39.54     68.48    172.40         $ Second Row Upper Right of Center Bottom
           -39.54     -68.48   172.40         $ Second Row Lower Left of Center Bottom
            39.54     -68.48   172.40          $ Second Row Lower Right of Center Bottom
             0.00      0.00    288.61         $ Third Row Center Bottom
           -79.07      0.00    288.61         $ Third Row Left of Center Bottom
            79.07      0.00    288.61          $ Third Row Right of Center Bottom
           -39.54     68.48    288.61          $ Third Row Upper Left of Center Bottom
            39.54     68.48    288.61         $ Third Row Upper Right of Center Bottom
           -39.54     -68.48   288.61         $ Third Row Lower Left of Center Bottom
            39.54     -68.48   288.61         $ Third Row Lower Right of Center Bottom
C
C  MATERIAL CARDS
C
C  PU-POLY FOR THE FISSILE MASS.
M1    94239.00C  -0.032962
      1001.00C  -0.138977
      6012.00C  -0.819201
      6013.00C  -0.008860
MT1     h-poly.40t
C
C  3 KG BE / 100% POLY MIX AROUND THE FISSILE MASS.
M2      4009.00C  -0.011739
      1001.00C  -0.142027
      6012.00C  -0.837180
      6013.00C  -0.009055
MT2    be-met.40t    h-poly.40t
C
C    LEAD
M3   82204.00C    0.014
     82206.00C    0.241
     82207.00C    0.221
     82208.00C    0.524
C
C      SCA A569 STEEL WALLS.
M4       6012.00C -1.4830E-03
        6013.00C -1.7000E-05
       15031.00C -3.5000E-04
       16032.00C -3.7861E-04
       16033.00C -3.1258E-06
       16034.00C -1.8178E-05
```

```
        16036.00C -8.9732E-08
        25055.00C -6.0000E-03
        26054.00C -5.5990E-02
        26056.00C -9.1143E-01
        26057.00C -2.1425E-02
        26058.00C -2.9013E-03
C
C  MGO LAYER.
M5       8016.00C     0.5
        12024.00C   0.39495
        12025.00C     0.05
        12026.00C   0.05505
C
C  SALT REFLECTOR.
M6      11023.00C     0.5
        17035.00C    0.3789
        17037.00C    0.1211
C
C     PRINT TABLE 40 FOR MASS FRACTIONS
PRINT
```

H.6.3 MCNP Input File (SC-55G1b09MC) SC-55G1 Two-Container Model with Machine Compacted Waste, 200 FGE Moderated with 100% Poly Surrounded by 100% Poly 3 kg Be Dispersed Reflected by 300 cm of MgO:

```
STACKED SC-55G1 Shielded Containers, 200 FGE and 3kg Be per, H/Pu=          900
C     TWO CONTAINER MODEL OF SHIELDED CONTAINERS WITH 200 GRAMS PU
C     EACH. ALL FISSILE BEARING CONTAINERS CONTAIN A 100% POLY
C     MODERATOR WHICH IS MIXED WITH THE PU. THE FISSILE MASSES ARE AGIANST THE
C     UPPER AND LOWER INTERIOR SURFACE OF THE SCA'S RESPECTIVLY.  THIS CONFIGURATION
C     ALLOWS THE FISSLE MASSES TO BE CLOSE IN PROXIMITY.  THE FISSLE MASSES ARE CYLINDRICAL
C     IN SHAPE WITH A H/D RATIO OF 1.0.  THE FISSLE MASSES ARE REFLECTED BY THE 3 KG's OF
C     DISPERSED BERYLLIUM AND 100% POLY IN THE REMAINING VOLUME.  THE TWO-DRUM STACK
C    IS SURROUNDED ON ALL SIDES WITH 300 CM OF MGO. THE BOUNDARIES ARE MIRRORED TO
C    SIMULATE INFINITE REFLECTION.
C CCCC
```

```
C
C    SURFACE CARDS FOR ALL CONTAINER SUFFACES
C
1      PZ          102.8700            $ SCA Top Outer Steel Surface
2      PZ           0.0000             $ SCA Bottom Outer Steel Surface
7      PZ           96.7740            $ SCA Top Inside Steel Surface
8      PZ           5.9690             $ Bottom Inside Steel Surface
9      CZ          37.4650            $ SCA Outer Steel Radius
12     CZ          31.6230           $ Inside Steel Radius
C
C    SURFACE CARDS FOR THE FISSILE MASS.
C
14     CZ           9.7088             $ Radius of fuel
16     PZ           96.7739            $ Top surface fuel
18     PZ           77.3563            $ Bottom surface fuel
C
C    SURFACE CARDS FOR UPPER SCA CONTAINER
C
21     PZ          205.7401            $ UPPER SCA Top Outer Steel Surface
22     PZ          102.8701            $ UPPER SCA Bottom Outer Steel Surface
27     PZ          199.6441            $ UPPER SCA Top Inside Steel Surface
28     PZ          108.8391            $ UPPER SCA Bottom Inside Steel Surface
C
C    SURFACE CARDS FOR THE FISSILE MASS.
C
36     PZ          128.2568            $ Top surface fuel
38     PZ          108.8392            $ Bottom surface fuel
C
C    SURFACE CARDS FOR 300 CM REFLECTOR AROUND THE TWO CONTAINERS
C
*100    CZ          337.4650            $ Reflector
*101    PZ          505.7401            $ Reflector
*102    PZ          -300.0000           $ Reflector
C

C  DATA CARDS.
MODE N
C
C  SOURCE CARDS.
KCODE 10000 1.0 100 1100
KSRC        0.00      0.00     87.07         $ LOWER CONTAINER
0.00       0.00     118.55                   $ UPPER CONTAINER
C
C  MATERIAL CARDS
C
C  PU-POLY FOR THE FISSILE MASS.
M1       94239.00C   -0.036491
1001.00C   -0.138469
6012.00C   -0.816212
6013.00C   -0.008828
MT1      h-poly.40t
C
C  3 KG BE / 100% POLY MIX AROUND THE FISSILE MASS.
M2         4009.00C   -0.011598
1001.00C   -0.142047
6012.00C   -0.837299
6013.00C   -0.009056
MT2     be-met.40t        h-poly.40t
C
C       SCA A569 STEEL WALLS.
M4          6012.00C -1.4830E-03
```

```
  6013.00C -1.7000E-05
15031.00C -3.5000E-04
16032.00C -3.7861E-04
16033.00C -3.1258E-06
16034.00C -1.8178E-05
16036.00C -8.9732E-08
25055.00C -6.0000E-03
26054.00C -5.5990E-02
26056.00C -9.1143E-01
26057.00C -2.1425E-02
26058.00C -2.9013E-03
C
C  MGO LAYER.
M5        8016.00C      0.5
12024.00C    0.39495
12025.00C     0.05
12026.00C    0.05505
C
C  SALT REFLECTOR.
M6        11023.00C      0.5
17035.00C    0.3789
17037.00C    0.1211
C
C  CONCRETE
M7        1001.00C  -5.6000E-03
8016.00C  -4.9810E-01
11023.00C  -1.7100E-02
12024.00C  -2.0267E-03
12025.00C  -2.6278E-04
12026.00C  -3.0618E-04
13027.00C  -4.5700E-02
14028.00C  -2.8949E-01
14029.00C  -1.5225E-02
14030.00C  -1.0382E-02
16032.00C  -1.2305E-03
16033.00C  -1.0159E-05
16034.00C  -5.9078E-05
16036.00C  -2.9163E-07
19039.00C  -1.7844E-02
19040.00C  -2.2961E-06
19041.00C  -1.3538E-04
20040.00C  -8.0133E-02
20042.00C  -5.6153E-04
20043.00C  -1.1996E-04
20044.00C  -1.8966E-03
20046.00C  -3.8021E-06
20048.00C  -1.8548E-04
26054.00C  -7.0005E-04
26056.00C  -1.1396E-02
26057.00C  -2.6789E-04
26058.00C  -3.6276E-05
MT7      lwtr.01t
C
C     PRINT TABLE 40 FOR MASS FRACTIONS
PRINT
```

H.6.4 MCNP Input File (SC-30G1r10) SC-30G1 Reflection Model, 55-gallon Drum Array with 650 FGE Surrounded by SC-30G1s of Non-Compacted Waste, 200 FGE with 75% Poly 25% H_2O mix Surrounded by 3 kg Be Dispersed:

```
55-gal Drum Array, 650G/7-PACK, REFL BY 200G/PB CONT., H/PU=              1000
C    650 G PU per 7-PACK OF DRUMS (3=200G/1=50G) AS PER CONFIG. 4 TABLE A-1.
C    INFINITE ARRAY 7-PACK MODEL OF 55-GALLON DRUMS REFLECTIED BY
C    SHIELDED CONTIANERS. ALL FISSILE BEARING DRUMS CONTAIN A
C    75% POLY 25% H2O MODERATOR WHICH IS MIXED WITH THE PU. THE FISSILE
C    MASSES ARE CENTRALLY LOCATED IN THE FISSILE BEARING DRUMS AND
C    ARE CYLINDRICAL IN SHAPE WITH A H/D RATIO OF 1.0.  THE FISSILE MASSES
C    ARE REFLECTED BY BERYLLIUM IN THE REMAINING VOLUME. NON FISSLE DRUMS ARE
C    EMPTY. THE CONTAINER STEEL WALL DENSITY IS 100% AND THE DRUM
C    STEEL WALL DENSITY IS 50% TO ACCOUNT FOR DEGRADATION. THE 7-PACKS
C    ARE STACKED 3-HIGH WITH A MGO LAYER ON TOP.  THE UPPER AND LOWER VERTICAL
C    PLANES ARE REFLECTED BY 300 CM OF SALT.  THE LATERAL BOUNDARIES ARE
C    MIRRORED TO SIMULATE INFINITE REFLECTION IN THE LATERAL PLANE.
C CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C    CELL CARDS FOR THE 200G PU DRUMS.
1     1   -1.0050   -14 -16 18                  U=1   IMP:N=1
2     3   -0.0239    (14:16:-18)  -2 -10 8      U=1   IMP:N=1
4     6   -3.93      (2:10:-8) -4 6 -12          U=1   IMP:N=1
5     0              (4:-6:12)                   U=1   IMP:N=1
C
C    CELL CARDS FOR THE 50G PU DRUMS.
C
31    1   -1.0050   -34 -36 38                  U=2   IMP:N=1
32    3   -0.0233    (34:36:-38)  -2 -10 8      U=2   IMP:N=1
34    6   -3.93      (2:10:-8) -4 6 -12          U=2   IMP:N=1
35    0              (4:-6:12)                   U=2   IMP:N=1
C
C    CELL CARDS FOR THE 0G PU DRUMS.
C
43    3   -0.0231   -2 -10 8                    U=3   IMP:N=1
44    6   -3.93      (2:10:-8) -4 6 -12          U=3   IMP:N=1
45    0              (4:-6:12)                   U=3   IMP:N=1
C
C    CELL CARDS FOR THE HEXAGONAL 7-PACK STACK.
C
12    0               -21 20 -22 25 -23 24 -27 26 LAT=2 U=4    IMP:N=1
                     FILL=-3:3 -3:3 0:2
                     4 16R
                      1 3   4 4 4 4
                     1 2 3  4 4 4 4
                      1 3   4 16R
                     4 16R
                      1 3   4 4 4 4
                     1 2 3  4 4 4 4
                      1 3   4 16R
                    4 16R
                      1 3   4 4 4 4
                     1 2 3  4 4 4 4
                      1 3   4 16R
13    0               -61 60 -62 65 -63 64 -67 66 FILL=4       IMP:N=1
C
C    CELL CARDS FOR THE MGO AND SALT LAYERS.
C
14    8   -2.165     (53:-66) -61 60 -62 65 -63 64 50 -52     IMP:N=1
```

```
15     7    -1.45      -61 60 -62 65 -63 64 67 -53                  IMP:N=1
C
C    CELL CARDS FOR THE SHIELDED CONTAINERS.
C
21     1    -1.0050   -124 -126 128                               U=7    IMP:N=1
22     3    -0.0231    (124:126:-128)  -102 -110 108             U=7    IMP:N=1
24     6    -7.86      (102:110:-108) -104 106 -112              U=7    IMP:N=1
25     4   -11.34       104  -116          106 -112               U=7    IMP:N=1
26     6    -7.86      116:-106:112                               U=7    IMP:N=1
C
101    0            -118                        FILL=7    IMP:N=1
102    LIKE 101 BUT TRCL = (  51.17   -29.54  0)
103    LIKE 101 BUT TRCL = (  80.50   -80.35  0)
104    LIKE 101 BUT TRCL = (  80.50  -139.29  0)
105    LIKE 101 BUT TRCL = (  51.17  -190.10  0)
106    LIKE 101 BUT TRCL = (   0     -219.64  0)
107    LIKE 101 BUT TRCL = ( -58.64  -219.64  0)
108    LIKE 101 BUT TRCL = (-109.81  -190.10  0)
109    LIKE 101 BUT TRCL = (-139.13  -139.29  0)
110    LIKE 101 BUT TRCL = (-139.13   -80.35  0)
111    LIKE 101 BUT TRCL = (-109.81   -29.54  0)
112    LIKE 101 BUT TRCL = ( -58.64     0     0)
C
201    LIKE 101 BUT TRCL = (   0        0     90.79865)
202    LIKE 101 BUT TRCL = (  51.17   -29.54  90.79865)
203    LIKE 101 BUT TRCL = (  80.50   -80.35  90.79865)
204    LIKE 101 BUT TRCL = (  80.50  -139.29  90.79865)
205    LIKE 101 BUT TRCL = (  51.17  -190.10  90.79865)
206    LIKE 101 BUT TRCL = (   0     -219.64  90.79865)
207    LIKE 101 BUT TRCL = ( -58.64  -219.64  90.79865)
208    LIKE 101 BUT TRCL = (-109.81  -190.10  90.79865)
209    LIKE 101 BUT TRCL = (-139.13  -139.29  90.79865)
210    LIKE 101 BUT TRCL = (-139.13   -80.35  90.79865)
211    LIKE 101 BUT TRCL = (-109.81   -29.54  90.79865)
212    LIKE 101 BUT TRCL = ( -58.64     0     90.79865)
C
301    LIKE 101 BUT TRCL = (   0        0     181.5973)
302    LIKE 101 BUT TRCL = (  51.17   -29.54  181.5973)
303    LIKE 101 BUT TRCL = (  80.50   -80.35  181.5973)
304    LIKE 101 BUT TRCL = (  80.50  -139.29  181.5973)
305    LIKE 101 BUT TRCL = (  51.17  -190.10  181.5973)
306    LIKE 101 BUT TRCL = (   0     -219.64  181.5973)
307    LIKE 101 BUT TRCL = ( -58.64  -219.64  181.5973)
308    LIKE 101 BUT TRCL = (-109.81  -190.10  181.5973)
309    LIKE 101 BUT TRCL = (-139.13  -139.29  181.5973)
310    LIKE 101 BUT TRCL = (-139.13   -80.35  181.5973)
311    LIKE 101 BUT TRCL = (-109.81   -29.54  181.5973)
312    LIKE 101 BUT TRCL = ( -58.64     0     181.5973)
C
C    CELL CARDS FOR THE REFLECTION AREA (W/ MGO AND SALT LAYERS).
C
120    0    (61:-60:62:-65:63:-64)  -161 160 -162 165 -163 164 -167 166
         #101  #102 #103 #104 #105 #106 #107 #108 #109 #110 #111 #112
         #201  #202 #203 #204 #205 #206 #207 #208 #209 #210 #211 #212
         #301  #302 #303 #304 #305 #306 #307 #308 #309 #310 #311 #312
IMP:N=1
114    8    -2.165     (61:-60:62:-65:63:-64)  (153:-66)
                    -161 160 -162 165 -163 164 50 -52         IMP:N=1
115    7    -1.45      (61:-60:62:-65:63:-64)
                     -161 160 -162 165 -163 164 167 -153       IMP:N=1
C
```

```
C    CELL CARDS FOR THE REST OF THE UNIVERSE.
C
999  0            -50:52:161:-160:162:-165:163:-164       IMP:N=0

C
C    SURFACE CARDS FOR THE 200 FGE IN THE DRUMS.
C
14    CZ          10.47811327              $ Radius of fuel
16    PZ          52.82661327              $ Top surface fuel
18    PZ          31.87038673              $ Bottom surface fuel
C
C    SURFACE CARDS FOR THE 50 FGE IN THE DRUMS.
C
34    CZ          6.600797734              $ Radius of fuel
36    PZ          48.94929773              $ Top surface fuel
38    PZ          35.74770227              $ Bottom surface fuel
C
C    SURFACE CARDS FOR THE FISSILE MASS IN THE SCA CONTAINERS.
C
124    1 CZ        10.47811327              $ Radius of fuel
126    1  PZ       55.88061327              $ Top surface fuel
128    1 PZ        34.92438673              $ Bottom surface fuel
C
C    SURFACE CARDS FOR ALL DRUM SUFFACES
C
2    CZ  28.575
4    CZ  28.696
6    PZ  0.0
8    PZ  0.121
10    PZ  84.576
12    PZ  84.697
C
C    SURFACE CARDS FOR THE INDIVIDUAL HEXAGONS IN THE 7-PACK.
C
20    PX -28.75                           $ Outer Radius of Drum
21    PX  28.75                           $ Outer Radius of Drum
22    P   1    1.7321    0    57.5        $ 2 times Drum Outer Radius
23    P  -1    1.7321    0    57.5        $ 2 times Drum Outer Radius
24    P  -1    1.7321    0   -57.5        $ 2 times Drum Outer Radius
25    P   1    1.7321    0   -57.5        $ 2 times Drum Outer Radius
26    PZ  0.0                             $ Base of Drum = 0
27    PZ  84.697                          $ External Top of Drum
C
C    SURFACE CARDS FOR THE MGO AND SALT LAYERS (7-PACK).
C
50     PZ -300.00                         $ Salt thickness below SCA cm
52     PZ  634.6450                        $ SCA Stack Height + MGO + 300 cm salt
53     PZ  334.6450                        $ Stack + MGO Height of 62.3 cm
C
C    SURFACE CARDS FOR THE 7-PACK STACK ARRAY.
C
60    PY -78.5
61    PY  78.5
62    P   1.7321   1    0   157
63    P   1.7321  -1    0   157
64    P   1.7321  -1    0  -157
65    P   1.7321   1    0  -157
66    PZ  0.0
67    PZ  254.091
C
C    SURFACE CARDS FOR ALL SCA CONTAINER SUFFACES
```

```
C
102     1 CZ          25.71750                $ Inside Steel Radius
104     1 CZ          26.17216                $ Inside Lead Radius
106     1 PZ           0.00000               $ SCA Bottom Outer Steel Surface
108     1 PZ           7.62000               $ Bottom Inside Steel Surface
110     1 PZ          83.18500                $ SCA Top Inside Steel Surface
112     1 PZ          90.80500                $ SCA Top Outer Steel Surface
116     1 CZ          29.13380                $ Outside Lead Radius
117     1 CZ          29.43860                $ SCA Outer Steel Radius
118      1 RCC 0 0 0  0 0 90.79865  29.31922          $CONTAINER BOUNDARY
C
C    SURFACE CARDS FOR THE CONTAINER AREA REFLECTING THE 7-PACK STACK ARRAY
C
*160     PY -139.5
*161     PY  139.5
*162     P   1.7321   1    0   279
*163     P   1.7321  -1    0   279
*164     P   1.7321  -1    0  -279
*165     P   1.7321   1    0  -279
166     PZ  0.0
167     PZ  272.39595
153     PZ  334.62595     $ MGO 24.5" thick over containers

C
C  DATA CARDS.
C
TR1   29.31922  109.81922  0
C
MODE N
C
C  SOURCE CARDS.
KCODE 10000 1.0 100 1100
KSRC         0.00       0.00       42.35          $ First Row Center Bottom
            -57.39      0.00       42.35          $ First Row Right of Center Bottom bottom)
            -57.39      49.70      42.35          $ First Row Upper Right of Center Bottom
            -57.39     -49.70      42.35          $ First Row Lower Right of Center Bottom
              0.00      0.00      127.05          $ Second Row Center Bottom
            -57.39      0.00      127.05          $ Second Row Right of Center Bottom
            -57.39      49.70     127.05          $ Second Row Upper Right of Center Bottom
            -57.39     -49.70     127.05          $ Second Row Lower Right of Center Bottom
              0.00      0.00      211.74          $ Third Row Center Bottom
             -57.39     0.00      211.74          $ Third Row Right of Center Bottom
             -57.39     49.70     211.74           $ Third Row Upper Right of Center Bottom
             -57.39    -49.70     211.74           $ Third Row Lower Right of Center Bottom
C
C  MATERIAL CARDS
C
C  PU-POLY-H20 FOR THE FISSILE MASS.
C
M1        94239.00C   -0.02753306
          1001.00C     -0.1160858
          6012.00C    -0.19360755
          6013.00C    -0.00209401
          8016.00C    -0.66067958
MT1     h-h2o.40t
C
C  3 KG BE / 0% POLY MIX AROUND THE FISSILE MASS.
M3          4009.00C          -1
MT3     be-met.40t
C
C    LEAD (density = 11.34 g/cc)
```

```
M4        82204.00C     0.014
         82206.00C     0.241
         82207.00C     0.221
         82208.00C     0.524
C
C  STEEL WALLS.
M6          6012.00C  -1.48300E-03
            6013.00C  -1.70000E-05
           15031.00C  -3.50000E-04
           16032.00C  -3.78610E-04
           16033.00C  -3.12580E-06
           16034.00C  -1.81780E-05
           16036.00C  -8.97320E-08
            25055.00C  -6.00000E-03
            26054.00C  -5.59900E-02
            26056.00C  -9.11430E-01
            26057.00C  -2.14250E-02
            26058.00C  -2.90130E-03
C
C  MGO LAYER.
M7          8016.00C  0.5
         12024.00C  0.39495
         12025.00C  0.05
         12026.00C  0.05505
C
C  SALT REFLECTOR.
M8         11023.00C      0.5
           17035.00C    0.3789
           17037.00C    0.1211
C
C     PRINT TABLE 40 FOR MASS FRACTIONS
C
PRINT
```